# QUARRY RIDGE PROJECT 

## SCH\# 2017092027

# Final Environmental Impact REPORT 



ApriL 2019

# Quarry Ridge Project Final Environmental Impact Report 

SCH\# 2017092027

Lead Agency:<br>County of Placer Community Development Resource Agency<br>3091 County Center Drive, Suite 190<br>Auburn, CA 95603<br>Shirlee Herrington<br>Environmental Coordination Services<br>(530) 745-3132

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## APPENDIX

A. Revised Traffic Impact Analysis (April 1, 2019)

## 1. INTRODUCTION AND LIST OF COMMENTERS

### 1.1 INTRODUCTION

This Final Environmental Impact Report (EIR) contains agency, group, and public comments received during the public review period of the Quarry Ridge Project (proposed project) Draft EIR. This document has been prepared by Placer County, as Lead Agency, in accordance with the California Environmental Quality Act (CEQA) and the CEQA Guidelines, Section 15132. The Introduction and List of Commenters chapter of the Final EIR discusses the background of the Draft EIR and purpose of the Final EIR, identifies the comment letters received on the Draft EIR, and provides an overview of the Final EIR's organization.

### 1.2 BACKGROUND

The Draft EIR identified the proposed project's potential environmental impacts and the mitigation measures that would be required to be implemented. The following environmental analysis chapters are contained in the Draft EIR:

- Noise;
- Transportation and Circulation;
- Statutorily Required Sections; and
- Alternatives.

In accordance with CEQA, a Notice of Completion (NOC) of the Draft EIR was published on the Placer County Community Development Resource Agency website, and the Draft EIR was sent to the State Clearinghouse (SCH\#: 2017092027) for distribution to State agencies on January 22, 2019 for a 45-day public review period, ending on March 7, 2019. The Draft EIR was also posted on the Placer County website, and printed copies of the document were made available for review at: 1) the Granite Bay Public Library, located at 6475 Douglas Boulevard, Granite Bay, CA, 2) the Placer County Community Development Resource Agency offices in Auburn, located at 3091 County Center Drive, Auburn, CA, and 3) the County Clerk’s Office, located at 2954 Richardson Drive, Auburn, CA. In addition, a public hearing was held on February 14, 2019 to solicit public comments regarding the Draft EIR.

### 1.3 Purpose of the Final EIR

Under CEQA Guidelines Section 15132, the Final EIR shall consist of:

1. The Draft EIR or a revision of the Draft.
2. Comments and recommendations received on the Draft EIR.
3. A list of persons, organizations, and public agencies commenting on the Draft EIR.
4. The responses to significant environmental points raised in the review process.
5. Any other information added by the Lead Agency.

As required by CEQA Guidelines, Section 15090(a)(1)-(3), a Lead Agency must make the following three determinations in certifying a Final EIR:

1. The Final EIR has been completed in compliance with CEQA.
2. The Final EIR was presented to the decision-making body of the Lead Agency, and the decision-making body reviewed and considered the information in the Final EIR prior to approving the project.
3. The Final EIR reflects the Lead Agency's independent judgment and analysis.

Under CEQA Guidelines Section 15091, a public agency shall not approve or carry out a project for which an EIR has been certified that identifies one or more significant environmental effects of the project unless the public agency makes one or more written findings (Findings of Fact) for each of those significant effects. Findings of Fact must be accompanied by a brief explanation of the rationale for each finding supported by substantial evidence in the record. The Findings of Fact are included in a separate document that will be considered for adoption by the County's decision-makers.

Pursuant to CEQA Guidelines, Section 15093(b), when a Lead Agency approves a project that would result in significant and unavoidable impacts, the agency must state in writing the reasons supporting the action (Statement of Overriding Considerations). The Statement of Overriding Considerations shall be supported by substantial evidence. Here, the proposed project would not result in any project-level or cumulative significant and unavoidable impacts; thus, a Statement of Overriding Considerations is not required.

### 1.4 LIST OF COMMENTERS

Placer County received eight comment letters during the public comment period on the Draft EIR for the proposed project. The comment letters, presented in the order in which they were received, were authored by the following agencies, groups, and members of the public:

## Agencies

Letter 1
Terri Shirhall, City of Roseville
Letter 2.........................................................Ralph Gibson, Placer County Museums Division

## Groups

Letter 3 Cherilyn Neider, United Auburn Indian Community
Letter 4........................................... Daniel Fonseca, Shingle Springs Band of Miwok Indians
Letter 5.............................................. Sandra H. Harris, Granite Bay Community Association

## Members of the Public

| Lette | issa Berry |
| :---: | :---: |
| Letter 7. | Shannon Quin |
| Letter 8. | Holly Johnson |

In addition, verbal comments were provided during the February 14, 2019 public meeting to accept comments on the Draft EIR. The comments from the Draft EIR comment meeting are included as Letter 9.

Letter 9 Verbal Comments: Draft EIR Public Meeting (February 14, 2019)

### 1.5 Organization of the Final EIR

The Final EIR is organized into the following chapters:

## 1. Introduction and List of Commenters

Chapter 1 provides an introduction and overview of the document, describing the background and organization of the Final EIR. Chapter 1 also provides a list of commenters who submitted letters in response to the Draft EIR.

## 2. Responses to Comments

Chapter 2 presents the comment letters received and responses to each comment. Each comment letter received has been numbered at the top and bracketed to indicate how the letter has been divided into individual comments. Each comment is given a number with the letter number appearing first, followed by the comment number. For example, the first comment in Letter 1 would have the following format: 1-1. The response to each comment will reference the comment number.

## 3. Revisions to the Draft EIR Text

Chapter 3 summarizes minor changes made to the Draft EIR text since its release.

## 4. Mitigation Monitoring and Reporting Program

CEQA Guidelines, Section 15097, requires lead agencies to adopt a program for monitoring the mitigation measures required to avoid the significant environmental impacts of a project. The intent of the Mitigation Monitoring and Reporting Program (MMRP) is to ensure implementation of the mitigation measures identified within the EIR for the Quarry Ridge Project.

## 2. RESPONSES TO COMMENTS

## RESPONSES TO COMMENTS

This chapter contains responses to each of the comment letters submitted regarding the Quarry Ridge Project Draft EIR. Each bracketed comment letter is followed by numbered responses to each bracketed comment. The responses amplify or clarify information provided in the Draft EIR and/or refer the reader to the appropriate place in the document where the requested information can be found. Comments that are not directly related to environmental issues (e.g., opinions on the merits of the project that are unrelated to its environmental impacts) are either discussed or noted for the record, as appropriate. Where revisions to the Draft EIR text are required in response to the comments, such revisions are noted in the response to the comment, and are also listed in Chapter 3 of this Final EIR. All new text is shown as double underlined and deleted text is shown as struek through.

The changes to the analysis contained in the Draft EIR represent only minor clarifications/amplifications and do not constitute significant new information. In accordance with CEQA Guidelines, Section 15088.5, recirculation of the Draft EIR is not required.

## Letter 1

Development Services Department
Planning Division
311 Vernon Street
Roseville, California 95678-2649

March 5, 2019

Ms. Shirlee Herrington
Environmental Coordination Services
Placer County Community Development Resource Agency
3091 County Center Drive, Suite 190
Auburn, CA 95603

## Subject: Quarry Ridge Professional Office Park - DEIR Comments

Dear Ms. Herrington:
This comment letter is in response to the County's January 22, 2019 Notice of Availability of the Quarry Ridge Office Park Draft Environmental Impact Report. The City is concerned that existing intersection levels of service and congestion will continue to worsen with addition of vehicle trips generated by this and other pending projects proposed east of Sierra College Boulevard.

1-1 Due to existing capacity constraints on eastbound Douglas Boulevard at Sierra College Boulevard, the PM peak hour is experiencing severe congestion. As stated in previous comments submitted by the City for other Placer County development projects along Douglas Boulevard, the City of Roseville is supportive of mitigation fee payment into the County fee program for capacity improvements. Specifically, improvements at Douglas and Sierra College to extend the three eastbound through lanes through Cavitt Stallman Road.

Should the County have any questions concerning these comments, please don't hesitate to contact Jason Shykowski, Acting Public Works Director, at (916) 774-5331.

Sincerely,
Teistllo
Terri Shirhall
Environmental Coordinator

## Letter 1: Terri Shirhall, City of Roseville

## Response to Comment 1-1

The County appreciates the City's concern about increased vehicle trips associated with the proposed project and other pending projects east of Sierra College Boulevard. As discussed in Chapter 5, Transportation and Circulation, of the Draft EIR, Mitigation Measure 5-8 would require the project applicant to pay traffic impact mitigation fees pursuant to applicable Ordinances and Resolutions. The current estimate for the total project fees is $\$ 504,715.52$. Such fees would be used to fund necessary roadway improvements included in the County's Capital Improvement Program (CIP). Currently, the Granite Bay Fee Program includes a planned improvement at the Douglas Boulevard/Sierra College Boulevard intersection to extend the three eastbound lanes through Cavitt Stallman Road. Thus, while the proposed project would not directly improve the identified segment of Douglas Boulevard east of Sierra College Boulevard, the project would provide for a fair-share contribution towards the improvement, as requested in the comment.

It should be noted that the analysis within Chapter 5, Transportation and Circulation, of the Draft EIR includes consideration of pending and approved projects east of Sierra College Boulevard, specifically under the Existing Plus Approved/Pending Projects (EPAP) Condition and the Cumulative Plus Project Condition. In developing the EPAP Condition, Placer County staff identified a list of 33 pending and approved projects within Granite Bay. A complete list of the pending and approved projects analyzed, along with the trip generation for each individual project, is included in Table 16 of the Traffic Impact Analysis (see Appendix E to the Draft EIR). Cumulative conditions were developed using the Future Year 2036 traffic volume forecasts from the County's regional travel demand forecasting model. As discussed in Chapter 5 of the Draft EIR, under both the EPAP Plus Project and Cumulative Plus Project Conditions, the proposed project would not result in any significant impacts to study intersections or roadway segments, using the relevant LOS thresholds. Therefore, the proposed project would not substantially degrade operations or otherwise result in significant impacts to the Douglas Boulevard/Sierra College Boulevard intersection.

## Response to Comment 1-2

The comment is a concluding statement and does not address the adequacy of the Draft EIR.

## Letter 2



2-1
I read through the materials provided for the above project and I conducted research of the area at our Archives and Research Facility. I concur with the findings and recommendations by Natural Investigations who performed a pedestrian survey of the area and conducted research.

Although not related to Cultural Resources, I would add that if any Paleontological resources are discovered during grading activities, that the project coordinator contact Dr. Richard Hilton at Sierra College.

If you have any questions or need further information please feel free to contact me at: 530-889-6502 or rgibson@placer.ca.gov

## Letter 2: Ralph Gibson, Placer County Museums Division

## Response to Comment 2-1

The comment expresses concurrence with the conclusions presented in the Cultural and Paleontological Resource Inventory prepared for the proposed project by Natural Investigations Company, and does not address the adequacy of the Draft EIR.

## Response to Comment 2-2

As discussed on page 49 of the Initial Study prepared for the proposed project, per the Cultural and Paleontological Resources Inventory prepared for the proposed project by Natural Investigations Company, the project site is underlain by Rocklin Pluton, which consists of Mesozoic-aged rocks dated to the Lower Cretaceous period. Because of the geologic process involved in the formation of such rocks (high temperature and pressure at great depth), fossils do not have the potential to occur on the project site. Nonetheless, the comment has been forwarded to the project applicant for their consideration.

## Letter 3

From: Cherilyn Neider [mailto:cneider@auburnrancheria.com]
Sent: Tuesday, February 05, 2019 3:40 PM
To: Placer County Environmental Coordination Services; Jennifer Byous
Cc: Matthew Moore; Melodi McAdams
Subject: Notice of Availability of a Draft EIR for the Quarry Ridge Office Park (PLN16-00157)
Good afternoon Jennifer,
3-1 I am writing in response to the recent notice of availability for the Draft EIR for the Quarry Ridge Office Park project. We have reviewed the draft EIR had have a couple of questions and concerns.

In searching our records we were unable to find a letter notifying the United Auburn Indian Community of AB 52 consultation for this project. Can you provide additional information on the letter referred to on page 10 of the Initial Study?

There are a number of tribal cultural resources within the vicinity of the project area. In addition to the measures included in the draft EIR, we recommend that the attached measure incorporating a tribal cultural resource awareness training is incorporated as a third measure into the final EIR. Attached you will find a draft measure for the training and a brochure to accompany the training. We request that these measures are included under the section addressing Tribal Cultural Resources.

Thank you for considering these concerns.
Respectfully,
Cherilyn

## Cherilyn Neider

Tribal Historic Preservation
United Auburn Indian Community
530.883.2394

Nothing in this e-mail is intended to constitute an electronic signature for purposes of the Electronic Signatures in Global and National Commerce Act (E-Sign Act), 15, U.S.C. $\S \$ 7001$ to 7006 or the Uniform Electronic Transactions Act of any state or the federal government unless a specific statement to the contrary is included in this e-mail.

Nothing in this e-mail is intended to constitute an electronic signature for purposes of the Electronic

## Letter 3

## Cont'd

Signatures in Global and National Commerce Act (E-Sign Act), 15, U.S.C. $\S \S 7001$ to 7006 or Uniform Electronic Transactions Act of any state or the federal government unless a specific statement to the contrary is included in this e-mail.

## Letter 3 <br> Cont'd

## Tribal Cultural Resource - Awareness Training - Mitigation Measure


#### Abstract

A consultant and construction worker tribal cultural resources awareness brochure and training program for all personnel involved in project implementation will be developed in coordination with interested Native American Tribes. The brochure will be distributed and the training will be conducted in coordination with qualified cultural resources specialists and Native American Representatives and Monitors from culturally affiliated Native American Tribes before any stages of project implementation and construction activities begin on the project site. The program will include relevant information regarding sensitive tribal cultural resources, including applicable regulations, protocols for avoidance, and consequences of violating State laws and regulations. The worker cultural resources awareness program will also describe appropriate avoidance and minimization measures for resources that have the potential to be located on the project site and will outline what to do and whom to contact if any potential archaeological resources or artifacts are encountered. The program will also underscore the requirement for confidentiality and culturally-appropriate treatment of any find of significance to Native Americans and behaviors, consistent with Native American Tribal values.


## Letter 3: Cherilyn Neider, United Auburn Indian Community

## Response to Comment 3-1

The comment is an introductory statement and does not address the adequacy of the Draft EIR.

## Response to Comment 3-2

The referenced notification letter was distributed to the United Auburn Indian Community (UAIC) by Placer County on July 15, 2016. In response to the commenter's request, Placer County resubmitted a copy of the original notification letter to the UAIC on February 6, 2019. It should be noted that consultation was confirmed to be "not requested" per a meeting between the UAIC and the County on October 12, 2017.

## Response to Comment 3-3

The Draft EIR includes Mitigation Measures V-1 and V-2, which provide for protection of any previously undiscovered cultural resources, including tribal cultural resources, that may be uncovered during ground-disturbing activities associated with the proposed project. Given that the existing mitigation measures provide sufficient protections for tribal cultural resources, the commenter's suggested mitigation will not be incorporated into the EIR. However, the project applicant has expressed that they would be willing to distribute a training brochure provided by UAIC to workers on the project site and/or allow a representative from the UAIC to provide cultural resources awareness training for workers on the project site prior to the initiation of site preparation/grading activities, at the tribe's expense.

## Letter 4



## CULTURAL RESOURCES

February 6, 2019
Placer County Community Development Resource Agency, Environmental Coordination Services 3091 County Center Drive, Suite 190
Auburn, CA 95603

## RE: Draft EIR, Quarry Ridge Office Park

Dear To Whom It May Concern,

## 4-1

Thank you for your letter dated January 22, 2019 in regard to the above mentioned project. Based on the information provided, the Shingle Springs Band Of Miwok Indians is not aware of any known cultural resources on this site. However, SSR would like to have continued consultation through updates, as the project progresses. This will foster a greater communication between the Tribe and your agency.

> SSR would also like to request any and all completed record searches and or surveys that were done in or around the project area up to and including environmental, archaeological and cultural reports. If during the progress of the project new information or human remains are found, we would like to be able to go over our process with you to protect such important and sacred artifacts (especially near rivers and streams).
> If such finds are made, please contact Kara Perry, Cultural Outreach Coordinator, at (530) 488-4049 or kperry@ssband.org.
> Thank you for providing us with this notice and opportunity to comment.


Cultural Resource Director
Tribal Historic Preservation Officer (THPO)
Most Likely Descendant (MLD)

## Letter 4: Daniel Fonseca, Shingle Springs Band of Miwok Indians

## Response to Comment 4-1

The comment does not address the adequacy of the Draft EIR, but rather requests continued consultation through updates, as the project progresses. The Placer County Community Development Resource Agency will continue to notify the tribe regarding the progress of the proposed project, including the upcoming public hearings.

## Response to Comment 4-2

On October 26, 2017, Placer County provided a copy of the Cultural and Paleontological Resources Inventory prepared for the proposed project to the Shingle Springs Band of Miwok Indians. Subsequently, the tribe has not requested any additional information.

Shirlee Herrington
Environmental Coordination Services
Placer County Community Development Resource Agency
3091 County Center Drive, Suite 190
Auburn, CA 95603
sherring@placer.ca.gov
Re: Quarry Ridge Office Park PLNN16-00157

The following comments are in response to the DEIR on the above project:
On June 3, 2016, the Granite Bay Community Association in response to the Initial Project Application, noted that the Granite Bay Community Plan discouraged two story buildings on Douglas. However, applicant stated that the western most building of the project necessitated two stories, in order to obtain the square footage needed for the building footprint without removing the existing oak trees. The letter noted that was acceptable to save the trees, but the second story should be conditioned that if the trees are removed, the second story is no longer approved.

The letter also noted that Berg Street is rural from Douglas north. Instead of urban curb, gutter, and sidewalk as proposed in DEIR, a treatment similar to the attractive pedestrian walkway on the west side of Berg along the Grove development extending from Macargo to Olive Ranch Road would better fit the rural character of the road. It is a meandering trail set back from the roadway and bordered by low maintenance landscaped areas.

In light of all the business/professional development approved and projected for the concentrated area of Berg and Douglas, serious consideration should be given to the environmentally superior Reduced Intensity Alternative in order to lessen the impacts of this development and the several others approved or proposed.

The landscaped median on Douglas Boulevard enhances the rural atmosphere of Granite Bay and is important to the community. Every project proposed on Douglas Is looking to lessen this median to provide longer turn pockets. This is unacceptable to the community. Other alternatives need to be considered. Perhaps a reduced speed zone posted in that business area? Douglas after crossing Sierra College into Roseville drops to 40 mph in that business area.

The parcel is elevated above the roadway and borders residential. Outdoor lighting should be at a minimum in off business hours. Perhaps motion sensitive lighting that would come on when activated for pedestrian safety. (The Quarry Ponds buildings to south are outlined in white lights which may be in violation of the Conditions of Approval.)


#### Abstract

A closing observation -- As always, outside traffic using the Douglas corridor is a major concern of the community. In addition, the DEIR notes 33 pending and approved projects in Granite Bay that would generate approximately 11,360 more daily trips. Widening roads and installing traffic signals in Granite Bay doesn't address the problem. Auburn Folsom was widened to 4 lanes and more commuters use it than before because it speeded up commute times. That doesn't fix the traffic problems in Granite Bay, it just encourages more outside traffic.


5-6


Sandra H. Harris, Secretary

## Letter 5: Sandra H. Harris, Granite Bay Community Association

## Response to Comment 5-1

The comment does not address the adequacy of the Draft EIR. As discussed on page 25 of the Initial Study prepared for the proposed project, of the 29 existing on-site trees, 10 trees have been recommended for removal due to defects, compromised health, and/or structural stability noted at the time of a field inventory of the project site conducted by Sierra Nevada Arborists on August 17,2015 . Fifteen of the trees would be preserved. Only two healthy trees would require removal as part of the proposed project, neither of which are located within the western portion of the site.

Only one of the proposed office buildings (Building 1) would include two stories. The building would be situated at an angle so as to avoid existing trees near the building footprint. Without the second story, the building would be too small to meet the space requirements identified by the project applicant for this general office building. Furthermore, residents of the existing residential homes to the north of the project site have expressed general support for the proposed second floor on Building 1, provided that the north side of the second-floor deck/patio is screened to protect the privacy of such residents. Such screening elements have been incorporated into the design of the proposed project.

## Response to Comment 5-2

The commenter requests different pedestrian treatments along the proposed project's Berg Street frontage and does not address the adequacy of the Draft EIR. The commenter's suggestions related to sidewalk improvements have been forwarded to the decision-makers for their consideration.

## Response to Comment 5-3

The comment suggests approval of the Reduced Intensity Alternative, but does not address the adequacy of the Draft EIR. The comment has been forwarded to the decision-makers for their consideration.

## Response to Comment 5-4

The comment is assumed to reference Mitigation Measure 5-6 in the Draft EIR, which requires increasing the length of the existing left-turn lane approaching Berg Street (eastbound) and the existing left-turn lane approaching Granite Estates Drive (westbound) along Douglas Boulevard.

In Preserve Poway v. City of Poway (2016) 245 Cal.App.4th 560, the Appellate Court evaluated whether community character is a consideration in CEQA and whether changes to community character or social impacts constitute an environmental impact under CEQA. The Court determined CEQA does not require an analysis of subjective psychological feelings or social impacts. Rather, CEQA's overriding and primary goal is to protect the physical environment. CEQA defines a "significant effect on the environment" as "substantial, or potentially substantial, adverse changes in physical conditions ...." (PRC section 21100. subd. (d)). Thus, the commenter's
concern about changes to the rural feel of the project area is not a CEQA issue. Nonetheless, the commenter's suggestions have been forwarded to the decision-makers for their consideration.

## Response to Comment 5-5

Mitigation Measure I-1, as included in the Initial Study prepared for the proposed project, requires the following related to on-site lighting:

MM I-1: $\quad$ Concurrent with submittal of Improvement Plans, a detailed lighting and photometric plan shall be submitted to the DRC for review and approval. The lighting and photometric plan shall include the following provisions:

- Parking lot lighting shall be accomplished with pole mounted decorative LED luminaries. The parking lot shall be illuminated by using 14-foot decorative post-top type LED fixtures mounted on metal poles. The pole color shall be such that the pole will blend into the landscape (i.e., black, bronze, or dark bronze). Such luminaires shall also be provided with house side shields to minimize light pollution to the areas outside of the property line.
- The parking lot lighting shall be photocell controlled to provide automatic light reduction by a minimum of 50 percent between the hours of 11 PM and 6 AM. The site lighting shall be dimmed to lower level automatically.
- Landscape lighting may be used to visually accentuate and highlight ornamental shrubs and trees adjacent to buildings and in open spaces. Lighting intensity will be of a level that only highlights shrubs and trees and will not impose glare on any pedestrian or vehicular traffic.
- Architectural lighting shall articulate and animate the particular building design and visibly promote and reinforce pedestrian movement. Indirect wall lighting or "wall washing" and interior illumination (glow) is encouraged in the expression of the building.
- Wall-mounted light fixtures will be permitted only if they have a 90 degree cut off to prevent glare.
- No lighting is permitted on top of structures.
- Pedestrian routes should utilize bollard type lighting rather than pole lights and should be integrated into building and landscape design. Pedestrian-scale light fixtures shall be durable and vandal resistant.

With implementation of Mitigation Measure I-1, impacts related to creation of new sources of substantial light and glare that would adversely affect day or nighttime views in the area were appropriately determined to be less-than-significant. The mitigation measure requires reduced lighting at night as requested by the comment.

## Response to Comment 5-6

The comment does not address the adequacy of the Draft EIR. The commenter's concerns are noted, and have been forwarded to the decision-makers for their consideration.

## Shirlee Herrington

| From: | Larissa Berry [Izberry@peoplepc.com](mailto:Izberry@peoplepc.com) |
| :--- | :--- |
| Sent: | Wednesday, March 06, 2019 8:18 AM |
| To: | Shirlee Herrington |
| Cc: | defendgb@gmail.com; GBCA; AEL-Leslie Warren |
| Subject: | Re: Quarry Ridge Professional Office Park (PLN16-00157), Draft Environmental Impact |
|  | Report Released |

Good morning Ms. Herrington,
Could you please see that my comments are included as part of the Administrative record.

Thank you
Larissa Berry

Planning Commissioners,

Please accept my comments on the Quarry Ridge Office Park DEIR as part of the administrative record. I will preface my comments by stating that the applicant has worked closely with the immediately adjacent and contiguous parcels to achieve a project acceptable to all. Interactions of this nature should be encouraged and commended by this Commission. The DEIR is also a reasonable length which is not true for a number of massive documents recently dumped on the public in a relatively short period of time in direct conflict with the intent of CEQA to clearly expose impacts and actively seek public participation.

Comments:

The entitlement requested for "Granite Bay Community Plan text amendment to modify the setback standard for buildings located on the north side of Douglas Boulevard" has not been evaluated for impacts on the Aesthetics of the Community Plan identified Scenic Corridor. Adoption and amendment of a General Plan is a "project" under CEQA and therefore, environmental review must be performed. City of Santa Ana v City of Garden Grove (1979) 100 CA3d 521. Adopting or amending a general plan must be done so in accordance with Government Code section 35350 et seq.
"Right-of-Way. All development on the north side of Douglas west of Auburn-Folsom Road shall be required to dedicate 70 feet of right-of-way as measured from centerline. Building setbacks from the edge of the road right-ofway shall be a minimum of 75 feet. For discretionary permits, a setback of less than 75 feet as otherwise required by the Community Plan may be approved by the Decision-making Body as long as a visual buffer is in place that provides for one or more of the following: 1. Landscaping, building architectural design or other buffer techniques have been incorporated into the project to reduce visual impacts of the project when viewed from the Douglas Boulevard right-of-way; 2. A setback of less than 75 feet would result in increased setbacks from either adjacent properties or on-site resources and/or conditions, which, on balance, result in better overall site planning and design...... on a case-by-case basis ....."

## Letter 6 <br> cont'd

Zoning ordinance must give enough guidance to provide clear context for planning decisions and approvals with regards
to zoning regulations and permits. The lack of a minimum setback negates any clear context. Trying to claim an
exemption under CEQA will also fail under Save Our Big Trees v City of Santa Cruz, (2015) 241. For an exemption, the zoning text amendment must be more, not less restrictive.

This Planning Commission recently found a 1.3 acre, rectangular, flat parcel with no topographic limitations to be disadvantaged. Entitling a set-back variance on Douglas. The DEIR should clarify why a parcel with a 20 -foot slope differential requiring multiple levels of retaining walls is not disadvantaged; negating the need to re-write the Granite Bay Community Plan.

Respectfully,

Larissa Berry
-----Original Message-----
From: Shirlee Herrington
Sent: Jan 22, 2019 4:07 PM
To:
Subject: Quarry Ridge Professional Office Park (PLN16-00157), Draft Environmental Impact Report Released

Good Afternoon:
The Draft EIR prepared for the subject project is now available on the County's website for public review and can be accessed at this LINK

The 45-day public comment period starts on 01-22-09 and ends on 03-07-19 with a public hearing scheduled on 02-14-19 to receive comments. Attached is the Notice of Availability for your reference.

If you will have comments on the DEIR, please send them to my attention at cdraecs@placer.ca.gov or at the mailing address below.

Jhank you,
Shirlee
Shirlee I. Herrington
Environmental Coordination Services
Placer County Community Development Resource Agency
3091 County Center Drive, Suite \#190
Auburn, CA 95603
530-745-3132
sherring@placer.ca.gov


## LETTER 6: LARISSA BERRY

## Response to Comment 6-1

The comment does not address the adequacy of the Draft EIR. The commenter's other statements are noted and have been forwarded to the decision-makers for their consideration.

## Response to Comment 6-2

As noted on page 3-13 of the Draft EIR, the Community Design Element of the Granite Bay Community Plan (GBCP), Section 4.2.11, Road Corridors, requires a 75 -foot building setback along the north side of Douglas Boulevard. As noted by the commenter, the proposed project entitlements include a request to amend this language to enable a building setback of less than 75 feet, for discretionary permits, for approval by the decision-making body, as long as a visual buffer is in place that provides for one or more of the following:

1. Landscaping, building architectural design or other buffer techniques have been incorporated into the project to reduce visual impacts of the project when viewed from the Douglas Boulevard right-of-way;
2. A setback of less than 75 feet would result in increased setbacks from either adjacent properties or on-site resources and/or conditions, which, on balance, result in better overall site planning and design.

The proposed additions were carefully drafted so as to include language akin to performance standards, which are often included in program-level mitigation measures designed to ensure that future projects associated with the program comply with the performance standards and thus avoid environmental impacts (CEQA Guidelines Section 15126.4(a)(1)(B)). A mitigation performance standard is sufficient if it identifies the criteria the agency will apply in determining that the impact will be mitigated. Here, performance standards are added to the setback policy to ensure that a visual buffer is required for each project along the north side of Douglas Boulevard.

The added flexibility that would be provided with the proposed amendment to the building setback standard is also consistent with the Community Design Element of the GBCP, wherein it is stated (GBCP, Community Design, pg. 41):

> Design objectives and principals [sic] form an integral part of the County's land use planning and decision-making processes to achieve the goal of high quality and sustainable physical environments. As guidelines, these recommendations will not regulate with the same rigidity as an ordinance. Rather, it will indicate the County's intent regarding the various components of design. The existing development pattern and natural features of Granite Bay will require a measure of flexibility in the design review process for new development and redevelopment/revitalization projects.

It is instructive that this portion of the GBCP notes that "As guidelines, these recommendations will not regulate with the same rigidity as an ordinance." The proposed amendments to the 75 -foot setback standard reflect the GBCP's acknowledgement that the existing development pattern and
natural features of Granite Bay will require a measure of flexibility in the design review process for new development.

## Response to Comment 6-3

The comment is not entirely clear. The subject amendment is not related to the Zoning Ordinance, but rather the GBCP. No exemption is being sought for the proposed amendment to the GBCP 75foot building setback standard. Rather, the proposed amendment is included in the Draft EIR and evaluated at the appropriate level of detail (see pages 1-11 and 1-12, 3-13, and 3-15 of the Draft EIR). For the reasons set forth in Response to Comment 6-2, a minimum building setback distance is not necessary given the performance standards included in the proposed amendment language. It is also noted that the Zoning Ordinance building setbacks would still apply to each project along the north side of Douglas Boulevard.

## Response to Comment 6-4

Variances may be granted for Zoning Ordinance standards, but not for General Plan/GBCP policy standards. The 75 -foot setback identified in the Community Design Element of the GBCP, Section 4.2.11, Road Corridors, is a standard, rather than a regulation required by an ordinance. As such, relief (i.e., variance) from a development standard cannot be granted, even when conditions warrant such relief (e.g., irregularly shaped parcel and/or slopes greater than 20 percent). Thus, the proposed project is requesting to add language through an amendment to the GBCP, not a variance.

As noted in Response to Comment 6-3 above, the proposed project would be consistent with the minimum setback standards established for the Office and Professional (OP) zoning designation per Section 17.32.010(D) of the Placer County Code. Thus, a zoning variance would not be required for the project.

## Letter 7

## Shirlee Herrington

| From: | Shannon Quinn [shannoncts@gmailcom](mailto:shannoncts@gmailcom) |
| :--- | :--- |
| Sent: | Wednesday, March 06, 2019 3:25 PM |
| To: | Placer County Environmental Coordination Services; Shirlee Herrington |
| Subject: | Quarry Ridge Professional Office Park (PLN16-00157), Draft Environmental Impact |
|  | Report Comments |

Shirlee,
Please add these comments to the official record for Quarry Ridge Professional Office Park (PLN16-
00157), Draft Environmental Impact Report. While I am in complete support of this project, I believe the following items need clarity in the Draft EIR:

1. This project should seek a right-of-way variance if needed, not a Granite Bay Community Plan

Amendment. This attempt fails to provide the public an adequate review of the associated impacts of this amendment as required by CEQA. Other options exist and should be utilized which are far less impactful.
2. The Sierra College Blvd/Douglas Blvd intersection review utilizes an incorrect threshold level. This intersection falls under the jurisdiction of Roseville and therefore their significance threshold should be employed for analysis of impacts. This project incorrectly places it as a LOS E when the threshold is actually LOS C. As further evidence that this should be the standard, this is also referenced in the traffic study prepared for Whitehawk I \& II, by Fehr \& Peers. This should be corrected in the Final EIR and evaluated for cumulative impacts. It appears that under EPAP plus project verse just EPAP there is an increase in delay of 8.5 (sec/veh) which would appear considerable for an intersection operating below standard.
3. Douglas Blvd (from Sierra College to Cavitt Stallman) roadway segment study is incorrectly identified as a 4 lane arterial- High Access Control and then later under cumulative conditions is switched to a 4 lane arterial MAC without explanation- in addition the actual V/C should be reported not just the LOS classification as shown in Table 4. Further discussion as to why Douglas Boulevard was classified as an HAC verse MAC to begin with should occur-it would appear that the number of interruptions to traffic from intersections and driveways play a major role in determining control classification and was not properly evaluated. Again, this is important so that the public is able to adequately assess the impacts, especially when looking across multiple projects and trying to understand cumulative conditions.

Douglas Blvd (Sierra College to Cavitt)-
4 Lane HAC Arterial $=1.19$ V/C LOS F
4 Lane MAC Arterial $=1.32 \mathrm{~V} / \mathrm{C}$ LOS F
Thank you for your consideration.
Sincerely,
Shannon Quinn

## Letter 7: Shannon Quinn

## Response to Comment 7-1

The comment is an introductory statement expressing support for the project. Specific concerns raised by the commenter are addressed in the responses below.

## Response to Comment 7-2

Please see Responses to Comments 6-2 and 6-4 above.

## Response to Comment 7-3

The LOS E minimum operations standard noted for the Douglas Boulevard/Sierra College Boulevard intersection in the Quarry Ridge Draft EIR is appropriate, as the intersection is located within Placer County and is under the County's jurisdiction. Thus, associated revisions to the Quarry Ridge Draft EIR are not necessary. An erratum to the Whitehawk I and II Project's Final EIR was issued by the County to clarify and make the necessary revisions to the traffic section related to the LOS E standard for the Douglas Boulevard/Sierra College Boulevard intersection.

## Response to Comment 7-4

In response to the comment, Tables 5-4, 5-9, 5-11, and 5-13 from Chapter 5, Transportation and Circulation, of the Draft EIR are hereby revised as shown on the following pages. In addition, the Traffic Impact Analysis prepared for the proposed project has been revised similarly and is included as Appendix A to this Final EIR.

The classification of Douglas Boulevard between Sierra College Boulevard and Cavitt Stallman Road has been changed to "Arterial - Moderate access control" to reflect the spacing of the signalized intersections, presence of commercial driveways along the roadway segment and to be consistent with the assumptions used for the Whitehawk I and II Projects EIR. The LOS identified for the roadway would remain at LOS F under all scenarios evaluated in the Draft EIR, with and without the addition of traffic from the proposed project. The project's impact is determined based on Placer County's Impact Analysis Methodology of Assessment memorandum. This memorandum states that the project would trigger a significant roadway segment impact if the project increases the volume-to-capacity ratio by 0.05 or adds 100 ADT or more per lane. Because the project's incremental increase in V/C is, at most, 0.009 , considering all scenarios, and the project is forecasted to add, at most, 80 ADT per lane to this segment, considering all scenarios, the project's impacts would remain less than significant for the identified segment. Thus, the forgoing revisions do not alter the conclusions presented in the Draft EIR.

| Table 5-1Study Roadway Segment LOS - Existing Condition |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Roadway | Segment | Classification | Lanes | ADT | LOS |
| Douglas Blvd | Sierra College Blvd to Cavitt Stallman Rd | Arterial HighModerate | 4 to 6 | 47,570 | F |
|  | Cavitt Stallman Rd to Seeno Ave | Arterial High | 4 | 46,830 | F |
|  | Seeno Ave to Barton Rd | Arterial High | 4 | 44,800 | F |
|  | Barton Rd to Auburn-Folsom Rd | Arterial High | 4 | 42,630 | F |
| Berg St | Olive Ranch Rd to Douglas Blvd | Arterial Low | 2 | 1,200 | A |
| Source: KD Anderson \& Associates, Inc., 2018. |  |  |  |  |  |


| Table 5-9 <br> Study Roadway Segment LOS - Existing Plus Project Condition |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Roadway | Segment | Classification | Lanes | Existing |  | Existing Plus Project |  |  |  |
|  |  |  |  |  |  |  |  |  |  |
|  |  |  |  | ADT | LOS | Project Only | Total | LOS | Change in $V / C$ |
| Douglas <br> Blvd | Sierra College Blvd to Cavitt Stallman Rd | Arterial HighModerate | 4 | 47,570 | F | 320 | 47,890 | F | $0.008 \underline{\underline{9}}$ |
|  | Cavitt Stallman Rd to Seeno Ave | Arterial High | 4 | 46,830 | F | 320 | 47,150 | F | 0.008 |
|  | Seeno Ave to Barton Rd | Arterial High | 4 | 44,800 | F | 340 | 45,140 | F | 0.009 |
|  | Berg St to Barton Rd | Arterial High | 4 | 44,800 | F | 190 | 44,990 | F | 0.005 |
|  | Barton Rd to Auburn-Folsom Rd | Arterial High | 4 | 42,630 | F | 110 | 42,740 | F | 0.003 |
| Berg St | Olive Ranch Rd to Project | Arterial Low | 2 | 1,200 | A | 40 | 1,240 | A | 0.003 |
|  | Project to Douglas Blvd | Arterial Low | 2 | 1,200 | A | 530 | 1,730 | A | 0.035 |
| Note: Bold indicates applicable LOS threshold exceeded. <br> Source: KD Anderson \& Associates, Inc., 2018. |  |  |  |  |  |  |  |  |  |


| Table 5-11Study Roadway Segment LOS - EPAP Plus Project Condition |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Roadway | Segment | Classification | Lanes | EPAP |  | EPAP Plus Project |  |  |  |
|  |  |  |  | ADT | LOS | ADT |  | LOS | Change in V/C |
|  |  |  |  |  |  | Project Only | Total |  |  |
| Douglas Blvd | Sierra College Blvd to Cavitt Stallman Rd | Arterial HighModerate | 4 to 6 | 51,320 | F | 320 | 51,640 | F | $0.008 \underline{\underline{9}}$ |
|  | Cavitt Stallman Rd to Seeno Ave | Arterial High | 4 | 50,160 | F | 320 | 50,480 | F | 0.008 |
|  | Seeno Ave to Barton Rd | Arterial High | 4 | 47,610 | F | 340 | 47,950 | F | 0.009 |
|  | Berg St to Barton Rd | Arterial High | 4 | 45,480 | F | 190 | 45,670 | F | 0.005 |
|  | Barton Rd to Auburn-Folsom Rd | Arterial High | 4 | 44,690 | F | 110 | 44,800 | F | 0.003 |
| Berg St | Olive Ranch Rd to Project | Arterial Low | 2 | 1,460 | A | 40 | 1,500 | A | 0.003 |
|  | Project to Douglas Blvd | Arterial Low | 2 | 1,990 | A | 530 | 2,520 | A | 0.035 |
| Note: Bold indicates applicable LOS threshold exceeded. <br> Source: KD Anderson \& Associates, Inc., 2018. |  |  |  |  |  |  |  |  |  |


| Table 5-13 <br> Study Roadway Segment LOS - Cumulative Plus Project Condition |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Cumulative No Project |  |  | Cumulative No Project |  | Cumulative Plus Project |  |  |  |
|  |  |  |  |  |  | AD |  |  | Change in V/C |
| Roadway | Segment | Classification | Lanes | ADT | LOS | Project Only | Total | LOS |  |
| Douglas Blvd | Sierra College Blvd to Cavitt Stallman Rd | Arterial Moderate | -4-6 | 54,380 | F | $323 \underline{\underline{0}}$ | 54,700 | F | 0.008 相 |
|  | Cavitt Stallman Rd to Woodgrove Way | Arterial High | 4 | 51,980 | F | 323 0 | 52,300 | F | 0.008 |
|  | Woodgrove Way to Seeno Ave | Arterial High | 4 | 50,510 | F | 340 | 50,850 | F | 0.009 |
|  | Seeno Ave to Barton Rd | Arterial High | 4 | 50,160 | F | 340 | 50,500 | F | 0.009 |
|  | Berg St to Barton Rd | Arterial High | 4 | 47,560 | F | $1889 \underline{\underline{0}}$ | 47,750 | F | 0.005 |
|  | Barton Rd to AuburnFolsom Rd | Arterial High | 4 | 48,340 | F | 1120 | 48,450 | F | 0.003 |
| Berg St | Olive Ranch Rd to Project | Arterial Low | 2 | 1,460 | A | 40 | 1,500 | A | 0.003 |
|  | Project to Douglas Blvd | Arterial Low | 2 | 1,420 | A | 52830 | 1,950 | A | 0.035 |
| Note: Bold indicates applicable LOS threshold exceeded.Source: KD Anderson \& Associates, Inc., 2018. |  |  |  |  |  |  |  |  |  |

## Letter 8

## Shirlee Herrington

| From: | hollyjesq@aol.com |
| :--- | :--- |
| Sent: | Thursday, March 07, 2019 11:14 AM |
| To: | Placer County Environmental Coordination Services |
| Subject: | Comments on Quarry Ridge Office Park, Draft Environmental Impact Report |

## To Whom It May Concern:

Please ensure that my comments are included in the administrative record on this matter.

## 8-1

The request to modify the setback standard for the buildings located on the North side of Douglas Boulevard have not been fully evaluated, including, but not limited to, impacts to the Aesthetics and affect on the Scenic Corridor. This is just one of several projects that will be affecting Douglas Boulevard, and the singular as well as cumulative affects have not been evaluated. There are also proposed projects on Douglas Boulevard that will affect not only the Scenic aspect of Douglas Boulevard, but also traffic, sewer, etc. There has additionally been a proposal to increase sewer user fees, and it are seeking to increase usage, one of which would be this proposal.

If the requested setback standard modifies the Community or Granite Bay Plan, then it is a "project" under the California Environmental Quality Act ("CEQA") and, therefore, environmental review must be performed. City of Santa Ana v City of Garden Grove (1979) 100 CA3d 521. Adopting or amending a general plan must be done so in accordance with Government Code section 35350 et seq.
"Right-of-Way. All development on the north side of Douglas west of Auburn-Folsom Road shall be required to dedicate 70 feet of right-of-way as measured from centerline. Building setbacks from the edge of the road right-ofway shall be a minimum of 75 feet. For discretionary permits, a setback of less than 75 feet as otherwise required by the Community Plan may be approved by the Decision-making Body as long as a visual buffer is in place that provides for one or more of the following: 1. Landscaping, building architectural design or other buffer techniques have been incorporated into the project to reduce visual impacts of the project when viewed from the Douglas Boulevard right-of-way; 2. A setback of less than 75 feet would result in increased setbacks from either adjacent properties or on-site resources and/or conditions, which, on balance, result in better overall site planning and design...... on a case-by-case basis ....."

The amendment is less restrictive, not more, and does not qualify for an exemption under CEQA. (See, Save Our Big Trees v City of Santa Cruz, (2015) 241.)

Please do not allow a reduction in any setback, require that there be the requisite setback on Douglas Boulevard and do not negatively affect the scenic aspect of Douglas Boulevard by approving this draft environmental impact report (DEIR), without modifying to require the requisite amount per the plan and law.

Thank you in advance for your consideration.
Holly Johnson

## Letter 8: Holly Johnson

## Response to Comment 8-1

Please see Response to Comment 6-2.

## Response to Comment 8-2

As discussed on page 58 of the Initial Study prepared for the proposed project, per Section 13.12.270 of the Placer County Code, the project applicant would be required to pay a sewer connection fee to the County prior to connection to the County's existing conveyance system. The County's sewer connection fees are distributed to both Placer County and the City of Roseville for ongoing and future upgrades to the Dry Creek Wastewater Treatment Plant. In addition, the fees are used to help offset additional demands on conveyance infrastructure created by new connections. According to CEQA Section 15130(a)(3), paying a "fair share fee" is permissible as effective mitigation for cumulative impacts if the fees are part of a reasonable plan of actual mitigation that the relevant agency commits itself to implementing. The Placer County Board of Supervisors has determined that a development impact fee is needed in order to finance public improvements to wastewater infrastructure and to pay for the development's fair share of the construction costs of these improvements.

The County has calculated the sewer connection fees for Building 1 of the project to be approximately $\$ 17,000$. Additional connection fees will be paid by the applicant, on an equivalent dwelling unit basis, prior to issuance of building permits for each building. Furthermore, the Placer County Public Works Department has issued a letter (dated March 10, 2016) stating that the Placer County Sewer Maintenance District would be capable of serving the project pending fulfillment of the District's requirements, including payment of fees, compliance with applicable San Juan Water District ordinances and requirements, and other standard conditions. ${ }^{1}$ As such, the proposed project would not result in a cumulatively considerable contribution to sewer capacity impacts associated with cumulative development in the project area.

Chapter 5, Transportation and Circulation, of the Draft EIR includes an analysis of cumulative traffic impacts, including cumulative development in Granite Bay. As discussed under Impacts 58 and 5-9 within the Draft EIR, the project's incremental contribution to cumulative impacts to study intersections and roadway segments under the Cumulative Plus Project Condition would not be cumulatively considerable. In addition, as noted under Response to Comment 1-1 above, Mitigation Measure 5-8 from the Draft EIR would require the project applicant to pay traffic impact mitigation fees that would be used to fund necessary roadway improvements included in the County's CIP. Thus, the project would provide for a fair-share contribution to necessary roadway improvements in the project area.

[^0]
## Response to Comment 8-3

Please see Response to Comment 6-2.

## Quarry Ridge Draft EIR <br> Public Comment Meeting Summary

Letter 9

| Date: | February 14, 2019 |
| :--- | :--- |
| Time: | 1:30 PM |
| Location: | Placer County Community Development Resource Center |
|  | Planning Commission Hearing Room |
|  | 3091 County Center Drive, |
|  | Auburn, CA 95603 |

## I. Verbal Comments (arranged in order of "appearance" of commenter):

Public Comments:
None.

## Planning Commission Comments:

- Commissioner Wayne Nader
o Commissioner Nader questioned whether a traffic signal was considered at the
intersection of Berg Street and Douglas Boulevard.
- Commissioner Richard Johnson

9-2
o Commissioner Johnson noted that the distance between traffic signals along Douglas helps meter the traffic along Douglas, including at the Berg Street and Douglas Boulevard intersection.
$\qquad$

- Commissioner Sam Cannon

9-3
o Commissioner Cannon questions the security gate access to the parking lot, specifically why and when the gate would be closed.

## Letter 9: Public Comment Meeting

## Response to Comment 9-1

The Placer County Engineering and Surveying Division has indicated that installation of a traffic signal at the Douglas Boulevard/Berg Street intersection is not supported by the Granite Bay community. Such is evidenced on page 113 of the Circulation Element of the GBCP, Policy 9.1.21, which states the following:

The community's desire to retain the character of the Country Roadways and the design guidelines for Country Roadways shall be earnestly considered when designing improvements to arterial or collector roads designated as Country Roadways. The County shall strive for a balance between local community desires and engineering solutions and shall present proposed designs to the community for review prior to approval. Upgrades made to minor arterial and collector roads designated as Country Roadways should be limited to critical safety issues and sufficient shoulder for cyclists and pedestrians.

With regard to future signal improvement projects at the intersections of Douglas Boulevard/Berg Street and Douglas Boulevard/Quail Oaks Drive, as well as Auburn Folsom Road/Cavitt-Stallman Road, Footnote 3 of Table 9.6.3 in the Circulation Element of the GBCP states the following:

It is the desire of the community to avoid these three signal projects. They should be implemented only to correct identified safety or traffic operational problems and only after other measures have been explored and either implemented or rejected. The signals may be necessary as a result of approval of specific land development projects.

In addition, the Douglas Boulevard/Berg Street intersection operates acceptably with the addition of Quarry Ridge traffic under all traffic scenarios evaluated in the EIR (Tables 5-8, 5-10, and 512).

## Response to Comment 9-2

The comment does not address the adequacy of the Draft EIR.

## Response to Comment 9-3

As noted on page 3-5 of the Draft EIR, the proposed security gate would be open during normal business hours and closed with authorized access only during non-business hours. Per the project applicant, the security gate is intended to prevent trespass onto the project site after hours when the proposed offices are closed. Given that views of the proposed parking area from Douglas Boulevard would be obscured by the proposed buildings and landscaping elements, provision of a gated access was deemed necessary to alleviate potential security concerns.

## 3. REVISIONS TO THE DRAFT EIR TEXT



### 3.1 INTRODUCTION

The Revisions to the Draft EIR Text chapter presents minor corrections, additions, and revisions made to the Draft EIR initiated by the Lead Agency (Placer County) based on comments received during the public review period by reviewing agencies and/or the public.

The changes represent minor clarifications/amplifications of the analysis contained in the Draft EIR and do not constitute significant new information that, in accordance with CEQA Guidelines, Section 15088.5, would trigger the need to recirculate portions or all of the Draft EIR.

### 3.2 Description of Changes

New text is double underlined and deleted text is struck through. Text changes are presented in the page order in which they appear in the Draft EIR.

## 1 Introduction

As a staff-initiated change, footnote 2 on page 1-4 of the Draft EIR is hereby revised as follows:
1 Note: While the Transportation Section of the Appendix G Checklist has been updated consistent with Senate Bill 743, deleting reference to level of service, and instead inserting a reference to new Guidelines Section 16054.3, subdivision (b), to focus on vehicle miles traveled where appropriate, this shift in focus on vehicle miles traveled is not required until Jantary July 1, 2020.

The forgoing revision is for clarification purposes and does not affect the adequacy of the Draft EIR.

## 2. Executive Summary

For clarification purposes, Table 2-1 in Chapter 2, Executive Summary, of the Draft EIR is hereby revised to reflect minor revisions made to mitigation measures as part of this Final EIR, as presented throughout this chapter. Rather than include the entirety of Table 2-1 with revisions shown where appropriate, only the impacts for which mitigation has been revised or added are presented in this chapter. The revisions to Table 2-1 are for clarification purposes only and do not change the conclusions of the Draft EIR. Please refer to the end of this chapter for Table 2-1.

## 4 Noise

In response to a staff-initiated change, Mitigation Measure 4-3(a) on page 4-24 of the Draft EIR is hereby revised as follows:

Mitigation Measure(s)
Implementation of the following mitigation measures would reduce the above impact to a less-than-significant level.

4-3(a) A Blasting Plan for construction shall be prepared and submitted to the County Planning Services Division at least ten (10) days prior to initiation of construction activities. The plan shall include the following:

The forgoing revision is for clarification purposes and does not affect the adequacy of the Draft EIR.

## 5 Transportation and Circulation

Tables 5-4, 5-9, 5-11, and 5-13 from Chapter 5, Transportation and Circulation, of the Draft EIR are hereby revised as shown on the following pages. As discussed under Response to Comment 74 in Chapter 2.0 of this EIR, the revisions do not alter the conclusions presented in the Draft EIR.

## Other

All references in the EIR to the Placer County Department of Public Works and Facilities (DPWF) are hereby revised to instead reference the Department of Public Works (DPW). These changes have been made simply to reflect recent name changes to County departments.

| Table 5-4Study Roadway Segment LOS - Existing Condition |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Roadway | Segment | Classification | Lanes | ADT | LOS |
| Douglas Blvd | Sierra College Blvd to Cavitt Stallman Rd | Arterial HighModerate | 406 | 47,570 | F |
|  | Cavitt Stallman Rd to Seeno Ave | Arterial High | 4 | 46,830 | F |
|  | Seeno Ave to Barton Rd | Arterial High | 4 | 44,800 | F |
|  | Barton Rd to Auburn-Folsom Rd | Arterial High | 4 | 42,630 | F |
| Berg St | Olive Ranch Rd to Douglas Blvd | Arterial Low | 2 | 1,200 | A |
| Source: KD Anderson \& Associates, Inc., 2018. |  |  |  |  |  |


| Table 5-9 <br> Study Roadway Segment LOS - Existing Plus Project Condition |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Roadway | Segment | Classification | Lanes | Existing |  | Existing Plus Project |  |  |  |
|  |  |  |  |  |  |  |  |  |  |
|  |  |  |  | ADT | LOS | Project Only | Total | LOS | Change in $V / C$ |
| Douglas <br> Blvd | Sierra College Blvd to Cavitt Stallman Rd | Arterial HighModerate | 4 | 47,570 | F | 320 | 47,890 | F | $0.008 \underline{\underline{9}}$ |
|  | Cavitt Stallman Rd to Seeno Ave | Arterial High | 4 | 46,830 | F | 320 | 47,150 | F | 0.008 |
|  | Seeno Ave to Barton Rd | Arterial High | 4 | 44,800 | F | 340 | 45,140 | F | 0.009 |
|  | Berg St to Barton Rd | Arterial High | 4 | 44,800 | F | 190 | 44,990 | F | 0.005 |
|  | Barton Rd to Auburn-Folsom Rd | Arterial High | 4 | 42,630 | F | 110 | 42,740 | F | 0.003 |
| Berg St | Olive Ranch Rd to Project | Arterial Low | 2 | 1,200 | A | 40 | 1,240 | A | 0.003 |
|  | Project to Douglas Blvd | Arterial Low | 2 | 1,200 | A | 530 | 1,730 | A | 0.035 |
| Note: Bold indicates applicable LOS threshold exceeded. <br> Source: KD Anderson \& Associates, Inc., 2018. |  |  |  |  |  |  |  |  |  |


| Table 5-11Study Roadway Segment LOS - EPAP Plus Project Condition |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Roadway | Segment | Classification | Lanes | EPAP |  | EPAP Plus Project |  |  |  |
|  |  |  |  | ADT | LOS | ADT |  | LOS | Change in V/C |
|  |  |  |  |  |  | Project Only | Total |  |  |
| Douglas Blvd | Sierra College Blvd to Cavitt Stallman Rd | Arterial HighModerate | 4 to 6 | 51,320 | F | 320 | 51,640 | F | $0.008 \underline{\underline{9}}$ |
|  | Cavitt Stallman Rd to Seeno Ave | Arterial High | 4 | 50,160 | F | 320 | 50,480 | F | 0.008 |
|  | Seeno Ave to Barton Rd | Arterial High | 4 | 47,610 | F | 340 | 47,950 | F | 0.009 |
|  | Berg St to Barton Rd | Arterial High | 4 | 45,480 | F | 190 | 45,670 | F | 0.005 |
|  | Barton Rd to Auburn-Folsom Rd | Arterial High | 4 | 44,690 | F | 110 | 44,800 | F | 0.003 |
| Berg St | Olive Ranch Rd to Project | Arterial Low | 2 | 1,460 | A | 40 | 1,500 | A | 0.003 |
|  | Project to Douglas Blvd | Arterial Low | 2 | 1,990 | A | 530 | 2,520 | A | 0.035 |
| Note: Bold indicates applicable LOS threshold exceeded. <br> Source: KD Anderson \& Associates, Inc., 2018. |  |  |  |  |  |  |  |  |  |


| Table 5-13 <br> Study Roadway Segment LOS - Cumulative Plus Project Condition |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Roadway | Segment | Classification | Lanes | Cumulative No Project |  | Cumulative Plus Project |  |  |  |
|  |  |  |  | ADT | LOS | ADT |  | LOS | Change in V/C |
|  |  |  |  |  |  | Project Only | Total |  |  |
| Douglas Blvd | Sierra College Blvd to Cavitt Stallman Rd | Arterial Moderate | -4 6 | 54,380 | F | $323 \underline{\underline{0}}$ | 54,700 | F | 0.008 相 |
|  | Cavitt Stallman Rd to Woodgrove Way | Arterial High | 4 | 51,980 | F | 323 0 | 52,300 | F | 0.008 |
|  | Woodgrove Way to Seeno Ave | Arterial High | 4 | 50,510 | F | 340 | 50,850 | F | 0.009 |
|  | Seeno Ave to Barton Rd | Arterial High | 4 | 50,160 | F | 340 | 50,500 | F | 0.009 |
|  | Berg St to Barton Rd | Arterial High | 4 | 47,560 | F | 18890 | 47,750 | F | 0.005 |
|  | Barton Rd to Auburn-Folsom Rd | Arterial High | 4 | 48,340 | F | $112 \underline{\underline{0}}$ | 48,450 | F | 0.003 |
| Berg St | Olive Ranch Rd to Project | Arterial Low | 2 | 1,460 | A | 40 | 1,500 | A | 0.003 |
|  | Project to Douglas Blvd | Arterial Low | 2 | 1,420 | A | 52830 | 1,950 | A | 0.035 |
| Note: Bold indicates applicable LOS threshold exceeded. <br> Source: KD Anderson \& Associates, Inc., 2018. |  |  |  |  |  |  |  |  |  |


| TABLE 2-2SUMMARY OF IMPACTS AND MITIGATION MEASURES |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | Impact | Level of Significance prior to Mitigation |  | Mitigation Measures | Level of Significance after Mitigation |
| 4. Noise |  |  |  |  |  |
| 4-3 | Exposure of persons to or generation of excessive groundborne vibration or groundborne noise levels. | S | $4-3(a)$ | A Blasting Plan for construction shall be prepared and submitted to the County Planning Services Division at least ten (10) days prior to initiation of construction activities. The plan shall include the following: <br> (Note: No changes to the remainder of the mitigation measure are proposed or necessary; thus, the remainder of the mitigation measure has not been reproduced here.) | LS |
| IX-5. <br> IX-6. <br> IX-7. | Create or contribute runoff water which would include substantial additional sources of polluted water? (ESD) <br> Otherwise substantially degrade surface water quality?(ESD) <br> Otherwise substantially degrade ground water quality? (EHS) | S | MM IX-5: | The Improvement Plans shall show water quality treatment facilities/Best Management Practices (BMPs) designed according to the guidance of the California Stormwater Quality Association Stormwater Best Management Practice Handbooks for Construction, for New Development / Redevelopment, and for Industrial and Commercial (or other similar source as approved by the Engineering and Surveying Division (ESD) such as the Stormwater Quality Design Manual for the Sacramento and South Placer Regions). <br> Storm drainage from on- and off-site impervious surfaces (including roads) shall be collected and routed through specially designed catch basins, vegetated swales, vaults, infiltration basins, water quality basins, filters, etc. for entrapment of sediment, debris and oils/greases or other identified pollutants, as approved by the Engineering and Surveying Division (ESD). BMPs shall be designed in | LS |

## TABLE 2-2

SUMMARY OF IMPACTS AND MITIGATION MEASURES

| Impact | Level of <br> Significance <br> prior to <br> Mitigation | Mitigation Measures | Level of Significance after <br> Mitigation |
| :---: | :---: | :---: | :---: |
|  |  | accordance with the (CHOOSE ONE:-West-OR East) Placer Storm Water Quality Design Manual for sizing of permanent post-construction Best Management Practices for stormwater quality protection. No water quality facility construction shall be permitted within any identified wetlands area, floodplain, or right-of-way, except as authorized by project approvals. <br> All permanent BMPs shall be maintained as required to ensure effectiveness. The applicant shall provide for the establishment of vegetation, where specified, by means of proper irrigation. Proof of on-going maintenance, such as contractual evidence, shall be provided to ESD upon request. The project owners/permittees shall provide maintenance of these facilities and annually report a certification of completed maintenance to the County DPWF Stormwater Coordinator, unless, and until, a County Service Area is created and said facilities are accepted by the County for maintenance. Contractual evidence of a monthly parking lot sweeping and vacuuming, and catch basin cleaning program shall be provided to the ESD upon request. Failure to do so will be grounds for discretionary permit revocation. Prior to Improvement Plan approval, easements shall be created and offered for dedication to the County for maintenance and access to these facilities in anticipation of possible County maintenance. |  |

## 4. MITIGATION MONITORING AND REPORTING PROGRAM

# MITIGATION MONITORING AND REPORTING PROGRAM 

### 4.1 INTRODUCTION

Section 15097 of the California Environmental Quality Act (CEQA) requires all State and local agencies to establish monitoring or reporting programs for projects approved by a public agency whenever approval involves the adoption of either a "mitigated negative declaration" or specified environmental findings related to environmental impact reports.

The following is the Mitigation Monitoring and Reporting Program (MMRP) for the Quarry Ridge project (proposed project). The intent of the MMRP is to ensure implementation of the mitigation measures identified within the Environmental Impact Report (EIR) for the proposed project. Unless otherwise noted, the cost of implementing the mitigation measures as prescribed by this MMRP shall be funded by the applicant.

### 4.2 COMPLIANCE CHECKLIST

The MMRP contained herein is intended to satisfy the requirements of CEQA as they relate to the EIR and the Initial Study prepared for the proposed project. This MMRP is intended to be used by Placer County staff and mitigation monitoring personnel to ensure compliance with mitigation measures during project implementation. Mitigation measures identified in this MMRP were developed in the EIR and Initial Study.

The EIR presents a detailed set of mitigation measures that will be implemented throughout the lifetime of the project. Mitigation is defined by CEQA Guidelines, Section 15370, as a measure that:

- Avoids the impact altogether by not taking a certain action or parts of an action;
- Minimizes impacts by limiting the degree or magnitude of the action and its implementation;
- Rectifies the impact by repairing, rehabilitating, or restoring the impacted environment;
- Reduces or eliminates the impact over time by preservation and maintenance operations during the life of the project; or
- Compensates for the impact by replacing or providing substitute resources or environments.

The intent of the MMRP is to ensure the implementation of adopted mitigation measures. The MMRP will provide for monitoring of construction activities as necessary and in-the-field identification and resolution of environmental concerns.

Monitoring and documenting the implementation of mitigation measures will be coordinated by Placer County. The table attached to this report identifies the mitigation measure, the monitoring action for the mitigation measure, the responsible party for the monitoring action, and timing of the monitoring action. The applicant will be responsible for fully understanding and effectively implementing the mitigation measures contained within the MMRP. The County will be responsible for monitoring compliance.

### 4.3 Mitigation MONitoring and Reporting Program

The following table indicates the mitigation measure number, the impact the measure is designed to address, the measure text, the monitoring agency, implementation schedule, and an area for sign-off indicating compliance.

| MITIGATION MONITORING AND REPORTING PROGRAM QUARRY RIDGE PROJECT |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Impact <br> Number | Impact |  | Mitigation Measure | Monitoring Agency | Implementation Schedule | Sign-off |
| Chapter 4 - Noise |  |  |  |  |  |  |
| 4-2 | Exposure of persons to or generation of nontransportation noise levels in excess of standards established in the local General Plan, Community Plan or noise ordinance, or applicable standards of other agencies. | 4-2(a) <br> 4-2(b) | Prior to issuance of building permits for the proposed project, if rooftop condenser HVAC units are proposed on-site, building plans shall show that rooftop mechanical equipment will be shielded to the north by parapets. <br> Prior to issuance of building permits for the proposed project, if ground-mounted HVAC equipment is proposed on-site, the building plans shall demonstrate that all groundmounted HVAC equipment will be located 100 feet or further from the northern site boundary. In addition, the building plans shall show that ground-mounted HVAC equipment associated with Building 4 will be located on the west side of the building, breaking the line of sight relative to the eastern project site boundary. In addition, ground-mounted HVAC equipment associated with each of the four proposed buildings shall be located 100 feet or greater from the nearest property lines to the north of the project site. | Placer County Community Development Resources Agency <br> Placer County Community Development Resources Agency | Prior to issuance of building permits <br> Prior to issuance of building permits |  |
| 4-3 | Exposure of persons to or generation of excessive groundborne vibration or groundborne noise levels. | $4-3(a)$ | A Blasting Plan for construction shall be prepared and submitted to the County Planning Services Division at least ten (10) days prior to any scheduled blasting activities. The plan shall include the following: | Placer County <br> Planning <br> Services <br> Division | At least ten (10) days prior to any scheduled blasting activities |  |

ChAPTER 4 - Mitigation Monitoring and Reporting Program

| MITIGATION MONITORING AND REPORTING PROGRAM QUARRY RIDGE PROJECT |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Impact Number | Impact | Mitigation Measure | Monitoring Agency | Implementation Schedule | Sign-off |
|  |  | 1. The Blasting Plan shall be consistent with the County General Plan Noise Element's Policy 9.A.4. <br> 2. Primary components of the Blasting Plan shall include: <br> a. Identification of blast officer; <br> b. Scaled drawings of blast locations, and neighboring buildings, streets, or other locations which could be inhabited; <br> c. Blasting notification procedures, lead times, and lists of those notified. Public notification to potentially affected vibration receptors describing the expected extent and duration of the blasting; <br> d. Description of means for transportation and on-site storage and security of explosives in accordance with local, State and federal regulations; <br> e. Minimum acceptable weather conditions for blasting and safety provisions for potential stray current (if electric detonation); <br> f. Traffic control standards and traffic safety measures (if |  |  |  |

CHAPTER 4 - Mitigation Monitoring and REporting Program

| MITIGATION MONITORING AND REPORTING PROGRAM QUARRY RIDGE PROJECT |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Impact <br> Number | Impact | Mitigation Measure | Monitoring Agency | Implementation Schedule | Sign-off |
|  |  | applicable); <br> g. Requirements for personal protective equipment; <br> h. Minimum standoff distances and description of blast impact zones and procedures for clearing and controlling access to blast danger; <br> i. Procedures for handling, setting, wiring, and firing explosives, as well as procedures for handling misfires per federal code; <br> $j$. Type and quantity of explosives and description of detonation device. Sequence and schedule of blasting rounds, including general method of excavation, lift heights, etc.; <br> k. Methods of matting or covering of blast area to prevent flyrock and excessive air blast pressure; <br> l. Description of blast vibration and air blast monitoring programs; <br> m. Dust control measures in compliance with applicable air pollution control regulations (to interface with general construction dust control plan); |  |  |  |

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| MITIGATION MONITORING AND REPORTING PROGRAM QUARRY RIDGE PROJECT |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Impact <br> Number | Impact | Mitigation Measure | Monitoring Agency | Implementation Schedule | Sign-off |
|  |  | n. Emergency Action Plan to provide emergency telephone numbers and directions to medical facilities. Procedures for action in the event of injury; <br> o. Material Safety Data Sheets for each explosive or other hazardous materials to be used; <br> p. Evidence of licensing, experience, and qualifications of blasters; and <br> q. Description of insurance for the blasting work. <br> 3. A Blast Survey Workplan shall be prepared by the blaster. The Plan shall establish vibration limits in order to protect structures from blasting activities and identify specific monitoring points. At a minimum, a pre-blast survey shall be conducted of any potentially affected structures and underground utilities within 500 feet of a blast area, as well as the nearest residential structure, prior to blasting. The survey shall include visual inspection of the structures, documentation of structures by means of photographs, video, and a level survey of the ground floor of structures or the crown of major and critical utility lines, and these shall be |  |  |  |

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| MITIGATION MONITORING AND REPORTING PROGRAM QUARRY RIDGE PROJECT |  |  |  |  |  |
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| Impact <br> Number | Impact | Mitigation Measure | Monitoring Agency | Implementation Schedule | Sign-off |
|  |  | submitted to the County. This documentation shall be reviewed with the individual owners prior to any blasting operations. The County and impacted property owners shall be notified at least 48 hours prior to the visual inspections. <br> 4. Vibration and settlement threshold criteria (for example peak particle velocity of 0.5 inches per second) shall be submitted by the blaster to the County for review and approval during the design process. If the settlement or vibration criteria are exceeded at any time or if damage is observed at any of the structures or utilities, then blasting shall immediately cease and the County immediately notified. The stability of segmental retaining walls, existing slopes, creek canals, etc. shall be monitored and any evidence of instability due to blasting operations shall result in immediate termination of blasting. The blaster shall modify the blasting procedures or use alternative means of excavating in order to reduce the vibrations to below the threshold values, prevent further settlement, slope instability, and prevent further damage. |  |  |  |

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| MITIGATION MONITORING AND REPORTING PROGRAM QUARRY RIDGE PROJECT |  |  |  |  |  |
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| Impact <br> Number | Impact | Mitigation Measure | Monitoring Agency | Implementation Schedule | Sign-off |
|  |  | 5. Air blast overpressure limits shall be set and monitoring shall be conducted at the property line closest to the blast and at other above ground structures identified in the Plan for vibration monitoring. Air blast overpressure limits shall be in accordance with applicable law and shall be established to prevent damage to adjacent properties, new construction, and to prevent injuries to persons onsite and off-site. <br> 6. Prior to full-scale production blasting, the blaster shall conduct a series of test blasts at the sites where blasting is to occur. The tests shall start with reduced charge weights and shall increase incrementally to that of a full-scale production round. Monitoring shall be conducted as described in the Plan. <br> 7. Post-construction monitoring structures to identify (and repair if necessary) all damage, if any, from blasting vibrations. Any damage shall be documented by photograph, video, etc. This documentation shall be reviewed with the individual property owners. <br> 8. Reports of the results of the blast monitoring shall be provided to the |  |  |  |

CHAPTER 4 - Mitigation MONITORING AND REPORTING PROGRAM

| MITIGATION MONITORING AND REPORTING PROGRAM QUARRY RIDGE PROJECT |  |  |  |  |  |
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| Impact <br> Number | Impact | Mitigation Measure | Monitoring Agency | Implementation Schedule | Sign-off |
|  |  | County, the local fire department, and owners of any buried utilities on or adjacent to the site within 24 hours following blasting. Reports documenting damage, excessive vibrations, etc. shall be provided to the County and impacted property owners. <br> 4-3(b) Include the following standard note on the Improvement Plans: In the event of blasting, three copies of an approved plan and permit shall be submitted to the County not less than 10 days prior to the scheduled blasting. A blasting permit must be obtained from the Placer County Sheriff's Office for all blasting to be done in Placer County. Additionally, the County must be notified and give approval for all blasting done within County right-of-way. If utility companies are in the vicinity where blasting is to occur, the appropriate utility companies must be notified to determine possible damage prevention measures. If blasting is required, the blasting schedule shall be approved by the County and any other utility companies with facilities in the area prior to the commencement of work. | Placer County <br> Engineering and Surveying Division <br> Placer County <br> Sheriff's Office | Prior to approval of Improvement Plans |  |
| 4-4 | A substantial temporary or periodic increase in ambient noise levels in the project vicinity above | 4-4(a) The following notes shall be included in the project's Improvement Plans. Exceptions to allow expanded construction activities shall be reviewed on a case-by-case basis as | Placer County Community Development Resource | Prior to approval of Improvement Plans |  |

[^1]| MITIGATION MONITORING AND REPORTING PROGRAM QUARRY RIDGE PROJECT |  |  |  |  |  |
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| Impact <br> Number | Impact | Mitigation Measure | Monitoring Agency | Implementation Schedule | Sign-off |
|  | levels existing without the project. | determined by the Community Development Resource Agency Director and/or County Engineer. <br> - Noise-generating construction activities (e.g. construction, alteration or repair activities), including truck traffic coming to and from the project site for any purpose, shall be limited to the hours outlined in Placer County Board of Supervisors Minute Order 90-08; specifically, a) Monday through Friday, 6:00 AM to 8:00 PM (during daylight savings); b) Monday through Friday, 7:00 AM to 8:00 PM (during standard time); and c) Saturdays, 8:00 AM to 6:00 PM. <br> - Project construction activities should be limited to daytime hours unless conditions warrant that certain construction activities occur during evening or early morning hours (i.e., extreme heat). <br> - All noise-producing project equipment and vehicles using internalcombustion engines shall be equipped with mufflers, air-inlet silencers where appropriate, and any other shrouds, shields, or other noise-reducing features in good operating condition that meet or exceed original factory | Agency <br> Placer County <br> Planning <br> Services <br> Division |  |  |

CHAPTER 4 - Mitigation Monitoring and REporting Program

| MITIGATION MONITORING AND REPORTING PROGRAM QUARRY RIDGE PROJECT |  |  |  |  |  |
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| Impact <br> Number | Impact | Mitigation Measure | Monitoring Agency | Implementation Schedule | Sign-off |
|  |  | specifications. Mobile or fixed "package" equipment (e.g., arc welders, air compressors) shall be equipped with shrouds and noisecontrol features that are readily available for that type of equipment. <br> - All mobile or fixed noise-producing equipment used on the project site that are regulated for noise output by a federal, State, or local agency shall comply with such regulations while in the course of project activity. <br> - Electrically powered equipment shall be used instead of pneumatic or internal combustion-powered equipment, where feasible. <br> - Material stockpiles and mobile equipment staging, parking, and maintenance areas shall be located as far as practicable from noise-sensitive receptors. <br> - Construction site and access road speed limits shall be established and enforced during the construction period. <br> - The use of noise-producing signals, including horns, whistles, alarms, and bells, shall be for safety warning purposes only. <br> - Project-related public address or |  |  |  |

Chapter 4 - Mitigation Monitoring and Reporting Program

| MITIGATION MONITORING AND REPORTING PROGRAM QUARRY RIDGE PROJECT |  |  |  |  |  |
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| Impact <br> Number | Impact | Mitigation Measure | Monitoring Agency | Implementation Schedule | Sign-off |
|  |  | music systems shall not be audible at any adjacent receptor. <br> 4-4(b) Implement Mitigation Measures 4-3(a) and 43(b). | See Mitigation Measures 4-3(a) and 4-3(b) | See Mitigation Measures 4-3(a) and 4-3(b) |  |
| Chapter 5 - Transportation and Circulation |  |  |  |  |  |
| 5-1 | Traffic related to construction activities. | 5-1 The Improvement Plans shall include a striping and signing plan and shall include all on- and off-site traffic control devices. Prior to the commencement of construction, a construction signing and traffic control plan shall be provided to the Engineering and Surveying Division for review and approval. The construction signing and traffic control plan shall include (but not be limited to) items such as: <br> - Guidance on the number and size of trucks per day entering and leaving the project site; <br> - Identification of arrival/departure times that would minimize traffic impacts; <br> - Approved truck circulation patterns; <br> - Locations of staging areas; <br> - Methods for partial/complete street closures (e.g., timing, signage, location and duration restrictions); | Placer County <br> Engineering and Surveying Division | Prior to approval of Improvement Plans and prior to commencement of construction |  |

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| MITIGATION MONITORING AND REPORTING PROGRAM QUARRY RIDGE PROJECT |  |  |  |  |  |
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| Impact <br> Number | Impact | Mitigation Measure | Monitoring Agency | Implementation Schedule | Sign-off |
|  |  | - Criteria for use of flaggers and other traffic controls; <br> - Preservation of safe and convenient passage for bicyclists and pedestrians through/around construction areas; <br> - Monitoring for roadbed damage and timing for completing repairs; <br> - Limitations on construction activity during peak/holiday weekends and special events; <br> - Preservation of emergency vehicle access; <br> - Coordination of construction activities with construction of other projects that occur concurrently in Granite Bay to minimize potential additive construction traffic disruptions, avoid duplicative efforts (e.g., multiple occurrences if similar signage), and maximize effectiveness of traffic mitigation measures (e.g., joint employee alternative transportation programs); <br> - Removing traffic obstructions during emergency evacuation events; and <br> - Providing a point of contact for Granite Bay residents and guests to obtain construction information, have questions answered, and convey complaints. |  |  |  |


| MITIGATION MONITORING AND REPORTING PROGRAM QUARRY RIDGE PROJECT |  |  |  |  |  |  |
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| Impact <br> Number | Impact |  | Mitigation Measure | Monitoring Agency | Implementation Schedule | Sign-off |
| 5-2 | Study intersections under the Existing Plus Project Condition. | 5-2 | The Improvement Plans for the initial development phase shall show the construction of a raised median at the existing intersection of Douglas Blvd. / Woodgrove Way / Quail Oaks Drive that will prohibit northbound and southbound left turn movements onto Douglas Blvd. from Woodgrove Way and Quail Oaks Drive. In addition, the raised median shall allow for eastbound and westbound left turn movements onto Quail Oaks Drive and Woodgrove Way from Douglas Blvd. The construction of the new raised median shall also require the reconstruction of the existing landscaped median to a narrower, stamped, colored, concrete median that will provide a 12-footwide eastbound left turn lane along Douglas Blvd. The design shall be to the satisfaction of the Department of Public Works and shall conform to any applicable criteria specified in the latest version of the Caltrans Highway Design Manual for a design speed of 55 miles per hour (mph), unless an alternative is approved by the Department of Public Works. (ESD) | Placer County <br> Department of Public Works <br> Placer County <br> Engineering and <br> Surveying <br> Division | Prior to approval of Improvement Plans |  |
| 5-6 | Increased impacts to vehicle safety due to roadway design features (i.e. sharp curves or dangerous intersections) or incompatible uses |  | The Improvement Plans shall show the construction of an increase in existing turn lane pocket length of a total of approximately 100 combined feet for the existing left turn lane approaching Berg Street (eastbound) and the existing left turn lane approaching Granite | Placer County Department of Public Works <br> Placer County Engineering and | Prior to approval of Improvement Plans |  |

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| Impact <br> Number | Impact |  | Mitigation Measure | Monitoring Agency | Implementation Schedule | Sign-off |
|  | (e.g., farm equipment). |  | Estates Drive (westbound) along Douglas Blvd. The minimum increase in length for the existing left turn lane approaching Granite Estates Drive shall be 50 feet. The design shall be to the satisfaction of the Department of Public Works and shall conform to any applicable criteria specified in the latest version of the Caltrans Highway Design Manual for a design speed of 55 miles per hour (mph), unless an alternative is approved by the Department of Public Works. | Surveying Division |  |  |
| 5-8 | Study intersections under the Cumulative Plus Project Condition. |  | Prior to issuance of any Building Permits, this project shall be subject to the payment of traffic impact fees that are in effect in this area (Granite Bay), pursuant to applicable Ordinances and Resolutions. The applicant is notified that the following traffic mitigation fee(s) shall be required and shall be paid to Placer County DPW: <br> A. County Wide Traffic Limitation Zone: Article 15.28.010, Placer County Code <br> B. South Placer Regional Transportation Authority (SPRTA) <br> The current total combined estimated fee is $\$ 504,715.52$ (based on $\$ 7,426$ per DUE and 17,000 square feet of office use) The fees were calculated using the information supplied. If either the use or the square footage changes, | Placer County Department of Public Works | Prior to issuance of any Building Permits |  |

[^2]| MITIGATION MONITORING AND REPORTING PROGRAM QUARRY RIDGE PROJECT |  |  |  |  |  |  |
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| Impact <br> Number | Impact |  | Mitigation Measure | Monitoring Agency | Implementation Schedule | Sign-off |
|  |  |  | n the fees will change. The fees to be paid all be based on the fee program in effect at time the application is deemed complete. |  |  |  |
| Initial Study |  |  |  |  |  |  |
| I-4 | Create a new source of substantial light or glare, which would adversely affect day or nighttime views in the area. | MM I-1: | Concurrent with submittal of Improvement Plans, a detailed lighting and photometric plan shall be submitted to the DRC for review and approval. The lighting and photometric plan shall include the following provisions: <br> - Parking lot lighting shall be accomplished with pole mounted decorative LED luminaries. The parking lot shall be illuminated by using 14-foot decorative post-top type LED fixtures mounted on metal poles. The pole color shall be such that the pole will blend into the landscape (i.e., black, bronze, or dark bronze). Such luminaires shall also be provided with house side shields to minimize light pollution to the areas outside of the property line. <br> - The parking lot lighting shall be photocell controlled to provide automatic light reduction by a minimum of 50 percent between the hours of 11 PM and 6 AM. The | Placer County Community Development Resource Agency <br> Placer County <br> Planning <br> Services <br> Division | Concurrent with submittal of Improvement Plans |  |

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| MITIGATION MONITORING AND REPORTING PROGRAM QUARRY RIDGE PROJECT |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Impact <br> Number | Impact | Mitigation Measure | Monitoring Agency | Implementation Schedule | Sign-off |
|  |  | site lighting shall be dimmed to lower level automatically. <br> - Landscape lighting may be used to visually accentuate and highlight ornamental shrubs and trees adjacent to buildings and in open spaces. Lighting intensity will be of a level that only highlights shrubs and trees and will not impose glare on any pedestrian or vehicular traffic. <br> - Architectural lighting shall articulate and animate the particular building design and visibly promote and reinforce pedestrian movement. Indirect wall lighting or "wall washing" and interior illumination (glow) is encouraged in the expression of the building. <br> - Wall-mounted light fixtures will be permitted only if they have a 90 degree cut off to prevent glare. <br> - No lighting is permitted on top of structures. <br> - Pedestrian routes should utilize bollard type lighting rather than pole lights and should be integrated into building and landscape design. Pedestrian- |  |  |  |


| MITIGATION MONITORING AND REPORTING PROGRAM QUARRY RIDGE PROJECT |  |  |  |  |  |  |
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| Impact <br> Number | Impact |  | Mitigation Measure | Monitoring Agency | Implementation Schedule | Sign-off |
|  |  |  | scale light fixtures shall be durable and vandal resistant. |  |  |  |
| IV-1 | Have a substantial adverse effect, either directly or through habitat modifications, on any species identified as a candidate, sensitive, or special status species in local or regional plans, policies or regulations, or by the California <br> Department of Fish \& Game, U.S. Fish \& Wildlife Service or National Oceanic and Atmospheric Administration Fisheries. <br> Substantially reduce the habitat of a fish or wildlife species, cause a fish or wildlife population to drop below self-sustaining levels, threaten to eliminate a plant or animal community, substantially reduce the number of restrict the range of an endangered, rare, or | MM IV-1: | If ground disturbance activities take place during the breeding/nesting season (February 1 through August 31), disturbance of nesting activities could occur. Take of any active raptor nest, as well as nests of other birds protected by the Migratory Bird Treaty Act, is prohibited under California Fish and Game Code sections 3503, 3503.5, and 3513. To avoid impacts to nesting birds, necessary vegetation removal shall occur outside of the typical nesting season (February 1 through August 31). If vegetation removal must occur at any time during the typical nesting season, a preconstruction survey shall be conducted by a qualified biologist no more than 15 days prior to initiation of the proposed development activities. <br> The qualified biologist shall conduct a focused survey for active nests of raptors and migratory birds within and in the vicinity of the proposed project site (up to 100 feet beyond the project site boundaries, where possible). If active nests are found, trees/shrubs with nesting birds shall not be disturbed until abandoned by the birds as determined by a | Placer County Community Development Resource Agency <br> Placer County <br> Planning Services Division | If ground disturbance activities take place during the breeding/nesting season (February 1 through August 31), then no more than 15 days prior to initiation of the proposed development activities |  |


| MITIGATION MONITORING AND REPORTING PROGRAM QUARRY RIDGE PROJECT |  |  |  |  |  |  |
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| Impact <br> Number | Impact |  | Mitigation Measure | Monitoring Agency | Implementation Schedule | Sign-off |
|  | threatened species. |  | qualified biologist. If applicable, vegetation removal shall be restricted to a period following fledging of chicks, which typically occurs between late July and early August. <br> If an active nest is located within 100 feet (200 feet for raptors) of construction activities, other restrictions may include establishment of exclusion zones (no ingress of personnel or equipment at a minimum radius of 100 feet or 200 feet, as appropriate, around the nest or alteration of the construction schedule. If construction activities cause the nesting bird(s) to vocalize, make defensive flights at intruders, get up from a brooding position, or fly off the nest, then the exclusionary buffer shall be increased, as determined by the qualified biologist, such that activities are far enough from the nest to stop the agitated behavior. The exclusionary buffer shall remain in place until the young have fledged or as otherwise determined by a qualified biologist. |  |  |  |
| IV-7 | Conflict with any local policies or ordinances that protect biological resources, including oak woodland resources. | MM IV-2: | Prior to any removal of significant trees (equal to, or greater than, six inches $D B H$ or 10 inches $D B H$ aggregate for multitrunked trees), the project applicant shall obtain a tree removal permit from Placer | Placer County Community Development Resource Agency | Prior to any removal of significant trees |  |

[^3]| MITIGATION MONITORING AND REPORTING PROGRAM QUARRY RIDGE PROJECT |  |  |  |  |  |
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| Impact <br> Number | Impact | Mitigation Measure | Monitoring Agency | Implementation Schedule | Sign-off |
|  |  | County. In conjunction with submittal of a tree removal permit application, the applicant shall submit a site plan showing all protected trees proposed for removal. In accordance with Chapter 12.16.080 of the Placer County Code, the applicant shall comply with any permit conditions required by the Planning Services Division, which shall include one of the following requirements: 1:1 tree replacement using five-gallon size trees or greater, or in-lieu fees, or a combination of both, in accordance with Section 12.16.080 of the Placer County Code. <br> MM IV-3: Prior to Improvement Plan approval, the plans shall include a list of tree protection methods, for review and approval by the Planning Services Division. The list of tree protection methods shall be implemented during construction of the project. The list of tree protection methods shall include, but not limited to, the following: <br> - The applicant shall install a fourfoot tall, brightly colored (yellow or orange), synthetic mesh material fence around all oak trees to be preserved that are greater than six inches $D B H$ (or 10 inches DBH aggregate for | Placer County Planning Services Division <br> Placer County <br> Planning <br> Services <br> Division | Prior to Improvement Plan approval |  |

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| MITIGATION MONITORING AND REPORTING PROGRAM QUARRY RIDGE PROJECT |  |  |  |  |  |
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| Impact <br> Number | Impact | Mitigation Measure | Monitoring Agency | Implementation Schedule | Sign-off |
|  |  | multi-trunked trees). The fencing shall delineate an area that is at least the radius of which is equal to the largest radius of the protected tree's drip line plus one foot. The fence shall be installed prior to any site preparation or construction equipment being moved onsite or any site preparation or construction activities taking place. Development of this site, including grading, shall not be allowed until this condition is satisfied. Any encroachment within the areas listed above, including within driplines of trees to be saved, must first be approved by a designated representative of the Development Review Committee (DRC). Grading, clearing, or storage of equipment or machinery may not occur until a representative of the DRC has inspected and approved all temporary construction fencing. Trees shall be preserved where feasible. This may include the use of retaining walls, planter islands, or other techniques commonly associated with tree preservation. The Improvement |  |  |  |

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|  |  | Plans shall indicate the location of the fencing and include a note describing the fencing requirements consistent with this mitigation measure. <br> - The project applicant shall implement the following guidelines before and during grading and construction for protection of all oak trees to be preserved: <br> o Plans and specifications shall clearly state protection procedures for oak trees on the project site. The specifications shall also include a provision for remedies if oak trees are damaged; <br> o Before construction commences, those oak trees within 25 feet of construction sites shall be pruned by an ASI Certified Arborist and the soil aerated and fertilized; <br> o Vehicles, construction equipment, mobile offices, or materials shall not be parked, stored, or operated within the |  |  |  |

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|  |  | driplines of oak trees to be preserved; <br> o Cuts and fills around trees shall be avoided where feasible; <br> o Soil surface removal greater than one foot shall not occur within the driplines of oak trees to be preserved. Cuts shall not occur within five feet of their trunks; <br> o Earthen fill greater than one foot deep shall not be placed within the driplines of oak trees to be preserved, and fill shall not be placed within five feet of their trunks; <br> o Underground utility line trenching shall not be placed within the driplines of oak trees to be preserved where feasible without first obtaining approval from a designated representative of the DRC. If it is necessary to install underground utilities within the driplines of oak |  |  |  |

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|  |  | trees, boring or drilling rather than trenching shall be used; <br> o Paving shall not be placed in the vicinity of oak trees to be preserved (at a minimum, within the dripline of any oak tree) without first obtaining approval from a designated representative of the DRC; and <br> o Irrigation lines or sprinklers shall not be allowed within the dripline of native oak trees. <br> - If any of the on-site Significant Trees are heavily damaged during construction activities associated with the proposed project, the project applicant shall pay an inlieu fee for the damaged tree(s) in accordance with Section 12.16.080 of the Placer County Code. Payment of such fees shall be ensured as a standard condition of approval by the Planning Services Division. |  |  |  |


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| V-2 | Substantially cause adverse change in the significance of a unique archaeological resource pursuant to CEQA Guidelines, Section 15064.5. | MM V-1: If any unknown prehistoric or historic artifacts, or other indications of archaeological resources are inadvertently found during grounddisturbing activities associated with the proposed project, all work within 100 feet of the find shall cease and the applicant shall notify the Placer County Community Development Resources Agency and retain an archaeologist meeting the Secretary of the Interior's Professional Qualifications Standards in prehistoric or historical archaeology, as appropriate, to evaluate the finds. If the resource is determined to be eligible for inclusion in the California Register Historical Resources and project impacts cannot be avoided, data recovery shall be undertaken. Data recovery efforts could range from rapid photographic documentation to extensive excavation depending upon the physical nature of the resource. The degree of effort shall be determined at the discretion of a qualified archaeologist and shall be sufficient to recover data considered important to the area's history and/or prehistory. The language of this mitigation measure shall be included on any future grading plans, utility plans, and improvement drawings approved by the Placer County Engineering and Surveying Division for | Placer County <br> Community <br> Development <br> Resources <br> Agency <br> Placer County <br> Planning <br> Services <br> Division | During grounddisturbing activities |  |

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|  |  |  | the proposed project. |  |  |  |
| V-5 | Disturb any human remains, including those interred outside of dedicated cemeteries. | MM V-2: | If human remains are encountered on the proposed project site during construction activities, all work within 100 feet of the find must cease, and any necessary steps to ensure the integrity of the immediate area must be taken. The Placer County Coroner shall be immediately notified. If the Coroner determines the remains are of Native American origin, the Coroner shall notify the Native American Heritage Commission (NAHC) within 24 hours. The NAHC shall determine and notify a Most Likely Descendent (MLD). Further actions shall be determined, in part, by the desires of the MLD. The MLD shall be afforded 48 hours to make recommendations regarding the disposition of the remains following notification from the NAHC of the discovery. If the MLD does not make recommendations within 48 hours, the owner shall, with appropriate dignity, reinter the remains in an area of the property secure from further disturbance. Alternatively, if the owner does not accept the MLD's recommendations, the owner or the descendent may request mediation by the NAHC. | Placer County <br> Community <br> Development <br> Resource <br> Agency <br> Placer County <br> Planning <br> Services <br> Division <br> Placer County <br> Coroner <br> Native American <br> Heritage <br> Commission | During construction |  |
| VI-2 | Result in significant disruptions, displacements, | MM VI-1: | The applicant shall prepare and submit Improvement Plans, specifications and cost estimates (per the requirements of | Placer County <br> Engineering and Surveying | Prior to approval of Improvement Plans |  |

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| VI-3 | compaction or overcrowding of the soil. <br> Result in substantial change in topography or ground surface relief features. | Section II of the Land Development Manual $[L D M]$ that are in effect at the time of submittal) to the Engineering and Surveying Division (ESD) for review and approval of each project phase. The plans shall show all physical improvements as required by the conditions for the project as well as pertinent topographical features both on and off site. All existing and proposed utilities and easements, on site and adjacent to the project, which may be affected by planned construction, shall be shown on the plans. All landscaping and irrigation facilities within the public right-of-way (or public easements), landscaping within sight distance areas at intersections, shall be included in the Improvement Plans. The applicant shall pay plan check and inspection fees and, if applicable, Placer County Fire <br> Department improvement plan review and inspection fees, with the 1st Improvement Plan submittal. (NOTE: Prior to plan approval, all applicable recording and reproduction costs shall be paid). The cost of the above-noted landscape and irrigation facilities shall be included in the estimates used to determine these fees. It is the applicant's responsibility to obtain all required agency signatures on the plans and to secure department approvals. If the | Division |  |  |


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|  |  | Design/Site Review process and/or Development Review Committee (DRC) review is required as a condition of approval for the project, said review process shall be completed prior to submittal of Improvement Plans. Record drawings shall be prepared and signed by a California Registered Civil Engineer at the applicant's expense and shall be submitted to the ESD in both hard copy and electronic versions in a format to be approved by the ESD prior to acceptance by the County of site improvements. <br> Conceptual landscape plans submitted prior to project approval may require modification during the Improvement Plan process to resolve issues of drainage and traffic safety. <br> Any Building Permits associated with this project shall not be issued until, at a minimum, the Improvement Plans are approved by the Engineering and Surveying Division. <br> MM VI-2: The Improvement Plans shall show all proposed grading, drainage improvements, vegetation and tree removal and all work shall conform to provisions of the County Grading | Placer County <br> Engineering and Surveying Division | Prior to approval of Improvement Plans |  |

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|  |  | Ordinance (Ref. Article 15.48, Placer County Code) and Stormwater Quality Ordinance (Ref. Article 8.28, Placer County Code) that are in effect at the time of submittal. No grading, clearing, or tree disturbance shall occur until the Improvement Plans are approved and all temporary construction fencing has been installed and inspected by a member of the Development Review Committee (DRC). All cut/fill slopes shall be at a maximum of 2:1 (horizontal: vertical) unless a soils report supports a steeper slope and the Engineering and Surveying Division (ESD) concurs with said recommendation. <br> The applicant shall revegetate all disturbed areas. Revegetation, undertaken from April 1 to October 1, shall include regular watering to ensure adequate growth. A winterization plan shall be provided with project Improvement Plans. It is the applicant's responsibility to ensure proper installation and maintenance of erosion control/winterization before, during, and after project construction. Soil stockpiling or borrow areas, shall have proper erosion control measures applied for the duration of the construction as specified in the Improvement Plans. Provide for | Development Review Committee |  |  |

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|  |  | erosion control where roadside drainage is off of the pavement, to the satisfaction of the Engineering and Surveying Division (ESD). <br> The applicant shall submit to the ESD a letter of credit or cash deposit in the amount of 110 percent of an approved engineer's estimate for winterization and permanent erosion control work prior to Improvement Plan approval to guarantee protection against erosion and improper grading practices. One year after the County's acceptance of improvements as complete, if there are no erosion or runoff issues to be corrected, unused portions of said deposit shall be refunded to the project applicant or authorized agent. <br> If, at any time during construction, a field review by County personnel indicates a significant deviation from the proposed grading shown on the Improvement Plans, specifically with regard to slope heights, slope ratios, erosion control, winterization, tree disturbance, and/or pad elevations and configurations, the plans shall be reviewed by the DRC/ESD for a determination of substantial conformance to the project approvals prior to any further work proceeding. Failure of the |  |  |  |

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|  |  | DRC/ESD to make a determination of substantial conformance may serve as grounds for the revocation/modification of the project approval by the appropriate hearing body. <br> MM VI-3: The Improvement Plan submittal shall include a final geotechnical engineering report produced by a California Registered Civil Engineer or Geotechnical Engineer for Engineering and Surveying Division (ESD) review and approval. The report shall address and make recommendations on the following: <br> A. Road, pavement, and parking area design; <br> B. Structural foundations, including retaining wall design (if applicable); <br> C. Grading practices; <br> D. Erosion/winterization; <br> E. Special problems discovered onsite, (i.e., groundwater, expansive/unstable soils, potential for smectite clays etc.); and <br> F. Slope stability. <br> Once approved by the ESD, two copies of the final report shall be provided to the ESD and one copy to the Building Services | Placer County <br> Engineering and Surveying Division | Prior to approval of Improvement Plans |  |

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\hline \& \& \& Division for its use. It is the responsibility of the developer to provide for engineering inspection and certification that earthwork has been performed in conformity with recommendations contained in the report. \& \& \& \\
\hline VI-5

VI-6 \& \begin{tabular}{l}
Result in any significant increase in wind or water erosion of soils, either on or off the site. <br>
Result in changes in deposition or erosion or changes in siltation which may modify the channel of a river, stream, or lake.

 \& MM VI-4: \& 

The Improvement Plans shall show water quality treatment facilities/Best Management Practices (BMPs) designed according to the guidance of the California Stormwater Quality Association Stormwater Best Management Practice Handbooks for Construction, for New Development / Redevelopment, and for Industrial and Commercial (or other similar source as approved by the Engineering and Surveying Division (ESD). <br>
Storm drainage from on- and off-site impervious surfaces (including roads) shall be collected and routed through specially designed catch basins, vegetated swales, vaults, infiltration basins, water quality basins, filters, etc. for entrapment of sediment, debris and oils/greases or other identified pollutants, as approved by the Engineering and Surveying Division (ESD). BMPs shall be designed in accordance with the West Placer Storm Water Quality Design Manual for sizing of permanent post-construction Best

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Placer County <br>
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\end{tabular} \& Prior to approval of Improvement Plans \& <br>

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|  |  | Management Practices for stormwater quality protection. No water quality facility construction shall be permitted within any identified wetlands area, floodplain, or right-of-way, except as authorized by project approvals. <br> MM VI-5: Prior to construction commencing, the applicant shall provide evidence to the Engineering and Surveying Division of a WDID number generated from the State Regional Water Quality Control Board's Stormwater Multiple Application \& Reports Tracking System (SMARTS). This serves as the Regional Water Quality Control Board approval or permit under the National Pollutant Discharge Elimination System (NPDES) construction stormwater quality permit. | Placer County Engineering and Surveying Division | Prior to commencement of construction |  |
| IX-3 | Substantially alter the existing drainage pattern of the site or area. <br> Increase the rate or amount of surface runoff. | MM IX-1: As part of the improvement plan submittal process, the preliminary Drainage Report provided during environmental review shall be submitted in final format. The final Drainage Report may require more detail than that provided in the preliminary report, and will be reviewed in concert with the improvement plans to confirm conformity between the two. The report shall be prepared by a Registered Civil Engineer and shall, at a minimum, include: A written text addressing existing | Placer County Engineering and Surveying Division | Prior to approval of Improvement Plans |  |

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|  |  | conditions, the effects of the proposed improvements, all appropriate calculations, watershed maps, changes in flows and patterns, and proposed on- and off-site improvements and drainage easements to accommodate flows from this project. The report shall identify water quality protection features and methods to be used during construction, as well as long-term post-construction water quality measures. The final Drainage Report shall be prepared in conformance with the requirements of Section 5 of the Land Development Manual and the Placer County Storm Water Management Manual that are in effect at the time of improvement plan submittal <br> MM IX-2: The final Drainage Report shall evaluate the following off-site drainage facilities for condition and capacity and shall be upgraded, replaced, or mitigated as specified by the Engineering and Surveying Division. The Improvement Plans shall provide details of the location and specifications of all proposed off-site drainage facility improvements and drainage easements to accommodate the improvements. Prior to Improvement Plan or Final Parcel Map(s) approval, the applicant shall obtain all drainage | Placer County <br> Engineering and Surveying Division | Prior to approval of Improvement Plans |  |

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|  |  | easements and necessary permits required by outside agencies: <br> A) Shed A - The existing 18-inch culvert at the southeastern site boundary that conveys flows under Berg Street and the existing roadside ditch immediately downstream of the culvert. <br> B) Shed B - The existing roadside ditch along Douglas Boulevard and the existing culvert located on the adjacent parcel's frontage approximately 100 feet east of the eastern project boundary. <br> MM IX-3: This project is subject to the one-time payment of drainage improvement and flood control fees (Strap Ravine) pursuant to the "Dry Creek Watershed Interim Drainage Improvement Ordinance" (Ref. Chapter 15, Article 15.32, Placer County Code.) The current estimated development fee is $\$ 1,950$ per gross parcel acreage, payable to the Engineering and Surveying Division prior to Building Permit issuance. The fees to be paid shall be based on the fee program in effect at the time that the application is deemed complete. | Placer County <br> Engineering and <br> Surveying <br> Division | Prior to Building Permit issuance |  |

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|  |  | MM IX-4: | This project is subject to payment of annual drainage improvement and flood control fees (Strap Ravine) pursuant to the "Dry Creek Watershed Interim Drainage Improvement Ordinance" (Ref. Chapter 15, Article 15.32, Placer County Code). Prior to Building Permit issuance, the applicant shall cause the subject property to become a participant in the existing Dry Creek Watershed County Service Area for purposes of collecting these annual assessments. The current estimated annual fee is $\$ 252$ per gross parcel acreage. | Placer County <br> Engineering and Surveying Division | Prior to Building Permit issuance |  |
| IX-5 | Create or contribute runoff water which would include substantial additional sources of polluted water. | MM IX-5: | The Improvement Plans shall show water quality treatment $\quad$ facilities/Best Management Practices (BMPs) designed according to the guidance of the California $\quad$ Stormwater Association Stormwater Best Management | Placer County <br> Engineering and Surveying Division | Prior to approval of Improvement Plans |  |
| IX-6 | Otherwise substantially degrade surface water quality. |  | Practice Handbooks for Construction, for New Development / Redevelopment, and for Industrial and Commercial (or other similar source as approved by the |  |  |  |
| IX-7 | Otherwise substantially degrade ground water quality. |  | Engineering and Surveying Division (ESD) such as the Stormwater Quality Design Manual for the Sacramento and South Placer Regions). <br> Storm drainage from on- and off-site impervious surfaces (including roads) |  |  |  |

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|  |  | shall be collected and routed through specially designed catch basins, vegetated swales, vaults, infiltration basins, water quality basins, filters, etc. for entrapment of sediment, debris and oils/greases or other identified pollutants, as approved by the Engineering and Surveying Division (ESD). BMPs shall be designed in accordance with the West Placer Storm Water Quality Design Manual for sizing of permanent post-construction Best Management Practices for stormwater quality protection. No water quality facility construction shall be permitted within any identified wetlands area, floodplain, or right-of-way, except as authorized by project approvals. <br> All permanent BMPs shall be maintained as required to ensure effectiveness. The applicant shall provide for the establishment of vegetation, where specified, by means of proper irrigation. Proof of on-going maintenance, such as contractual evidence, shall be provided to ESD upon request. The project owners/permittees shall provide maintenance of these facilities and annually report a certification of completed maintenance to the County DPW Stormwater Coordinator, unless, |  |  |  |

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|  |  | and until, a County Service Area is created and said facilities are accepted by the County for maintenance. Contractual evidence of a monthly parking lot sweeping and vacuuming, and catch basin cleaning program shall be provided to the ESD upon request. Failure to do so will be grounds for discretionary permit revocation. Prior to Improvement Plan approval, easements shall be created and offered for dedication to the County for maintenance and access to these facilities in anticipation of possible County maintenance. <br> MM IX-6: $\quad$ The Improvement Plans shall include the message details, placement, and locations showing that all storm drain inlets and catch basins within the project area shall be permanently marked/embossed with prohibitive language such as "No Dumping! Flows to Creek." or other language and/or graphical icons to discourage illegal dumping as approved by the Engineering and Surveying Division (ESD). ESD-approved signs and prohibitive language and/or graphical icons, which prohibit illegal dumping, shall be posted at public access points along channels and creeks within the project area. The property owner or | Placer County <br> Engineering and Surveying Division | Prior to approval of Improvement Plans |  |

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|  |  | Property Owners' association is responsible for maintaining the legibility of stamped messages and signs. <br> MM IX-7: The Improvement Plans shall show that all stormwater runoff shall be diverted around trash storage areas to minimize contact with pollutants. Trash container areas shall be screened or walled to prevent off-site transport of trash by the forces of water or wind. Trash containers shall not be allowed to leak and must remain covered when not in use. <br> MM IX-8: This project is located within the permit area covered by Placer County's Small Municipal Separate Storm Sewer System (MS4) Permit (State Water Resources Control Board National Pollutant Discharge Elimination System (NPDES)). Project-related stormwater discharges are subject to all applicable requirements of said permit. <br> The project shall implement permanent and operational source control measures as applicable. Source control measures shall be designed for pollutant generating activities or sources consistent with recommendations from the California Stormwater Quality Association (CASQA) | Placer County <br> Engineering and <br> Surveying <br> Division <br> Placer County <br> Engineering and <br> Surveying <br> Division | Prior to approval of Improvement Plans <br> Prior to approval of Improvement Plans |  |

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|  |  | Stormwater BMP Handbook for New Development and Redevelopment, or equivalent manual, and shall be shown on the Improvement Plans. <br> The project is also required to implement Low Impact Development (LID) standards designed to reduce runoff, treat stormwater, and provide baseline hydromodification management as outlined in the West Placer Storm Water Quality Design Manual. <br> MM IX-9: $\quad$ Per the State of California NPDES Phase II MS4 Permit, this project is a Regulated Project that creates and/or replaces 5,000 square feet or more of impervious surface. A final Storm Water Quality Plan (SWQP) shall be submitted, either within the final Drainage Report or as a separate document that identifies how this project will meet the Phase II MS4 permit obligations. Site design measures, source control measures, and Low Impact Development (LID) standards, as necessary, shall be incorporated into the design and shown on the Improvement Plans. In addition, per the Phase II MS4 permit, projects creating and/or replacing one acre or more of impervious surface are also required to demonstrate | Placer County <br> Engineering and Surveying Division | Prior to approval of Improvement Plans |  |

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|  |  | hydromodification management of stormwater such that post-project runoff is maintained to equal or below preproject flow rates for the 2 year, 24-hour storm event, generally by way of infiltration, rooftop and impervious area disconnection, bioretention, and other LID measures that result in post-project flows that mimic pre-project conditions. |  |  |  |
| IX-12 | Impact the watershed of important surface water resources, including but not limited to Lake Tahoe, Folsom Lake, Hell Hole Reservoir, Rock Creek Reservoir, Sugar Pine Reservoir, French Meadows Reservoir, Combie Lake, and Rollins Lake. | Implement Mitigation Measures MM VI-1 through -5, MM IX-1, and MM IX-5 through -9. | See Mitigation Measures MM VI-1 through -5, MM IX-1, and MM IX-5 through -9 | See Mitigation Measures MM VI1 through -5, MM IX-1, and MM IX5 through -9 |  |
| XVIII-1 | Listed or eligible for listing in the California Register of Historical Resources, or in a local register of historical resources as defined in Public Resources Code section 5020.1(k), or | Implement Mitigation Measures MM V-1 and MM V-2. | See Mitigation Measures MM V-1 and MM V2 | See Mitigation Measures MM V-1 and MM V-2 |  |


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| XVIII-2 | A resource determined by the lead agency, in its discretion and supported by substantial evidence, to be significant pursuant to criteria set forth in subdivision (c) of Public Resources Code Section 5024.1. In applying the criteria set forth in subdivision (c) of Public Resource Code Section 5024.1, the lead agency shall consider the significance of the resource to a California Native American tribe. |  |  |  |  |

## APPENDIX A

# Traffic Impact Analysis 

FOR

# Quarry Ridge Professional Office Park 

Placer County, CA

Prepared For:
RANEY PLANNING \& MANAGEMENT
1501 Sports Drive
Sacramento, CA 95834

Prepared By:
KDAnderson \& Associates, Inc.
3853 Taylor Road, Suite G
Looms, CA 95650
(916) 660-1555

April 5, 2019

Job No. 5765-20

# TRAFFIC IMPACT ANALYSIS FOR QUARRY RIDGE PROFESSIONAL OFFICE PARK <br> Placer County, CA 

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# TRAFFIC IMPACT ANALYSIS FOR QUARRY RIDGE PROFESSIONAL OFFICE PARK <br> Placer County 

## INTRODUCTION

This report summarizes a traffic impact analysis prepared for the Quarry Ridge Professional Office Park project proposed in the Placer County community of Granite Bay. The proposed project will rezone 2.8 acres located at the northeast corner of the intersection of Douglas Blvd and Berg Street from RS to OP. The project proposes construction of up to four buildings totaling 17.0 ksf. The project will take access via full access driveway on Berg Street, and no access to Douglas Blvd is proposed.

## Scope of Analysis

This analysis is intended to describe the traffic impacts of the project and to identify any circulation / roadway improvements needed to reduce project impacts to a level of insignificance. Toward this end, existing traffic conditions have been evaluated through observation of current weekday a.m. and p.m. peak hour traffic volumes and through review of daily traffic count information provided by Placer County. Future background cumulative traffic conditions have been quantified to two conditions. A short-term cumulative background condition assumed occupancy of other approved / pending projects, and a long term cumulative scenario makes use of Year 2040 data developed for the Granite Bay Circulation Element Update.

Based on initial direction from Placer County staff and the result of an initial screenline assessment this analysis focuses on traffic operations at the following nine (9) locations:

Sierra College Blvd / Douglas Blvd
Douglas Blvd / Woodgrove Way / Quail Oaks Drive
Douglas Blvd / Seeno Avenue
Douglas Blvd / Granite Estates Drive intersection
Douglas Blvd / Berg Street intersection
Douglas Blvd / Barton Road
Douglas Blvd / Sierra College Blvd
Barton Road / Eureka Road
Berg Street / new project access
Project impacts have been quantified and assessed in a manner that is consistent with Placer County policy. Probable project trip generation has been estimated by applying appropriate trip generation rates to the project's land use inventory, and comparable estimates have been made of site development under the current RS zoning. The distribution of project trips was assumed to follow the current travel patterns observed at the existing businesses in the area or based on community demographics. Utilizing the expected distribution, project trips were assigned to the study area street system via the access driveway identified in the proposed site plan. Finally,
roadway and intersection Levels of Service were re-calculated for "plus project" conditions to determine the anticipated impacts of the proposed development on both existing and future traffic conditions.

## Project Description

The Quarry Ridge Offices project is located on the north side of Douglas Blvd just east of Berg Street, as noted in Figure 1. The Ponds and Quarry Pond retail centers are on the south side of Douglas Blvd directly opposite the project site. The property across Berg Street from the project is currently vacant but is proposed for development with professional / medical offices.

Land Use. As noted in Figure 2 (site plan), the proposed project includes development of four new buildings totaling $17,000 \mathrm{sf}$ that will be devoted to professional office uses ( 3.0 ksf ) and medical office uses ( 14.0 ksf ).

Access. The site plan indicates access to Berg Street, and no access to Douglas Blvd is proposed. The Berg Street access is 230 feet north of Douglas Blvd (centerline to centerline) and 140 feet from Granite Falls Way. Full access is proposed at this location. This access is roughly opposite the driveway proposed by the office project on the west side of Berg Street.

The project would be accompanied by frontage improvements typically required under the Placer County General Plan and Granite Bay Community Plan. Frontage improvements would involve widening the east side of Berg Street to Placer County's Plate 116 standard approach configuration.



## EXISTING SETTING

## Roadways / Intersections

Existing roadways serving this portion of Granite Bay are discussed below.
Douglas Boulevard is a major east-west arterial roadway extending from Vernon Street in Roseville across Interstate 80 through Roseville and into Placer County to Folsom Lake. Douglas Blvd is a six lane facility from Interstate 80 east to Sierra College Blvd through the City of Roseville. Douglas Blvd transitions to a 4-lane divided roadway with left turn channelization east of Sierra College Blvd into the unincorporated community of Granite Bay. The 4-lane section extends past the project site east to Auburn-Folsom Road, and east of Auburn-Folsom Road, Douglas Blvd continues as a 2-lane undivided roadway to the Folsom Lake recreational area. Douglas Blvd is designated a "Scenic" Roadway in the Granite Bay Community Plan Circulation Element.

Access to Douglas Blvd is controlled in many places. A 20' landscaped median exists on Douglas Blvd in the vicinity of the site. Eastbound and westbound left turn lanes are provided at the Berg Street intersection, but a raised median prohibits left turns or through traffic across Douglas Blvd. The posted speed limit on Douglas Blvd is 55 mph .

Daily traffic volume counts conducted in May 2017 indicate that the volume of traffic on Douglas Blvd varies along its length. Immediately east of the Sierra College Blvd intersection the roadway carried about 47,564 vehicles per day. The volume decreased to 40,789 east of Joe Rodgers Road.

Sierra College Blvd is a major north-south arterial roadway that links the Granite Bay area with Sacramento County to the south and with the Roseville - Rocklin area to the north. In the area of the proposed project Sierra College Blvd is a six lane facility that drops to four lanes in the area north of Olympus Drive.

The Douglas Blvd/ Sierra College Blvd intersection is controlled by a traffic signal. Each roadway has three through travel lanes in each direction, along with dual left turn lanes. Separate right turn lanes exist on the south, east and west legs of the intersection.

Woodgrove Way - Quail Oaks Drive are local / collector streets that intersect Douglas Blvd west of the project site. Quail Oaks Drive provides access to an existing residential neighborhood north of Douglas Blvd. Woodgrove Way extends south from Douglas Blvd to Greyhawk Drive, which in turn extends south to an intersection on Eureka Blvd. The Woodgrove Way-Greyhawk Drive route is the only link between Douglas Blvd and Eureka Road in the area from Sierra College Blvd to Barton Road. The posted speed limit is 25 mph on this route.

The Douglas Blvd / Quail Oaks Drive / Woodgrove Way intersection is controlled by stop signs on the Quail Oaks Drive and Woodgrove Way approaches. Douglas Blvd has two through lanes in each direction at this intersection. A separate right turn lane is provided on the
eastbound Douglas Blvd approach, and the Douglas Blvd approaches also have separate left turn lanes that are 160 to 180 feet long. The Quail Oaks Drive and Woodgrove Way approaches are striped as single lanes, although the Woodgrove Way approach is relatively wide (i.e., 30 feet). Crosswalks are striped across the south leg of the intersection.

Seeno Avenue is a local collector street that extends north from Douglas Blvd to provide access to the Olive Ranch community in Granite Bay. This two lane road is also a route to Greenhills Elementary School. The posted speed limit on Seeno Avenue is 25 mph .

The Douglas Blvd / Seeno Avenue intersection is controlled by an actuated traffic signal. Douglas Blvd has two through lanes in each direction at the intersection. Separate left turn / uturn lanes have been created on eastbound Douglas Blvd ( 150 feet long) and on westbound Douglas Blvd ( 80 feet long). The southbound Seeno Avenue approach is a single lane. There are no striped crosswalks at this intersection.

Granite Estates Drive is a local street that extends south from Douglas Blvd to provide access to a developing office park. In the area of the project Granite Estates Drive is roughly 24 feet wide (edge of pavement to edge of pavement). The Granite Estates Drive approach to Douglas Blvd has been improved to satisfy Placer County's Plate 116 standard approach configuration for the design speed of Douglas Blvd serving a rural estate (i.e., 45 ' radius returns and 175 foot long approach taper).

The Douglas Blvd / Granite Estates Drive intersection is currently controlled by a stop sign on the northbound Granite Estates Drive approach. The median is opened and while a westbound left turn lane is provided at the Granite Estates Drive intersection, the raised median prohibits left turns or through traffic across Douglas Blvd. Douglas Blvd is wide enough to accommodate westbound to eastbound u-turns. There are no crosswalks at this intersection.

Berg Street is a two lane collector street that extends for about $1 / 2$ mile to link Douglas Blvd with Olive Ranch Road. Berg Street is designated a "Country Road" in the Granite Bay Community Plan Circulation Element. The width of Berg Street varies along its length. While the two travel lanes are about 24 feet wide, paved shoulders and intersection approach tapers extend the pavement width in many locations. The speed limit on Berg Street is 35 mph .

The Granite Bay Community Plan indicates that Berg Street carried 700 vehicles per day in 2001. The recent intersection counts conducted for this study indicated that during peak traffic hours Berg Street carried about 111 to 126 vehicles per hour in the area north of Douglas Blvd which is equivalent to roughly 1,200 vehicles per day.

The Douglas Blvd / Berg Street intersection is currently controlled by stop signs on the southbound Berg Street approach and the northbound approach from the existing specialty rail center. Both of these approaches are limited to right urns only. Left turn lanes exist on Douglas Blvd approaching the intersection, and Douglas Blvd is wide enough to accommodate u-turns. Both Berg Street approaches are limited to right turns. There are no crosswalks at this intersection.

Macargo Road is a two-lane local street that links Berg Street and Barton Road in the area north of Douglas Blvd.

Barton Road is a two lane north-south arterial street that intersects Douglas Blvd about $1 / 2$ mile east of Berg Street. Barton Road extends northerly to the Town of Loomis and southerly through Granite Bay to the Sacramento County line. The speed limit on Barton Road is 35 mph in the area north of Douglas Blvd.

The Douglas Blvd / Barton Road intersection is controlled by an actuated traffic signal that operates with "split" phases on Barton Road. The northbound Barton Road approach has three lanes that are configured as a left turn, thru+left turn and separate right turn lanes. The southbound has two lanes that are striped as thru+left and separate right turn lanes. Separate left turn lanes are provided on the Douglas Blvd approaches, and there is a right turn lane on the westbound approach as well. Crosswalks are striped across the Barton Road legs and the eastern Douglas Blvd leg of the intersection.

Auburn-Folsom Road is a north-south arterial street that extends from Folsom northerly through Granite Bay to Auburn. Auburn Folsom Road from Folsom to Douglas Blvd has been widened to four lanes as has the short segment north of Douglas Blvd along the existing retail frontage.

The Douglas Blvd / Auburn Folsom Road intersection is controlled by a traffic signal. The Auburn Folsom Road approach operate with split phases, and the four lane northbound approach is configured with a left turn, combined left+through lane, through lane and right turn lane. Each approach on Douglas Blvd has two through lanes and separate left turn and right turn lanes, and the eastbound right turn lane is separated from the traffic signal control. Crosswalks are striped across each leg of the intersection.

The Barton Road / Eureka Road intersection is controlled by an all-way stop. Three approaches have single lanes, but the southbound approach has a separate right turn lane.

## Level of Service

Intersection Methodology. To assess the quality of existing traffic conditions and provide a basis for evaluating project impacts, Levels of Service were calculated for study area intersections. "Level of Service" (LOS) is a qualitative measure of traffic operating conditions whereby a letter grade, "A" through "F", corresponding to progressively worsening traffic operating conditions, is assigned to an intersection or roadway segment. The characteristics associated with the various Levels of Service are presented in the Appendix.

Various procedures are available for calculating Level of Service. Current operations at intersections and at project driveways were assessed using the procedures contained in the Highway Capacity Manual, $6^{\text {th }}$ Edition. Evaluation of both signaled and un-signalized intersection Level of Service is linked to the overall intersection Level of Service. Table 1 identifies the typical characteristics of intersection Level of Service grades. At un-signalized intersection Level of Service is supplemented by consideration of the need for traffic signals based on the Traffic Signal Warrant criteria published in the California Manual of Uniform

Traffic Control Devices (MUTCD). Peak hour traffic volume warrants have been used to identify needed improvements and/or confirm the significance of impacts at unsignalized locations.

| TABLE 1 <br> LEVEL OF SERVICE DEFINITIONS |  |  |  |
| :---: | :---: | :---: | :---: |
| Level of Service | Signalized Intersection | Unsignalized Intersection | Roadway (Daily) |
| "A" | Uncongested operations, all queues clear in a single-signal cycle. <br> Average Delay $\leq 10$ seconds per vehicle | Little or no delay. Average Delay $\leq 10 \mathrm{sec} / \mathrm{veh}$ | Completely free flow. |
| "B" | Uncongested operations, all queues clear in a single cycle. Delay $>10 \mathrm{sec} / \mathrm{veh}$ and $\leq 20 \mathrm{sec} / \mathrm{veh}$ | Short traffic delays. <br> Delay $>10 \mathrm{sec} / \mathrm{veh}$ and <br> $\leq 15 \mathrm{sec} / \mathrm{veh}$ | Free flow, presence of other vehicles noticeable. |
| "C" | Light congestion, occasional backups on critical approaches. Delay $>20 \mathrm{sec} / \mathrm{veh}$ and $<35 \mathrm{sec} / \mathrm{veh}$ | Average traffic delays. Delay $>15 \mathrm{sec} / \mathrm{veh}$ and $\leq 25 \mathrm{sec} / \mathrm{veh}$ | Ability to maneuver and select operating speed affected. |
| "D" | Significant congestions of critical approaches but intersection functional. Cars required to wait through more than one cycle during short peaks. No long queues formed. Delay $>35 \mathrm{sec} / \mathrm{veh}$ and $<55 \mathrm{sec} / \mathrm{veh}$ | Long traffic delays. <br> Delay $>25$ sec/veh and $\leq 35 \mathrm{sec} / \mathrm{veh}$ | Unstable flow, speeds and ability to maneuver restricted. |
| "E" | Severe congestion with some long standing queues on critical approaches. Blockage of intersection may occur if traffic signal does not provide for protected turning movements. Traffic queue may block nearby intersection(s) upstream of critical approach(es). Delay $>55 \mathrm{sec}$ and $\leq 80 \mathrm{sec} / \mathrm{veh}$ | Very long traffic delays, failure, extreme congestion. <br> Delay $>35 \mathrm{sec} / \mathrm{veh}$ and $\leq 50 \mathrm{sec} / \mathrm{veh}$ | At or near capacity, flow quite unstable. |
| "F" | Total breakdown, stop-and-go operation. Delay > $80 \mathrm{sec} / \mathrm{veh}$ | Intersection often blocked by external causes. <br> Delay $>50 \mathrm{sec} / \mathrm{veh}$ | Forced flow, breakdown. |
| Sources: Highway Capacity Manual, $6^{\text {th }}$ Edition, and Transportation Research Board (TRB) Special Report 209. |  |  |  |

Placer County General Plan Methodology for Evaluating Roadway Segment Level of Services. The Placer County General Plan presents daily traffic volume levels that are to be indicative of Levels of Service on arterial streets. These volume thresholds are shown in Table 2.

| TABLE 2 <br> PLACER COUNTY EVALUATION CRITERIA FOR <br> ROADWAY SEGMENT LEVEL OF SERVICE |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Roadway Capacity Class | Maximum Daily Traffic Volume Per Lane <br> Level of Service |  |  |  |  |
|  | A | B | C | D | E |
|  | 6,300 | 10,620 | 13,680 | 17,740 | 18,000 |
| 3. Freeway - Mountainous Terrain | 5,290 | 8,920 | 11,650 | 14,070 | 15,120 |
| 4. Arterial - High Access Control | 3,400 | 5,740 | 7,490 | 9,040 | 9,720 |
| 5. Arterial - Moderate Access Control | 6,000 | 7,000 | 8,000 | 9,000 | 10,000 |
| 6. Arterial - Low Access Control | 5,400 | 6,300 | 7,200 | 8,100 | 9,000 |
| 7. Rural 2-lane Highway - Level Terrain | 4,500 | 5,250 | 6,000 | 6,870 | 7,500 |
| 8. Rural 2-lane Highway - Rolling Terrain | 1,500 | 2,950 | 4,800 | 7,750 | 12,500 |
| 9. Rural 2-lane Highway - Mountainous Terrain | 800 | 2,100 | 3,800 | 5,700 | 10,500 |
| Source: Placer County General Plan FEIR | 400 | 1,200 | 2,100 | 3,400 | 7,000 |

Standards of Significance. Minimum acceptable Level of Service standards within this area of Placer County are defined by the Granite Bay Community Plan. The Community Plan notes that the Level of Service (LOS) on major roadways (i.e., arterial and collector routes) and intersections shall be at Level C or better during the a.m. and/or p.m. peak hour. The exceptions to this are intersections along Auburn-Folsom from Douglas Blvd southerly and along Douglas Blvd from Auburn-Folsom Road westerly, where the Level of Service shall be LOS E or better during the a.m. and/or p.m. peak hour. Based on this guidance, LOS E is the minimum Level of Service at intersections on Douglas Blvd in the area of the proposed project, and LOS C is the minimum elsewhere.

Placer County has adopted a methodology for determining the significance of traffic impacts within the context of the Level of Service goals established by the General Plan and local community plans. This methodology is noted below.

## Roadway Segment Assessment Methodology:

A project may be considered to exceed the minimum LOS policies if;

1) A roadway segment operating at or above the established Placer County policy without the project will decrease to an unacceptable LOS with the project; or
2) A roadway segment currently operating below the applicable established policy will experience an increase in V/C (volume to capacity) ratio of 0.05 or greater; or
3) A roadway segment operating below the established acceptable LOS policy experiences an increase in ADT of 100 or more project generated trips, per lane.

## Signalized Intersection Assessment Methodology:

A project may be considered to exceed the minimum LOS policies if;

1) An intersection operating at or above the established Placer County policies without the project will decrease to an unacceptable LOS with the project; or
2) An intersection currently operating below the acceptable LOS established policy will experience an increase in V/C (volume to capacity) ratio of 0.05 or greater; or
3) An intersection currently operating below the acceptable LOS policy will experience an increase in overall average intersection delay of 4 seconds or greater.

## Un-signalized Intersection Assessment Methodology:

A project may be considered to exceed the minimum LOS policies if;

1) An all-way stop or side-street controlled intersection which currently operates at or above the established Placer County policies without the project will deteriorate to an unacceptable LOS with the project and cause the intersection to meet MUTCD traffic signal warrants; or
2) An all-way stop or side-street controlled intersection which currently operates below the acceptable LOS established policy and meets MUTCD signal warrants will experience an increase of 2.5 seconds or more with the project.

Further consideration will be given in situations where the existing level of service is just above or at the approved minimum level of service and any increase in vehicle trips, or even daily fluctuations in traffic, will deteriorate the level of service to an unacceptable level. In such cases, it may be determined by the County that part (2) or (3) of the above exceptions is more applicable and should be used to analyze a proposed project's impacts.

Notes:
(1) Applicable MUTCD signal warrants to be determined in consultation with DPW Transportation Staff.
(2) Intersection Delay for all-ways stop control intersections to be defined as "overall intersection delay" Intersection delay for side-street stop intersections to be defined as the "overall weighted average delay for movements yielding the ROW."

## Existing Levels of Service

Intersections. Figure 3 displays existing a.m. and p.m. peak hour traffic volumes at study area intersections identified through traffic counts conducted on May 18, 2017 at all intersections, with the exception of counts at the Douglas Blvd / Granite Estates intersection which we conducted on February 1, 2018. Existing Levels of Service at study intersections were then calculated, delays were rounded to the nearest 0.5 seconds, and the results are summarized in Table 3.

As indicated in Table 3, Levels of Service can be calculated for all of the movements through an intersection where motorists are required to yield right of way. The signalized study intersections operate with overall Levels of Service that satisfy the GBCP's minimum LOS E policy. Two un-signalized intersections operate with overall Levels of Service that exceed the minimum standard. The Douglas Blvd / Woodgrove Way / Quail Oaks Drive intersection operates at LOS F in both the a.m. and p.m. peak hours, and the Barton Road / Eureka Road intersection operates at LOS F in the a.m. peak hour. The Douglas Blvd / Woodgrove Way / Quail Oaks Drive intersection satisfies peak hour warrants in the a.m. peak hour. The Barton Road / Eureka Road intersection carries traffic volumes that satisfy MUTCD peak hour warrants in the a.m. peak hour.

The Granite Bay Community Plan (Table 9.6.3) suggests that two new traffic signals may eventually be needed on Douglas Blvd based on projected traffic volumes but which the community has expressed a desire to avoid. These signals are at the Douglas Blvd / Woodgrove Way / Quail Oaks Drive and Douglas Blvd / Berg Street intersections. The reason that these signals are not desired is that they would impede the free-flow of traffic, potentially resulting in through traffic diverting from Douglas Blvd to other less desirable through routes. In other words, any additional delays along Douglas Blvd may cause through traffic to divert to parallel routes. By keeping Douglas Blvd more free-flowing, through traffic is less likely to divert to other roadways on which through traffic is to be discouraged. The Granite Bay Community Plan further states that these signals should be implemented only to correct identified safety or traffic operational problems and only after other measures have been explored and either implemented or rejected.

In response to current traffic volumes and Community Plan goals and policies, Placer County installed raised medians through the Berg Street intersection that eliminated left turns onto Douglas Blvd as well as cross traffic between Berg Street and the business on the south side of the street. With these restrictions, current traffic volumes at the Berg Street intersection do not reach the level that would satisfy peak hour traffic signal warrants.

| TABLE 3EXISTING PEAK HOUR INTERSECTION LEVELS OF SERVICE |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Intersection | Control | AM Peak Hour |  | PM Peak Hour |  |
|  |  | LOS | Average Delay ( $\mathrm{sec} / \mathrm{veh}$ ) | LOS | Average Delay (sec/veh) |
| Douglas Blvd / Sierra College Blvd | Signal | D | 43.0 | E | 60.0 |
| Douglas Blvd / Woodgrove Way (overall) <br> Eastbound left turn <br> Westbound left turn <br> Northbound left+thru+right turn Southbound left+thru+right turn | NB/SB Stop | $\begin{gathered} \text { (F) } \\ \text { C } \\ \text { B } \\ \text { F } \\ \text { E } \end{gathered}$ | $\begin{gathered} \mathbf{( 6 3 . 0})^{*} \\ 20.0 \\ 14.5 \\ 155.5 \\ 42.5 \end{gathered}$ | $\begin{gathered} (\mathbf{F}) \\ \mathrm{C} \\ \mathrm{C} \\ \mathrm{~F} \\ \mathrm{~F} \end{gathered}$ | $\begin{gathered} (\mathbf{1 2 0 . 5}) \\ 18.0 \\ 20.5 \\ 315.5 \\ 149.5 \end{gathered}$ |
| Douglas Blvd / Seeno Avenue | Signal | A | 6.5 | A | 7.0 |
| Douglas Blvd / Granite Estates Drive (overall) <br> Westbound left turn Northbound right turn | NB Stop | $\begin{gathered} \text { (C) } \\ \text { B } \\ \text { C } \\ \hline \end{gathered}$ | $\begin{gathered} (16.0) \\ 14.5 \\ 17.0 \\ \hline \end{gathered}$ | $\begin{gathered} \text { (C) } \\ \text { C } \\ \text { C } \end{gathered}$ | $\begin{gathered} (23.5) \\ 19.5 \\ 24.5 \end{gathered}$ |
| Douglas Blvd / Berg Street (overall) <br> Eastbound left turn Westbound left turn Northbound right turn Southbound right turn | NB/SB Stop | $\begin{gathered} \text { (C) } \\ \text { C } \\ \text { B } \\ \text { B } \\ \text { C } \\ \hline \end{gathered}$ | $\begin{gathered} (20.0) \\ 20.0 \\ 13.0 \\ 14.5 \\ 23.5 \\ \hline \end{gathered}$ | $\begin{gathered} \text { (C) } \\ \text { C } \\ \text { C } \\ \text { C } \\ \text { C } \\ \hline \end{gathered}$ | $\begin{gathered} (19.0) \\ 18.0 \\ 19.0 \\ 20.0 \\ 20.0 \\ \hline \end{gathered}$ |
| Douglas Blvd / Barton Road | Signal | D | 39.0 | D | 42.5 |
| Douglas Blvd / Auburn - Folsom Road | Signal | D | 39.0 | D | 36.0 |
| Barton Road / Eureka Road | All-way Stop | F | 52.5* | C | 24.0 |
| (*) am peak hour volumes satisfy MUTCD peak hour warrants <br> BOLD values exceed the minimum LOS standard |  |  |  |  |  |



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EXISTING TRAFFIC VOLUMES AND LANE CONFIGURATIONS

Roadway Segments Level of Service based on General Plan Standards. Current Daily Traffic volumes have been employed to identify roadway segment Levels of Service based on Placer County General Plan thresholds. As indicated in Table 4, the four lane segments of Douglas Blvd from Sierra College Blvd to Auburn Folsom Road carry traffic volumes that are indicative of LOS F conditions.

| TABLE 4EXISTING ROADWAY SEGMENT LEVELS OF SERVICE |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Roadway | Location | Class | Lanes | Existing Conditions |  |
|  |  |  |  | Daily Volume | Level of Service |
| Douglas <br> Blvd | Sierra College Blvd to Cavitt Stallman Rd | Arterial Moderate | 4 | 47,570 | F |
|  | Cavitt Stallman Rd to Seeno Avenue | Arterial High | 4 | 46,830 | F |
|  | Seeno Avenue to Barton Road | Arterial High | 4 | 44,800 | F |
|  | Barton Rd to Auburn Folsom Rd | Arterial High | 4 | 42,630 | F |
| Berg Street | Olive Ranch Rd to Douglas Blvd | Arterial Low | 2 | 1,200 | A |

BOLD values exceed the minimum LOS standard of the GBCP

## Planned Improvements / Funding Sources

SPRTA. As a road of regional importance, improvements to Sierra College Blvd are important to both local residents and to the greater South Placer County public. While not uniformly endorsed, a mechanism has been created to accumulate funds towards the cost of installing improvements and to assign responsibility for longer term projects.

Placer County and the cities of Lincoln, Rocklin and Roseville have joined to form the South Placer Regional Transportation Authority (SPRTA). SPRTA is a Joint Powers Authority (JPA) formed for the purpose of implementing a Regional Transportation and Air Quality Mitigation Fee to fund specified regional transportation projects.

SPRTA funding is directed towards projects such as Placer Parkway, Sierra College Blvd widening, Lincoln Bypass, I-80 / Douglas Blvd interchange, SR 65 widening, I-80 / Rocklin Road interchange, Auburn Folsom Road widening and HOV lanes on Interstate 80 through Roseville.

Placer County Traffic Impact Fee Program and CIP. In April 1996, the Placer County Board of Supervisors adopted the Countywide Traffic Impact Fee Program, requiring new development within the County to mitigate impacts to the roadway system by paying traffic impact fees. The fees collected through this program, in addition to other funding sources, make it possible for the County to construct roads and other transportation facilities and improvements needed to accommodate new development. The fee was updated by Placer County in July 2016. The County's fee program and Capital Improvement Program is divided into eleven districts, and the Quarry Ridge Project site is included in the Granite Bay Benefit District.

The Granite Bay Benefit District includes funds for improvements to the Barton Road / Eureka Road intersection where a traffic signal or roundabout is anticipated.

## Existing Pedestrian, Bicycle and Transit Facilities

Sidewalks. The GBCP Circulation Element notes that Scenic and Country Roadways normally do not have sidewalks or curbs and gutters, although there are exceptions to this such as Douglas Boulevard and in areas where parcel sizes are less than 0.9 acres. Meandering paths of a native material and paved shoulders take the place of sidewalks. Streetlights are kept to a minimum and are generally only provided at major intersections or where specific significant safety issues make lighting essential.

Today sidewalks exist along the north side of Douglas Blvd from Berg Street west to Roseville. Sidewalks are generally available east of Berg Street but there are short gaps where development has not occurred and sidewalks have not yet been installed. Designated pedestrian crossings on Douglas Blvd are limited. Crosswalks exist at signalized intersections east of the project at Barton Road and at Seeno Avenue, but those locations are at least $1 / 2$ mile from the project. Under the California Vehicle Code (CVC) legal pedestrian crossings exist at public road intersections such as Douglas Blvd / Berg Street even though the crossing is not marked.

Bicycles and Trails. Trails and bikeways within the GBCP are classified as follows:

- Class I Bikeway (Bike Path) provides a completely separated facility designed for the exclusive use of cycles and pedestrians with minimal crossflows by motorists. Motorized vehicles are not allowed on Class I Bike Paths. Class I bikeways should have a minimum 8 foot width of hard surfaced pavement with 2 foot graded shoulders on either side. Class I Bike Paths that are regional in nature should have a minimum 10 foot paved width. In some cases, a wider shoulder or separated native earth pathway would provide adjacent use for equestrians and those who prefer a native trail surface. Class I Bike Paths must be at least 5 feet from the edge of a paved roadway.
- Class II Bikeway (Bike Lane) provides a restricted right-of-way designated for the exclusive or semi-exclusive use of cycles with through travel by motor vehicles or pedestrians prohibited, but with vehicle parking and crossflows by pedestrians and motorists permitted. Class II Bike Lanes generally require a 6 foot bike lane where posted speeds are greater than 40 mph with a 6 inch white stripe separating the roadway from the bike lane. Class II Bike Lanes are typically maintained as a part of the road system by the Department of Public Works.
- Class III Bikeway (Bike Route) provides a right-of-way designated by signs or permanent markings and shared with pedestrians and motorists. Roadways designated as Class III Bike Routes should have sufficient width to accommodate motorists, bicyclists, and pedestrians. Other than a street sign, there are not special markings required for a Class III Bike Route. Class III Bike Routes are typically maintained as a part of the road system by the Department of Public Works.
- Multiple Use Trails are designed to support pedestrian, cycle, and equestrian traffic. Motorized vehicles are not allowed on Multiple Use Trails. They are generally 6 feet in width but may be reduced in width to accommodate physical and easement restrictions. Depending on the stability of local soil conditions, Multiple Use Trails are constructed of native graded soil, decomposed granite (or similarly graded imported aggregate), or native soil treated with a stabilizing agent.

Existing and Planned Bicycle Facilities. Class II Bike Lanes exist on Douglas Blvd from Sierra College Blvd to Auburn-Folsom Road. A Class I Bike Trail is planned along Douglas Blvd.

Existing and Planned Trails. The intent of the trails system identified in the GBCP is to implement an interconnected system of trails and paths suitable for safe recreation as well as transportation and circulation. This is accomplished with connections between and through future development, thereby providing the feeder system for the major trails and enhancing overall connectivity of the trail system. The local trails should link to regional trails as well as to major residential areas and areas of horse populations, employment centers, park and recreation areas, schools, creek corridors and vista locations.

Today there are no trails in the immediate vicinity of the project. The GBCP Trails Plan notes that a Multi-purpose trail is planned along Berg Street from Douglas Blvd to Olive Ranch Road.

Transit. Limited transit services are provided within Granite Bay, and two adjacent jurisdictions provide transit services which influence travel patterns within Granite Bay.

Placer County Transit. There are no established transit routes in Granite Bay. The community is currently served by a demand responsive public transit system that is operated by the Consolidated Transportation Services Agency (CTSA) under contract to Placer County Transit (PCT). Service is provided Monday through Friday. The service transports patrons to the Sierra Gardens Transfer Center in the City of Roseville where linkages to other PCT routes and to Roseville Transit are available.

Western Placer Consolidated Transportation Services Agency. The Placer County Transportation Planning Agency (PCTPA) has designated the Western Placer Consolidated Transportation Service Agency as the Consolidated Transportation Service Agency (CTSA) to serve western Placer County, which includes the Granite Bay community.

As defined by California law, a CTSA is an agency that coordinates and/or provides transportation services for a particular region. This may include services for the elderly and individuals with disabilities who cannot use conventional transit services. Since June 2008, the CTSA has developed a public/private partnership (Transit Operator Working Group, Seniors First and its key partners) to run three pilot programs that are intended to serve elderly persons and persons with disabilities who are unable to use conventional public transit services.

## PROJECT IMPACTS

The traffic impacts associated with the Quarry Ridge Professional Offices project have been determined based on the projected change in operating Levels of Service accompanying the project. Project impacts have been quantified by estimating the number and directional distribution of project trips, superimposing those trips onto current traffic volumes and recalculating Levels of Service.

## Trip Generation

The number of automobile trips that will be generated by the project has been estimated through application of trip generation rates acceptable to Placer County. For regular operation of the project applicable trip generation rates were obtained from the Institute of Transportation Engineer's (ITE) publication, Trip Generation Ninth Edition, 2012, and Table 5 identifies the trip generation rates employed for this analysis.

Table 6 summarizes total regular weekday trip generation associated with development on this site as proposed. The proposed project would generate 567 daily trips with identified medical and professional office uses. Assuming the entire project was higher generating professional offices, the project would generate 43 trips in the a.m. peak hour and 73 trips during the p.m. peak hour.

| TABLE 5 <br> TRIP GENERATION RATES |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Description | ITE Category | Unit | Trips per unit |  |  |  |  |  |  |
|  |  |  | Daily | AM Peak Hour |  |  | PM Peak Hour |  |  |
|  |  |  |  | In | Out | Total | In | Out | Total |
| Typical Office Professional | 710 General Office building < 50 ksf | ksf | 18.31 | 88\% | 12\% | 2.53 | 17\% | 83\% | 4.27* |
| Medical / Dental Office | 720 Medical Dental Office Building | ksf | 36.13 | 79\% | 21\% | 2.39 | 28\% | 72\% | 3.57 |
| Single Family Residential | 210 Detached Single Family Residences | dwelling | 9.52 | 25\% | 75\% | 0.75 | 64\% | 36\% | 1.00 |
| (*) from Placer County fee program |  |  |  |  |  |  |  |  |  |


| TABLE 6 <br> TRIP GENERATION FORECASTS |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Description | Quantity |  |  |  | s per |  |  |  |
|  |  | Daily | AM Peak Hour |  |  | PM Peak Hour |  |  |
|  |  |  | In | Out | Total | In | Out | Total |
| Proposed Quarry Ridge Professional Offices |  |  |  |  |  |  |  |  |
| Professional Office | 3.20 ksf | 59 | 7 | 1 | 8 | 2 | 12 | 14 |
| Medical Offices | 14.06 ksf | 508 | 27 | 7 | 34 | 14 | 36 | 50 |
| Total | 17.0 ksf | 567 | 34 | 8 | 42 | 16 | 47 | 63 |
| 100\% Office |  |  |  |  |  |  |  |  |
| Professional Office | 17.0 ksf | 311 | 38 | 5 | 43 | 12 | 61 | 73 |
| Highlighted value used for impact analysis |  |  |  |  |  |  |  |  |

## Trip Distribution and Assignment

Distribution. The distribution of trips to and from the project site was determined by reviewing current traffic patterns in the area by considering the demographics of the Granite Bay area and through review of assumptions approved for previous traffic studies completed for projects along Douglas Blvd and review of regional traffic model results. Medical office uses would primarily serve Granite Bay area residents but both medical and professional office uses are likely to generate commute trips that could be attracted from a relatively wide region. For this analysis we have employed a distribution pattern that assumes the majority of the project's trips are oriented to the west but that a significant share will be directed to the east into Granite Bay, as shown in Figure 4 and summarized in Table 7.

| TABLE 7 <br> TRIP DISTRIBUTION |  |
| :--- | :---: |
| Direction | Percent of Total New Trips |
| West via Douglas Blvd beyond Sierra College Blvd | $40 \%$ |
| East via Douglas Blvd between Barton Rd and Auburn Folsom Rd | $7 \frac{1}{2} \%$ |
| East on Douglas Blvd beyond Auburn Folsom Road | $2 \frac{1}{2} \%$ |
| North on Barton Road | $7 \frac{1}{2} \%$ |
| South Via Auburn Folsom Road | $10 \%$ |
| South via Barton Road | $15 \%$ |
| South via Sierra College Blvd | $15 \%$ |
| South via Woodgrove Way | $2 \frac{1}{2} \%$ |
| Total | $100 \%$ |

Assignment. The assignment of project trips will reflect the access limitations that exist today on Douglas Blvd or are proposed with the project, as well as travel time along alternative routes.

Inbound traffic is direct. Motorists arriving from the east on Douglas Blvd can simply turn right onto Berg Street and then into the site at the new driveway. Trips arriving from the west on Douglas Blvd will turn left onto Berg Street and then use the new driveway. Trips from the north will simply turn left from Berg Street into the site.

However, due to the median on Douglas Blvd, leaving the site is more difficult. Trips headed west will turn from the driveway onto southbound Berg Street and the right on Douglas Blvd. Heading east is more complicated. Employees, customers and visitors destined for locations to the east can turn onto westbound Douglas Blvd and make a u-turn at the next median opening. The Granite Estates Drive median opening is 800 feet from Berg Street, or roughly 1,000 feet from the project driveway. Alternatively, exiting traffic can turn right onto Berg Street and then use Macargo Road to reach Barton Road and return to Douglas Blvd.

The choice for eastbound routes is likely to be based on distance and travel time. Measured from the driveway to the Douglas Blvd / Barton Road intersection, the Douglas Blvd route is roughly 4,500 feet as is the route via Macargo Road. Because the total distance involved on each alternative route is very similar, the probable travel time is a better indicator of the choice of routes. Accounting for delays along the way, it would take 105 seconds to reach Barton Road using the Douglas Blvd route. While the speed limits are lower, it would take about the same time to reach Douglas Blvd using Macargo Road. However, the times on each route do become different upon reaching the Barton Road intersection, as eastbound traffic on the Douglas Blvd route is more likely to catch a green indication or to face little delay when turning right onto southbound Barton Road. Alternatively, traffic southbound on Barton Road rarely arrives when the traffic signal is in green on Douglas Blvd and extra delay is likely.

Based on this comparison, it is reasonable to expect that motorists headed east on Douglas Blvd beyond Barton Road or south on Barton Road would be split between the two route. However, to provide a "worst case" assessment of impact to the Douglas Blvd / Berg Street intersection, all eastbound traffic was assumed to make a u-turn on Douglas Blvd rather than choosing Macargo Road.

The resulting assignment of trips with the proposed project is summarized in Figure 4.


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## Existing Plus Project Levels of Service

Intersections. Having identified the probable distribution and assignment of project trips, this traffic was superimposed onto current traffic volumes at study intersections and the project driveway. Figure 5 presents the sum of Existing traffic plus Project trips. These volumes were used to identify a.m. and p.m. peak hour Levels of Service, and Table 8 summarizes resulting operations with development of the project.

As shown, the addition of project trips will incrementally increase the length of delays at study intersections. At all but two locations the resulting Levels of Service will continue to satisfy the minimum LOS E standard for Douglas Blvd and minimum C standard elsewhere from the Granite Bay Community Plan. Thus, the impacts of the project are not considered to be significant under CEQA at these locations.

The project's relative impact has been considered at the two intersections where current background conditions already fail to satisfy minimum GBCP standards. The Douglas Blvd / Woodgrove Way / Quail Oaks Drive intersection operates with an overall LOS F with and without the project in the a.m. and p.m. peak hour. Because existing and baseline conditions are already deficient, the project's impact is determined based on the incremental change in overall delay and the satisfaction of traffic signal warrants. In this case, the change during the p.m. peak hour exceeds the maximum 2.5 second increment permitted under Placer County guidelines, and as is the case under existing conditions the volume of traffic at the intersection with the project reaches the level that satisfies peak hour traffic signal warrants in the a.m. peak hour. While a traffic signal might be judged to be unjustified at this location since nearly all traffic turns right, satisfaction of signal warrant volume requirements remains the impact criteria. Thus, because the project's incremental change in average delay exceeds 2.5 seconds and peak hour warrant volume requirements are met, the project's impact is significant at this location, and mitigation is required.

Mitigation. Alternative mitigations were considered. A traffic signal is not a reasonable choice since a very minimum amount of traffic turns left onto Douglas Blvd and the effects of a new signal on the overall flow of traffic on Douglas Blvd may be contrary to the goals of the GBCP. Prohibiting left turns onto Douglas Blvd and cross traffic is the most reasonable solution. Installing a raised median on Douglas Blvd to eliminate cross traffic while permitting eastbound and westbound left turns from Douglas Blvd onto Quail Oaks Drive and onto Woodgrove Way would result in the intersection operating with an overall LOS C which satisfies the minimum LOS E requirements of the Granite Bay Community Plan. This mitigation is recommended.

This measure would have the effect of diverting cross traffic and left turns to other locations, but the number of diverted vehicles is relatively small. In the a.m. peak hour five (5) northbound vehicles on Woodgrove Way and one (1) southbound vehicle on Quail Oaks Drive would be affected.

The alternative paths for diverted vehicles have been identified. Northbound traffic might logically elect to turn right and make a u-turn at the signalized Douglas Blvd / Seeno Avenue
intersection. U-turns are allowed at this location. The southbound through vehicles which today cross the street to go south on Woodgrove Way may instead turn right and make a u-turn at the Sierra College Blvd or Cavitt Stallman Road signals or use Rolling Hills Drive to access Douglas Blvd at the Seeno Avenue signal. Today westbound U-turns at the Douglas Blvd / Cavitt Stallman Road are not permitted in order to accommodate that traffic signal's existing northbound right-turn-overlap phase, and the signal would need to be modified if it were necessary to allow u-turns at this location. However, the volume of traffic diverted at all these locations would be too small to have an appreciable effect on the operation of these intersections whether Douglas Blvd access is permitted or not. Under either condition the "mitigated" Levels of Service remain within the adopted minimum LOS standard.

The extent to which the Douglas Blvd / Seeno Avenue intersection can accommodate any increased queuing in the eastbound left turn lane caused by this change has been evaluated. The existing lane provided 280 feet of storage, and with the existing 150 foot long bay taper the area available for deceleration and storage is 430 feet. The longest queue occurs in the a.m. peak hour when the $95^{\text {th }}$ percentile queue is forecast to be 100 feet. The resulting space between the queue and beginning of bay taper (i.e., 330 feet), accommodates deceleration to a stop from 4045 mph (Caltrans HDM Table 405.2B) which satisfies HDM guidelines for a 55 mph design.

The Douglas Blvd / Woodgrove Way / Quail Oaks Drive intersection will operate with an overall Level of Service of LOS C with the turn prohibitions. With this improvement the project's impact is not significant.

The Barton Road / Eureka Road intersection operates at LOS F in the a.m. peak hour with and without the project and satisfies peak hour traffic signal warrants under both scenarios. The change in overall delay is the significance criteria under adopted Methodology of Assessment. Because the project adds traffic to approaches that experience lower individual delay, the overall delay at the intersection is reduced. In this case, the a.m. peak hour delay does not increase by more than the 2.5 second increment permitted under the Methodology of Assessment, the project's impact is not significant, and mitigation is not required.

Roadway Segments. Table 9 identifies the project's daily traffic volume contribution to study area roads and resulting Levels of Service. As indicated while the project will not change the Level of Service occurring on any roadway segment, the project will add traffic to roadways that already are deficient based on General Plan thresholds. In this case the significance of project impact is based on the criteria included under Placer County Methodology of Assessment, and the project contribution has been evaluated accordingly.

The project's incremental change can be described in terms of its change in roadway volume / capacity ratio. In this case, the project's contribution to Douglas Blvd ranges from 0.003 to 0.009 . As these changes are less than the 0.050 increment permitted under Placer County methodology, the project's impact is not significant under this metric.

The second criteria is the "vehicles per lane" (vpl) traffic increase. In this case, the project adds 28 to 85 vpl at various locations on Douglas Blvd. Because these increments do not exceed the 100 vpl threshold permitted under Placer County methodology, the project's impact is not significant.


EXISTING PLUS PROJECT

| TABLE 8EXISTING PLUS PROJECT PEAK HOUR INTERSECTION LEVELS OF SERVICE |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Intersection | Control | AM Peak Hour |  |  |  | PM Peak Hour |  |  |  |
|  |  | Existing |  | Existing Plus Project |  | Existing |  | Existing Plus Project |  |
|  |  | LOS | Average Delay (sec/veh) | LOS | Average Delay (sec/veh) | LOS | Average Delay (sec/veh) | LOS | Average Delay (sec/veh) |
| Douglas Blvd / Sierra College Blvd | Signal | D | 43.0 | D | 43.0 | E | 60.0 | E | 60.0 |
| Douglas Blvd / Woodgrove Way (overall) <br> Eastbound left turn Westbound left turn Northbound left+thru+right turn Southbound left+thru+right turn | NB/SB Stop | $\begin{gathered} (\mathbf{F}) \\ \text { C } \\ \text { B } \\ \text { F } \\ \text { E } \\ \hline \end{gathered}$ | $\begin{gathered} \mathbf{( 6 3 . 0})^{*} \\ 20.0 \\ 14.5 \\ 155.5 \\ 42.5 \\ \hline \end{gathered}$ | $\begin{gathered} (\mathbf{F}) \\ \mathrm{C} \\ \mathrm{~B} \\ \mathrm{~F} \\ \mathrm{E} \\ \hline \end{gathered}$ | $\begin{gathered} (64.5) * \\ 20.0 \\ 14.5 \\ 153.5 \\ 46.5 \\ \hline \end{gathered}$ | $\begin{gathered} (\mathbf{F}) \\ \mathrm{C} \\ \mathrm{C} \\ \mathrm{~F} \\ \mathrm{~F} \\ \hline \end{gathered}$ | $\begin{gathered} (\mathbf{1 2 0 . 5}) \\ 18.0 \\ 20.5 \\ 315.5 \\ 149.5 \\ \hline \end{gathered}$ | $\begin{gathered} (\mathbf{F}) \\ \mathrm{C} \\ \mathrm{C} \\ \mathrm{~F} \\ \mathrm{~F} \\ \hline \end{gathered}$ | $\begin{gathered} \mathbf{( 1 2 3 . 5 )} \\ 18.5 \\ 20.5 \\ 315.5 \\ 150.0 \\ \hline \end{gathered}$ |
| Douglas Blvd / Seeno Avenue | Signal | A | 6.5 | A | 6.5 | A | 7.0 | A | 7.0 |
| Douglas Blvd / Granite Estates Drive <br> (overall) <br> Westbound left turn <br> Northbound right turn | NB Stop | $\begin{gathered} \text { (C) } \\ \text { B } \\ \text { C } \\ \hline \end{gathered}$ | $\begin{gathered} (16.0) \\ 14.5 \\ 17.0 \\ \hline \end{gathered}$ | $\begin{gathered} \text { (C) } \\ \text { B } \\ \text { C } \\ \hline \end{gathered}$ | $\begin{gathered} (16.0) \\ 14.5 \\ 17.0 \\ \hline \end{gathered}$ | $\begin{gathered} \text { (C) } \\ \text { C } \\ \mathrm{C} \\ \hline \end{gathered}$ | $\begin{gathered} (23.5) \\ 19.5 \\ 24.5 \\ \hline \end{gathered}$ | $\begin{gathered} \text { (C) } \\ \text { C } \\ \mathrm{C} \\ \hline \end{gathered}$ | $\begin{gathered} (23.0) \\ 21.0 \\ 25.0 \\ \hline \end{gathered}$ |
| Douglas Blvd / Berg Street (overall) <br> Eastbound left turn Westbound left turn Northbound right turn Southbound right turn | NB/SB Stop | $\begin{gathered} \text { (C) } \\ \text { C } \\ \text { B } \\ \text { B } \\ \mathrm{C} \end{gathered}$ | $\begin{gathered} (20.0) \\ 20.0 \\ 13.0 \\ 14.5 \\ 23.5 \\ \hline \end{gathered}$ | $\begin{gathered} \text { (C) } \\ \text { C } \\ \text { B } \\ \text { B } \\ \text { C } \end{gathered}$ | $\begin{gathered} (20.5) \\ 20.0 \\ 13.0 \\ 14.5 \\ 24.5 \\ \hline \end{gathered}$ | $\begin{gathered} \text { (C) } \\ \text { C } \\ \text { C } \\ \text { C } \\ \text { C } \end{gathered}$ | $\begin{gathered} (19.0) \\ 18.0 \\ 19.0 \\ 20.0 \\ 20.0 \\ \hline \end{gathered}$ | $\begin{gathered} \text { (C) } \\ \text { C } \\ \text { C } \\ \text { C } \\ \text { C } \end{gathered}$ | $\begin{gathered} (21.5) \\ 18.0 \\ 19.0 \\ 20.0 \\ 25.0 \\ \hline \end{gathered}$ |
| Douglas Blvd / Barton Road | Signal | D | 39.0 | D | 39.5 | D | 42.5 | D | 45.0 |
| Douglas Blvd / Auburn - Folsom Road | Signal | D | 39.0 | D | 39.0 | D | 36.0 | D | 36.0 |
| Barton Road / Eureka Road | All-way Stop | F | 52.5* | F | 51.5* | C | 24.0 | C | 25.0 |
| Berg Street / Access <br> (overall) <br> Southbound left turn Westbound left+right turn | WB Stop | - | - | (A) <br> A <br> A | $\begin{gathered} (8.5) \\ 7.5 \\ 9.5 \\ \hline \end{gathered}$ | - | - | (A) <br> A <br> A | $\begin{gathered} (9.5) \\ 7.5 \\ 9.5 \\ \hline \end{gathered}$ |
| (*) a.m. peak hour volumes satisfy MUTCD peak hour warrants |  |  |  |  |  |  |  |  |  |

## TABLE 9

EXISTING PLUS PROJECT ROADWAY SEGMENT LEVELS OF SERVICE

| Roadway | Location | Classification | Lanes | Existing Conditions |  | Existing Plus Quarry Ridge Conditions |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Daily Volume | Level of Service | Daily Volume |  | $\begin{gathered} \text { Level } \\ \text { of } \\ \text { Service } \end{gathered}$ | Change in V/C |
|  |  |  |  |  |  | Project Alone | Total |  |  |
| Douglas Blvd | Sierra College Blvd to Cavitt Stallman Rd | Arterial Moderate | 4 | 47,570 | F | 320 | 47,890 | F | 0.009 |
|  | Cavitt Stallman Rd to Seeno Avenue | Arterial High | 4 | 46,830 | F | 320 | 47,150 | F | 0.008 |
|  | Seeno Avenue to Berg Street | Arterial High | 4 | 44,800 | F | 340 | 45,140 | F | 0.009 |
|  | Berg Street to Barton Road | Arterial High | 4 | 44,800 | F | 190 | 44,990 | F | 0.005 |
|  | Barton Road to Auburn Folsom Road | Arterial High | 4 | 42,630 | F | 110 | 42,540 | F | 0.003 |
| Berg Street | Olive Ranch Road to Project | Arterial Low | 2 | 1,200 | A | 40 | 1,240 | A | 0.003 |
|  | Olive Ranch Road to Douglas Blvd | Arterial Low | 2 | 1,200 | A | 530 | 1,730 | A | 0.035 |

## DOUGLAS BLVD ACCESS DESIGN

## Key Issues

Three issues have been evaluated with regards to the project's impact on the local traffic operations on Douglas Blvd in the area of the Granite Drive and Berg Street intersections.

Weaving Across Douglas Blvd. To travel easterly on Douglas Blvd motorists leaving the site will need to turn right onto Douglas Blvd and then use the Granite Estates Drive left turn lane to make a u-turn. The Berg Street intersection is roughly 840 feet from the Granite Estates Drive median break. To use the opening for u-turns, exiting motorists will initially accelerate and then decelerate into the turn pocket. The distance traveled and speed achieved during acceleration and deceleration has been determined from AASHTO guidelines. Table 10 shows the relationship between the available distance from the Berg Street intersection to the end of the left turn lane at Granite Estates Drive as well as the estimated speed achieved by a motorist making the maneuver in this distance. As shown, if there was no queue in the left turn lane, then an exiting motorist could accelerate to $44-45 \mathrm{mph}$ on eastbound Douglas Blvd before slowing to stop in the empty turn lane. If another vehicle was waiting to turn, then the total length would be reduced by 25 feet and the maximum speed would be reduced slightly (i.e., 43-44 mph). In comparison the design speed on Douglas Blvd is 55 mph . so the speed differential is 11 to 12 mph.

The adequacy of this layout is based on the relative difference in speed between weaving and through traffic, as well as the characteristics of traffic flow. Placer County has accepted guidance from the Caltrans Highway Design Manual (HDM) Section 4 which describes the permitted speed differential between decelerating and through traffic at turn lanes. The HDM notes that a differential of up to 20 mph can be accepted. Placer County also considers the relative availability of gaps in through traffic created by up-stream traffic signals.

In this case, because the speed differential is less than 20 mph and the traffic signal at Barton Road is observed to create gaps in westbound traffic the available weaving distance is considered to be adequate.

Weaving across eastbound Douglas Blvd from driveways that are closer to the intersections can be more problematic. For example the speed of motorists leaving the Lake Center driveways and headed eastbound to the Berg Street left turn lane could be much less. The driveway for the nursery west of Berg Street is at the beginning of the westbound left turn lane approaching Granite Estates Drive. Motorists cross Douglas Blvd and enter the turn lane at $10-15 \mathrm{mph}$.

Weaving across eastbound Douglas Blvd was contemplated in the traffic studies for the Little Sunshine Pre-School and Granite Estates Professional Center on the south side of Douglas Blvd, and improvements have been installed in the area between Granite Estates Drive and Berg Street. The Granite Estates Drive intersection is roughly 840 feet from the next median break on Douglas Blvd at Berg Street. If there was no queue in the left turn lane at Berg Street, then an exiting motorist could accelerate to $44-45 \mathrm{mph}$ on Douglas Blvd before slowing to stop in the empty turn lane. If another vehicle was waiting to turn, then the total length would be reduced
by 25 feet and the maximum speed would be reduced slightly (i.e., $43-44 \mathrm{mph}$ ). In comparison the design speed on Douglas Blvd is 55 mph . Based on the distance from Granite Estates Drive to Berg Street, weaving across the lanes should not be a problem.

| TABLE 10 |  |  |  |
| :--- | :---: | :---: | :---: |
| SPEED REACHED FROM ACCESS TO U-TURN |  |  |  |
| Location | Distance <br> Traveled | Maximum Speed <br> Reached |  |
| Eastbound on Douglas Blvd from Granite Estates Drive to Berg Street | 800 | $44-45 \mathrm{mph}$ |  |
| Westbound on Douglas Blvd from Berg Street to Granite Estates Drive | 800 | $44-45 \mathrm{mph}$ |  |
| Source: Exhibit 2-24 and 2-25 AASHTO A Policy on Geometric Design of Highways and Streets, 2012 |  |  |  |

Queuing in Left Turn Lanes. Existing, approved and proposed businesses along Douglas Blvd take access via median openings that are preceded by left / u-turn lanes. The adequacy of these lanes is related to two factors: 1) storage for waiting vehicles, and 2) room for deceleration outside of the flow of through traffic on Douglas Blvd.

To put this issue in perspective, Table 11 identifies the length of left turn lanes and bay tapers at all of the un-signaled locations on Douglas Blvd from the Cavitt Stallman Road intersection to Auburn Folsom Road. The entry speed at the beginning of the bay taper is also presented based on HDM Table 406.3B, which is noted in Table 12. The calculation assumes that no vehicles are queued in the left turn lane.

It is important to note that the length of every un-signalized left turn pocket on Douglas Blvd falls below the design threshold for full deceleration from 55 mph to a stop (i.e., 485 feet), and some slowing in the adjoining travel lanes on Douglas Blvd is required.

| TABLE 11 <br> CONFIGURATION OF EXISTING UN-SIGNALIZED LEFT TURN LANES ON DOUGLAS BLVD |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\begin{gathered} \text { Dimensions } \\ \text { (feet) } \\ \hline \end{gathered}$ |  |  | Entry |
| Direction | Location | Bay Taper | Left Turn Lane | Total | $\begin{gathered} \text { Speed(*) } \\ \text { (mph) } \\ \hline \end{gathered}$ |
| Eastbound | Quail Oaks Drive | 150 | 160 | 310 | 40 |
|  | Kingsgate Drive | 150 | 150 | 300 | 39 |
|  | Douglas Ranch Drive | 200 | 200 | 400 | 47 |
|  | Bushnell Gardens Nursery | 145 | 110 | 255 | 33 |
|  | Berg Street | 125 | 300 | 425 | 49 |
|  | Church | 150 | 160 | 300 | 39 |
|  | Plaza Del Lago | 120 | 140 | 260 | 33 |
|  | Joe Rogers Road | 130 | 120 | 250 | 32 |
|  | Shady Lane | 130 | 170 | 300 | 39 |
|  | Granite Bay Library | 120 | 90 | 210 | 27 |
|  | Dover Drive | 120 | 110 | 230 | 30 |
|  | Granite Cove Drive | 120 | 120 | 240 | 30 |
|  | Christy Lane | 120 | 160 | 280 | 35 |
|  | Rear entrance to Raley's SC | 70 | 50 | 120 | 20 |
|  | Raley's SC | 60 | 120 | 180 | 25 |
|  | Raley's SC | 50 | 120 | 170 | 25 |
| Westbound | Christy Lane | 60 | 60 | 120 | 20 |
|  | Arabian Circle | 130 | 110 | 240 | 30 |
|  | Berg Street | 110 | 340 | 450 | 52 |
|  | Granite Estates Drive | 120 | 230 | 350 | 43 |
|  | Kingsgate Drive | 100 | 80 | 180 | 25 |
|  | Woodgrove Way | 100 | 180 | 280 | 35 |
| (*) entry speed per HDM with no vehicles in queue |  |  |  |  |  |


| TABLE 12 |  |
| :---: | :---: |
| HDM DECELERATION STANDARDS |  |\(\left|\begin{array}{c}Deceleration Lane Length <br>


(feet)\end{array}\right|\)| Design Speed | 235 |
| :---: | :---: |
| 25 | 275 |
| 30 | 315 |
| 35 | 375 |
| 40 | 435 |
| 45 | 485 |
| 50 | 530 |
| 55 |  |
| 60 |  |

Design Parameters. Tables 13 and 14 identify the volume of traffic anticipated in the existing Douglas Blvd left turn lanes in the immediate area of the proposed project. These tables note the length of storage available in each lane and the peak hour design queue length. The length of queue anticipated in the left turn lanes has been estimated from two standpoints. First, the queue length is identified as a byproduct of Level of Service analysis. Secondly, the storage recommended in the Highway Design Manual (HDM) has been identified. The HDM suggests that un-signalized left turn lanes provide storage equivalent to a two-minute accumulation of peak hour vehicles. However, because the gap in traffic needed for u-turns is longer than for left turns, this analysis assumes a three-minute accumulation for u-turns and a two minute accumulation for left turns. In each case a waiting vehicle is assumed to occupy 25 feet.

The HDM also contains recommended distances for deceleration lane planning. Table 16 presents these recommendations. It is important to note that some deceleration in the adjoining through travel lanes is permitted prior to the bay taper. The HDM indicates that up to 20 mph deceleration prior to the bay taper can be acceptable.

| TABLE 13 <br> DOUGLAS BLVD MEDIAN OPENING ASSESSMENT <br> GRANITE ESTATES DRIVE WESTBOUND LEFT TURN LANE |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Condition | StorageLength(feet) | Time Period | Westbound at Granite Estates Dr |  |  |  |
|  |  |  | Volume |  | Queue (feet) |  |
|  |  |  | U-turn | Left | HCM | HDM |
| Existing | 230 | AM | 10 | 6 | <25 | <25 |
|  |  | PM | 4 | 9 | <25 | <25 |
| Existing Plus Quarry Ridge Project |  | AM | 12 | 6 | <25 | <25 |
|  |  | PM | 24 | 9 | <25 | 50 |
| Existing Plus Approved / Pending Projects |  | AM | 13 | 60 | <25 | 75 |
|  |  | PM | 20 | 33 | 25 | 75 |
| EPAP Plus Quarry Ridge Project |  | AM | 15 | 60 | $<25$ | 75 |
|  |  | PM | 40 | 33 | 50 | 100 |
| Year 2036 No Project |  | AM | 13 | 60 | 25 | 75 |
|  |  | PM | 20 | 35 | 25 | 75 |
| Year 2036 with Quarry Ridge Project |  | AM | 15 | 60 | 25 | 75 |
|  |  | PM | 40 | 35 | 50 | 100 |
| HCM is queue based on Highway Capacity Manual LOS analysis. HDM is storage recommended by Caltrans Highway Design Manual (HDM).. |  |  |  |  |  |  |

Evaluation of Westbound Left Turn Lane Deceleration and Storage at Granite Estates
Drive. As noted in Table 16, today the westbound left turn lane on Douglas Blvd at Granite Estates Drive is 230 feet long. This lane is preceded by a 120 foot long bay taper. If the Quarry Ridge Professional Offices project proceeds under Existing plus Project conditions then a two car queue is likely in the lane during the p.m. peak hour. The left turn lane has the capacity to provide storage for up to 9 waiting vehicles, so the design is adequate in that regard.

Under EPAP conditions the combination of regional development and the turning requirements of projects in the area of Berg Street will increase the number of vehicles in the westbound left turn lane, and the forecast queues will be longer. Without the Quarry Ridge Professional Offices project, a three car queue is expected during both the a.m. and p.m. peak hour under Existing plus Approved Projects conditions. The addition of Quarry Ridge Professional Offices traffic will increase the queue to four cars in the p.m. peak hour. The left turn lane provides adequate storage for these cars.

The length of queues expected under Year 2036 conditions are similar to those shown under EPAP conditions. With the project, a four car queue is expected, and adequate storage will be available.

To use the left turn lane, motorists will slow to a stop behind the forecast queue, and the adequacy of the remaining area for deceleration has been evaluated. Under Existing plus Project conditions the two car queue leaves 300 feet for deceleration from the beginning of the bay taper to the waiting vehicle. This distance accommodates a stop from 38 mph . As the posted speed limit on this section of Douglas Blvd is 55 mph , the relative difference between through traffic and slowing traffic is 17 mph , which satisfies the HDM guideline for speed differential (i.e., 20 mph ).

If background projects are developed under the Existing plus Approved / Pending Projects condition and Year 2036 conditions the maximum queue becomes three vehicles, the deceleration distance is 275 feet and the entering speed is 35 mph . The speed differential is 20 mph , which is the maximum under the HDM guideline.

With development of the project under EPAP or Year 2036 conditions with the longest queues (i.e., four vehicles under) 250 feet will be available for deceleration from the beginning of the bay taper to the waiting vehicle. This distance provides space to decelerate to a stop from 32 mph . As the posted speed limit on this section of Douglas Blvd is 55 mph , the relative difference between through traffic and slowing traffic is 23 mph , which exceeds the HDM guideline for speed differential (i.e., 20 mph ). Thus, the project's cumulative impact could be considered to be significant, and mitigation is required. Mitigation alternatives are discussed in the test which follows.

| TABLE 14 <br> DOUGLAS BLVD MEDIAN OPENING ASSESSMENT EASTBOUND BERG STREET LEFT TURN LANE |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Condition | Storage Length (feet) | Time Period | Eastbound at Berg Street |  |  |  |
|  |  |  | Volume |  | Queue (feet) |  |
|  |  |  | U-turn | Left | HCM | HDM |
| Existing | 300 | AM | 2 | 36 | <25 | 50 |
|  |  | PM | 12 | 56 | <25 | 75 |
| Existing Plus Quarry Ridge Project |  | AM | 2 | 59 | <25 | 75 |
|  |  | PM | 12 | 63 | <25 | 75 |
| Existing Plus Approved / Pending Projects |  | AM | 45 | 60 | 50 | 125 |
|  |  | PM | 56 | 80 | 75 | 150 |
| EPAP Plus Quarry Ridge Project |  | AM | 45 | 83 | 75 | 150 |
|  |  | PM | 56 | 87 | 75 | 150 |
| Year 2036 No Project |  | AM | 45 | 62 | 75 | 125 |
|  |  | PM | 55 | 83 | 75 | 150 |
| Year 2036 With Quarry Ridge Project |  | AM | 45 | 85 | 75 | 150 |
|  |  | PM | 55 | 90 | 75 | 150 |
| HCM is queue based on Highway Capacity Manual LOS analysis. HDM is storage recommended by Caltrans Highway Design Manual (HDM). |  |  |  |  |  |  |

Evaluation of Eastbound Left Turn Lane Deceleration and Storage at Berg Street. The eastbound left turn lane approach at Berg Street is longer and provides additional space for queueing. The 300 foot long left turn lane provides storage for 12 waiting vehicles and is preceded by a 125 foot long bay taper. As noted in Table 14, if the Quarry Ridge Professional Offices project is in operation, then a three car queue could be expected in the a.m. and p.m. peak hour under Existing plus Project conditions. The left turn lane can accommodate this queue. The queue lengthens as other local development occurs and is 150 feet long with Quarry Ridge and other approved / pending projects proceed. Under Year 2036 conditions with Quarry Ridge this queue would also be 150 feet long, which can still be accommodated by the left turn lane.

The effects of queueing on deceleration have been considered. Under Existing plus Project conditions the remaining distance between the beginning of bay taper and waiting vehicles in a three car queue is 350 feet. This distance can accommodate deceleration to a stop from 43 mph , and the difference between through traffic and turning traffic is 12 mph , which is within the HDM guideline.

Under cumulative conditions a six vehicle queue is expected, the distance between beginning of the bay taper and waiting cars is 275 feet. This distance accommodates deceleration from 35 mph , and the difference between this speed and the 55 mph speed limit on Douglas Blvd is 20 mph, which also meets the threshold noted in the HDM.

Improvement Options - Eliminate Landscaped Median. It is possible to make the westbound left turn lane approaching the Granite Estates Drive intersection longer by eliminating the short landscaped median altogether and constructing back-to-back turn lanes in the median area. Another 100 feet could be added to the westbound left turn lane or the 100 foot distance could be split between the back to back turn lanes approaching Granite Estates Drive and Berg Street. Adding 50 feet to each lane would increase the deceleration area behind anticipated queues and increases the permissible entry speed by 5 mph . Under Year 2036 plus Project conditions adding 50 feet to the westbound left turn lane at Granite Estates Drive would yield 300 feet of lane + bay taper behind the queue. This distance accommodates deceleration from 38 mph . The incremental difference between speed limit and entry speed is 18 mph , which would satisfy HDM guidance. Adding the entire 100 feet to this lane would yield 350 feet of deceleration, an entry speed of 43 mph and an incremental difference of 12 mph .

Mitigation. The project proponents shall be responsible for reconstructing the Douglas Blvd median between Granite Estates Drive and Berg Street to provide longer left turn lanes to the satisfaction of the Placer County DPWF. With this improvement the project's cumulative impact is not significant.

## BERG STREET ACCESS DESIGN

## Proposed Design

The project proposes full access onto Berg Street. The site plan indicates that Berg Street will be widened along the project frontage to meet Plate 116 requirements. With these improvements, the adequacy of the full access at the Berg Street driveway is based on consideration of three factors. First, the sight distance available from the exit has been considered relative to the speed of northbound traffic on Berg Street. Second, the need for a southbound left turn lane to separate project traffic from through traffic has been evaluated. Third, the length of any queue of southbound traffic waiting at the Douglas Blvd intersection relative to the project driveway has also been considered.

## Evaluation

Sight Distance. The posted speed limit on Berg Street is 35 mph . The sight distance needed at that speed is noted in Plate 116 of the Placer County standard plans (i.e., 385 feet) and should not be less than the minimum sight distance requirement under Table 201.1 of the Highway Design Manual (i.e. 250 feet). The Plate 116 distance is clearly available looking to the north from the project driveway. Looking to the south, turning vehicles would be visible in the Douglas Blvd intersection at a distance of roughly 220 feet. Because all northbound traffic first makes a left or right turn from Douglas Blvd, the adequacy of the available sight distance should be predicated on the speed of those turning vehicles. In general, the available turning radii would limit the speed of traffic leaving the Douglas Blvd intersection to $20-25 \mathrm{mph}$. The Plate 116 sight distance requirement for 25 mph is 275 feet, while the minimum is 150 feet. Based on the speed on northbound Berg Street, the sight distance at the driveway ( 220 feet) which satisfies minimum HDM requirements ( 150 feet) should be adequate looking south.

Left Turn Lane Channelization. The methodology employed by Caltrans and local agencies was used to quantitatively determine whether a left turn lane is justified in this case. The American Association of State Transportation and Highway Officials (AASHTO) have identified guidelines for the installation of left turn lanes in their publication A Policy on Geometric Design of Highways and Streets. These guidelines, which are presented in their Table 9-23 and Table 15 which follows, base the need for a left turn lane on the volume of traffic on the mainline road and the relative percentage of that traffic that turns. These criteria are applicable to intersections where the major street traffic proceeds freely and side street traffic is controlled by stop signs. These guidelines are the basis for determination of left turn warrants at un-signalized intersection based strictly on traffic volumes. A second metric of impact to public safety is also considered by Placer County. Each location is analyzed on an individual basis, and traffic engineering judgment is employed.

The need for the left turn lane could be based on the volumes occurring in the a.m. peak hour when the volume of inbound traffic is highest. Under Cumulative plus Project conditions there would be 5 left turns into the site at this location. The resulting cumulative opposing / advancing volume occurring at the site access have been determined. As noted in Table 15, for the volume of northbound traffic (i.e., 105 vehicles per hour), the advancing volume would need to be in the
range of 600 to 700 vph at 40 mph design to justify a separate left turn lane at the access. The anticipated volume (i.e., 80 vph ) falls well outside that range. Therefore, a left turn lane would not be needed under these criteria.

| TABLE 15 <br> TRAFFIC VOLUMES JUSTIFYING LEFT TURN LANES |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Opposing Volume (veh/hr) | Advancing Volume (veh/hr) |  |  |  |
|  | $5 \%$ <br> Left Turns | $\begin{gathered} \hline 10 \% \\ \text { Left Turns } \end{gathered}$ | $\begin{gathered} 20 \% \\ \text { Left Turns } \end{gathered}$ | $\begin{gathered} \hline 30 \% \\ \text { Left Turns } \end{gathered}$ |
| 40-mph operating speed |  |  |  |  |
| 800 | 330 | 240 | 180 | 160 |
| 600 | 410 | 305 | 225 | 200 |
| 400 | 510 | 380 | 275 | 245 |
| 200 | 640 | 470 | 350 | 305 |
| 105 | 80(6\%) |  |  |  |
| 100 | 720- | 515 | 390 | 340- |
| Source: A Policy on Geometric Design of Highway and Streets, AASHTO, 2012, Chapter 9. Cumulative Plus Project AM Peak Hour Volumes are shown in RED |  |  |  |  |

Southbound Queue. The length of the southbound queue on Berg Street approaching the Douglas Blvd intersection can be identified as a byproduct of the HCM Level of Service calculation. Because Berg Street traffic must turn right, the delays for these motorists are relatively low, and as a result the projected $95^{\text {th }}$ percentile queue is 2 vehicles or less under Cumulative plus Project conditions. At 25 feet per vehicle this queue would extend 50 feet but would not have an appreciable effect on the operation of the site access roughly 170 feet further north. This access as proposed is adequate under these criteria.

## Relationship to Douglas Blvd Frontage Improvements

Westbound deceleration on Douglas Blvd. Placer County may require that improvements be made to the project frontage to satisfy Plate 116 requirements. These requirements could include a westbound deceleration taper.

## EXISTING PLUS APPROVED / PENDING PROJECTS (EPAP) IMPACTS

This analysis section addresses the relative impacts of the project within the context of other approved and pending development projects in Granite Bay. The main purpose of this assessment is to confirm the adequacy of the configuration of the Granite Drive - Berg Street turn lanes on Douglas Blvd, but traffic conditions at all study intersections have been assessed. This assessment does not however address the long term effects of regional traffic growth which is evaluated in the subsequent Cumulative analysis.

## Project Characteristics

Land Use. Placer County staff identified pending and approved projects for this analysis, as noted in Table 16. This list of projects includes those in the immediate area of the proposed project as well as other Granite Bay area projects that had not been occupied when the baseline traffic counts employed for this analysis were collected in 2017. The local projects include:

- Berg Street Medical / Office Complex
- The Ponds Event Pavilion and Office
- Granite Estates Professional Center
- Little Sunshine Pre-School

As indicated, a total of 33 development projects were considered for this analysis.
Trip Generation. Table 16 also indicates the daily and weekday peak hour trip generation associated with the approved / pending projects list. As indicated, these 33 projects could generate 11,360 daily trips, with 898 a.m. and 1,312 p.m. peak hour trips.

| TABLE 16IDENTIFIED APPROVED / PENDING PROJECTS AND TRIP GENERATION |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Project | Unit | Quantity |  |  |  | Trips |  |  |  |
|  |  |  | Daily | AM Peak Hour |  |  | PM Peak Hour |  |  |
|  |  |  |  | In | Out | Total | In | Out | Total |
| Trip Attractions |  |  |  |  |  |  |  |  |  |
| The Ponds Pavilion and Office (20.44 ksf Phase 1 and 24 ksf office Phase 2) | Office ksf | 40.44 | 740 | 90 | 12 | 102 | 29 | 144 | 173 |
| Granite Bay Medical Office Complex | MOB ksf | 15.9 ksf | 575 | 30 | 8 | 38 | 16 | 41 | 57 |
| Granite Estates Professional Center | Office ksf | $19.7 \mathrm{ksf}^{1}$ | 393 | 25 | 6 | 31 | 12 | 36 | 48 |
| Little Sunshine Preschool | Students | 144 | 631 | 61 | 54 | 115 | 55 | 62 | 117 |
| Granite Bay Memory Care | beds | 66 | 176 | 5 | 4 | 9 | 6 | 9 | 15 |
| Ovation Senior Living | beds | 114 | 303 | 10 | 6 | 16 | 11 | 14 | 25 |
| Roseville Congregate Living home | beds | 15 | 40 | 1 | 1 | 2 | 2 | 2 | 4 |
| Amazing Facts | Church ksf | 120.2 | 1,095 | 42 | 25 | 67 | 32 | 34 | 66 |
| Chabad of Roseville ${ }^{2}$ | Church ksf students | $\begin{gathered} 25.0 \\ 130 \\ \hline \end{gathered}$ | 348 | 10 | 4 | 14 | 6 | 6 | 12 |
| Pardee Court Commercial (net) | ksf | 8.8 ksf | 360 | 9 | 11 | 20 | 2 | -5 | -3 |
| 2Placer Retirement Residences | units | 145 | 293 | 5 | 4 | 9 | 14 | 11 | 25 |
| Sehr Winery \& Events ${ }^{3}$ | Tasting Room Attendees | $\begin{gathered} 4.8 \mathrm{ksf} \\ 200 \end{gathered}$ | 212 | 4 | 4 | 8 | 84 | 4 | 88 |
| Hacienda Carnelitas ${ }^{4}$ | Event ksf Attendees | $\begin{gathered} 8.60 \mathrm{ksf} \\ 205 \\ \hline \end{gathered}$ | 184 | 2 | 2 | 4 | 82 | 0 | 82 |
| St Joseph's Church ${ }^{5}$ | Church ksf multipurpose | $\begin{aligned} & 25.0 \\ & 16.3 \\ & \hline \end{aligned}$ | 176 | 7 | 4 | 11 | 5 | 6 | 11 |
| Subtotal Non-Residential |  |  | 5,526 | 301 | 145 | 446 | 356 | 364 | 720 |
| (1) 7,900 sf operating when traffic counts conducted <br> (2) ITE rates applied to net increase of 12,200 sf of community center and 88 students <br> (3) Average weekday visitation based on Placer Wineries counts plus 200 person event starting in p.m. peak hour <br> (4) 205 person event starting in p.m. peak hour <br> (5) 5.9 ksf multipurpose and 16.5 ksf church already exist |  |  |  |  |  |  |  |  |  |


| TABLE 16 (continued) <br> IDENTIFIED APPROVED / PENDING PROJECTS AND TRIP GENERATION |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Project | Unit | Quantity | Trips |  |  |  |  |  |  |
|  |  |  |  |  | Peak |  |  | Peak |  |
|  |  |  | Daily | In | Out | Total | In | Out | Total |
| Trip Productions |  |  |  |  |  |  |  |  |  |
| The Grove at Granite Bay(6) | SFR | 32 | 105 | 2 | 6 | 8 | 7 | 4 | 11 |
| Granite Rock Estates | SFR | 16 | 152 | 3 | 9 | 12 | 10 | 6 | 16 |
| Lake Vista Estates | SFR | 15 | 143 | 3 | 8 | 11 | 9 | 6 | 15 |
| Enclave at Granite Bay | SFR | 12 | 114 | 2 | 7 | 9 | 8 | 4 | 12 |
| Maher Subdivision | SFR | 7 | 67 | 1 | 4 | 5 | 4 | 3 | 7 |
| Rancho Del Oro | SFR | 89 | 847 | 17 | 50 | 67 | 56 | 33 | 89 |
| Whitehawk I (Granite Bay 17) | SFR | 24 | 228 | 5 | 13 | 18 | 15 | 9 | 24 |
| Whitehawk II (Granite Bay 33) | SFR | 55 | 524 | 10 | 31 | 41 | 35 | 20 | 55 |
| Barton Ranch | SFR | 10 | 95 | 2 | 6 | 8 | 6 | 4 | 10 |
| Greyhawk III | SFR/MFR | 28 SFR / 44 MFR | 523 | 8 | 32 | 40 | 33 | 18 | 51 |
| Park at Granite Bay | SFR | 56 | 533 | 11 | 31 | 42 | 35 | 21 | 56 |
| Hawk Homestead | SFR | 108 | 1,028 | 20 | 61 | 81 | 69 | 39 | 108 |
| Edon Roc II | SFR | 6 | 57 | 1 | 4 | 5 | 4 | 2 | 6 |
| Colinas Estates | SFR | 10 | 95 | 2 | 6 | 8 | 6 | 4 | 10 |
| Eureka at Granite Bay | MFR | 28 | 163 | 2 | 10 | 12 | 10 | 5 | 15 |
| Amazing Facts Residential | SFR | 16 | 152 | 3 | 9 | 12 | 10 | 6 | 16 |
| Pardee Court | MFR | 35 | 204 | 3 | 12 | 15 | 12 | 6 | 18 |
| Premier Granite Bay | MFR | 52 | 302 | 4 | 19 | 23 | 18 | 9 | 27 |
| Residences at Granite Bay Golf | SFR | 4 | 38 | 1 | 2 | 3 | 3 | 1 | 4 |
| Rolling Greens | SFR | 9 | 96 | 2 | 5 | 7 | 6 | 3 | 9 |
| Ventura at Granite Bay | SFR | 33 | 314 | 6 | 19 | 25 | 21 | 12 | 33 |
| Subtotal Residential |  |  | 5,780 | 108 | 344 | 452 | 377 | 215 | 592 |
| (1) Eleven lots unoccupied when traffic counts conducted |  |  |  |  |  |  |  |  |  |
|  |  |  | Daily trips | AM Peak Hour Trips |  |  | PM Peak Hour Trips |  |  |
|  |  |  |  | In | Out | Total | In | Out | Total |
| TOTAL TRIPS |  |  | 11,360 | 409 | 489 | 898 | 733 | 579 | 1,312 |

## Traffic Volume Forecasts

Approach. The trips associated with the identified project list were assigned to the Granite Bay circulation network based on distribution assumptions derived from review of other traffic studies, assessment current traffic patterns and relative travel times and review of regional traffic model forecasts. The trip assignment was performed manually using a TRAFFIX local area assignment model to provide adequate detail for assessment of specific intersections. To provide a "worst case" assessment no attempt was made to match trips between productions and attractions as would be the case using a regional model.

Volumes. Figure 6 presents resulting "Existing plus Approved / Pending Projects (EPAP)" peak hour traffic volumes at intersections, while Figure 7 presents the sum of EPAP and Quarry Ridge traffic volumes.

## Background EPAP Conditions

Improvements. Identified approved projects are conditioned to install improvements to study area intersections or will make access improvements. The Ventura at Eureka subdivision will add a westbound left turn lane at the Eureka Road / Barton Road intersection, and this improvement has been assumed. At the Douglas Blvd / Seeno Avenue intersection the Whitehawk II project will be constructing the south leg of the intersection, and at the Quarry Ridge access on Berg Street the Granite Bay Medical Offices will construct their access on the west side of the intersection.

Intersection Levels of Service. Table 17 presents the results of intersection Level of Service calculations for "Existing plus Approved / Pending Projects" conditions. As indicated, three intersections will operate with Levels of Service that do not satisfy minimum standards. The Douglas Blvd / Woodgrove Way / Quail Oaks Drive intersection will operate at LOS F in the a.m. and p.m. peak hour. This deficiency also occurs under Existing conditions. while a traffic signal might be considered, the anticipated improvement would be prohibiting left turns from side streets onto Douglas Blvd.

The Douglas Blvd / Granite Estates Drive intersection will operate at LOS F in the p.m. peak hour, and measures to improve the overall Level of Service are limited at this side-street stopcontrolled intersection. Outbound left turns are already prohibited. Eliminating westbound left turns would actually increase the overall average delay because the individual delay associated with that movement is less than average. A separate eastbound right turn lane could be constructed on Douglas Blvd, but while this treatment would reduce delay for northbound right turns slightly, the overall Level of Service would remain LOS F.

The Barton Road / Eureka Road intersection is projected to operate at LOS F in the a.m. and p.m. peak hour if no improvements are made. This deficiency already occurs in the existing a.m. peak hour. The Granite Bay CIP includes a traffic signal at this location, and implementation of a traffic signal with applicable auxiliary lanes would yield LOS C or better conditions.

Roadway Segment Levels of Service Based on General Plan Thresholds. Table 18 identifies projected daily traffic volumes assuming occupancy of approved / pending project. The same locations which are already deficient under existing conditions would continue to operate with Level of Service that falls below the minimums standards of the GBCP. The four lane segments of Douglas Blvd from Cavitt Stallman Road to Auburn Folsom Road would operate at LOS F.


-
(36) 3544
(358) $149 \xrightarrow{2}$
1589) $1156 \rightarrow$
(281) 1727
Sierra College Blvd/ Douglas Blvd

Woodgrove Way/ Quail Oaks Dr/ Douglas Blvd


Seeno Ave/ Douglas Blvd


Granite Estates Dr/ Douglas Blvd

|  |  |
| :---: | :---: |
| $\begin{array}{r} (56) 45 \\ (80) 60 \\ (2009) 1448 \\ (27) 14 \end{array}$ | $\begin{aligned} & C \frac{0}{R 1-1} \\ & \sim \\ & \stackrel{\mathrm{~J}}{\mathrm{E}} \end{aligned}$ |

(27) 14

Berg St/ Douglas Blvd


Douglas Blvd/ Auburn Folsom Rd
8 (

Barton Rd/ Eureka Rd
9


Berg St/ Access

KD Anderson \& Associates, Inc

EXISTING PLUS APPROVED PROJECTS TRAFFIC VOLUMES AND LANE CONFIGURATIONS


TABLE 17
EXISTING PLUS APPROVED / PENDING PROJECTS PLUS QUARRY RIDGE PEAK HOUR INTERSECTION LEVELS OF SERVICE

| Intersection | Control | AM Peak Hour |  |  |  | PM Peak Hour |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Existing Plus Approved / Pending Projects |  | EPAP Plus Project |  | Existing Plus Approved / Pending Projects |  | EPAP Plus Project |  |
|  |  | LOS | Average Delay (sec/veh) | LOS | Average Delay (sec/veh) | LOS | Average Delay (sec/veh) | LOS | Average Delay (sec/veh) |
| Douglas Blvd / Sierra College Blvd | Signal | D | 46.5 | D | 48.0 | E | 61.5 | E | 70.0 |
| Douglas Blvd / Woodgrove Way (overall) <br> Eastbound left turn Westbound left turn Northbound left+thru+right turn Southbound left+thru+right turn | NB/SB Stop | $\begin{gathered} (\mathbf{F}) \\ \mathrm{C} \\ \mathrm{C} \\ \mathrm{~F} \\ \mathrm{~F} \\ \hline \end{gathered}$ | $\begin{gathered} (\mathbf{1 4 8 . 0}) \\ 23.0 \\ 16.0 \\ 419.0 \\ 61.5 \\ \hline \end{gathered}$ | $\begin{gathered} (\mathbf{F}) \\ \mathrm{C} \\ \mathrm{C} \\ \mathrm{~F} \\ \mathrm{~F} \\ \hline \end{gathered}$ | $\begin{gathered} (\mathbf{1 4 8 . 0}) \\ 23.0 \\ 16.0 \\ 414.0 \\ 61.5 \\ \hline \end{gathered}$ | $\begin{gathered} (\mathbf{F}) \\ \text { C } \\ \text { C } \\ \text { F } \\ \text { F } \end{gathered}$ | $\begin{gathered} \mathbf{( 2 4 3 . 5 )} \\ 21.5 \\ 27.5 \\ 711.0 \\ 153.0 \\ \hline \end{gathered}$ | $\begin{gathered} (\mathbf{F}) \\ \mathrm{C} \\ \mathrm{C} \\ \mathrm{~F} \\ \mathrm{~F} \\ \hline \end{gathered}$ | $\begin{gathered} \mathbf{( 2 4 1 . 5 )} \\ 22.0 \\ 27.5 \\ 711.0 \\ 153.5 \\ \hline \end{gathered}$ |
| Douglas Blvd / Seeno Avenue | Signal | B | 15.5 | B | 15.5 | B | 16.5 | B | 17.0 |
| Douglas Blvd / Granite Estates Drive <br> (overall) <br> Westbound left turn <br> Northbound right turn | NB Stop | (C) <br> C <br> C | $\begin{gathered} (20.5) \\ 18.0 \\ 23.0 \\ \hline \end{gathered}$ | $\begin{gathered} \text { (C) } \\ \text { B } \\ \text { C } \\ \hline \end{gathered}$ | $\begin{gathered} (21.0) \\ 18.5 \\ 23.0 \\ \hline \end{gathered}$ | $\begin{gathered} (\mathbf{F}) \\ \mathrm{D} \\ \mathrm{~F} \\ \hline \end{gathered}$ | $\begin{gathered} \mathbf{( 5 7 . 0}) \\ 27.5 \\ 68.5 \\ \hline \end{gathered}$ | $\begin{gathered} (\mathbf{F}) \\ \mathrm{D} \\ \mathrm{~F} \\ \hline \end{gathered}$ | $\begin{gathered} \mathbf{5 6 . 0}) \\ 31.0 \\ 69.5 \\ \hline \end{gathered}$ |
| Douglas Blvd / Berg Street (overall) <br> Eastbound left turn Westbound left turn Northbound right turn Southbound right turn | NB/SB Stop | (C) <br> D <br> B <br> C <br> D | $\begin{gathered} (23.5) \\ 26.5 \\ 15.0 \\ 15.5 \\ 28.0 \\ \hline \end{gathered}$ | $\begin{gathered} \text { (D) } \\ \text { C } \\ \text { B } \\ \text { B } \\ \text { C } \end{gathered}$ | $\begin{gathered} (25.0) \\ 29.0 \\ 15.0 \\ 15.5 \\ 29.0 \\ \hline \end{gathered}$ | (D) <br> D <br> C <br> C <br> D | $\begin{gathered} (25.5) \\ 27.0 \\ 23.0 \\ 22.5 \\ 25.0 \\ \hline \end{gathered}$ | (D) <br> D <br> C <br> C <br> D | $\begin{gathered} (30.0) \\ 28.5 \\ 23.5 \\ 22.5 \\ 34.5 \\ \hline \end{gathered}$ |
| Douglas Blvd / Barton Road | Signal | E | 57.5 | E | 59.0 | E | 73.5 | E | 76.5 |
| Douglas Blvd / Auburn - Folsom Road | Signal | D | 46.5 | D | 47.0 | D | 46.0 | D | 46.0 |
| Barton Road / Eureka Road | All-way Stop | F | 73.5 | F | 75.5 | E | 44.0 | E | 46.0 |
| Berg Street / Access (overall) <br> Northbound Left turn Southbound left turn Eastbound left+right turn Westbound left+right turn | EB/WB Stop | (A) <br> A <br> A | $\begin{gathered} (7.5) \\ 7.5 \\ - \\ 8.5 \end{gathered}$ | (A) <br> A <br> A <br> A <br> B | $\begin{gathered} (8.0) \\ 7.5 \\ 7.5 \\ 8.5 \\ 10.0 \\ \hline \end{gathered}$ | (A) <br> A <br> A | $\begin{gathered} (8.0) \\ 7.5 \\ - \\ 9.0 \\ - \\ \hline \end{gathered}$ | (A) <br> A <br> A <br> A <br> B | $\begin{gathered} (9.5) \\ 7.5 \\ 7.5 \\ 9.0 \\ 10.5 \\ \hline \end{gathered}$ |


| TABLE 18 <br> EXISTING PLUS APPROVED / PENDING PROJECTS AND QUARRY RIDGE ROADWAY SEGMENT LEVELS OF SERVICE |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Roadway | Location | Lanes | Existing PlusApproved / Pending ProjectsConditions |  |  | EPAP <br> Plus Quarry Ridge Conditions |  |  |  |
|  |  |  | Daily Volume |  | LOS | Daily Volume |  | LOS | Change in V/C |
|  |  |  | Projects Only | Total |  | Project Alone | Total |  |  |
| Douglas Blvd | Sierra College Blvd to Cavitt Stallman Rd | 4 | 3,760 | 51,320 | F | 320 | 51,640 | F | 0.009 |
|  | Cavitt Stallman Road to Seeno Avenue | 4 | 3,330 | 50,160 | F | 320 | 50,480 | F | 0.008 |
|  | Seeno Avenue to Berg Street | 4 | 2,810 | 47,610 | F | 340 | 47,950 | F | 0.009 |
|  | Berg Street to Barton Road | 4 | 2,680 | 45,480 | F | 190 | 45,670 | F | 0.005 |
|  | Barton Road to Auburn Folsom Road | 4 | 2,070 | 44,690 | F | 110 | 44,800 | F | 0.003 |
| Berg Street | Olive Ranch Road to Project | 2 | 260 | 1,460 | A | 40 | 1,500 | A | 0.003 |
|  | Olive Ranch Road to Douglas Blvd | 2 | 790 | 1,990 | A | 530 | 2,520 | A | 0.035 |

## EPAP Plus Quarry Ridge Project Levels of Service

Intersections. As shown in Table 17, the addition of project trips will incrementally increase the length of delays at study intersections. At all but three locations the resulting Levels of Service will continue to satisfy the minimum LOS E standard for Douglas Blvd and minimum C standard elsewhere from the Granite Bay Community Plan. Thus, the impacts of the project are not considered to be significant under CEQA at these locations.

The project's relative impact has been considered at the three intersections where EPAP background conditions already fail to satisfy minimum GBCP standards. At each location the applicable Methodology of Assessment criteria has been reviewed. The Douglas Blvd / Woodgrove Way / Quail Ridge Drive intersection operates at an overall LOS F with and without the project, and the change in overall delay is the applicable criteria. In this case, because the project adds vehicles to movements with individual delays that are below average, the overall weighted average delay does not increase as a result of the project. Thus the project's impact is not significant.

Similarly, the Douglas Blvd / Granite Estate Drive intersection is projected to operate with an overall LOS F with and without the project. Again, because the project adds to movements with lower than average delays, the overall weighted average does not increase, and the projects impact is not significant.

The Barton Road / Eureka Road intersection will operate at LOS F with and without the project, and the change in overall day is the significance criteria. In this case, the a.m. peak hour delay increases by 2.0 seconds and the average delay in the p.m. peak hour increases by 2.0 seconds. Because these increases are less than the 2.5 second increment permitted under the Methodology of Assessment, the project's impact is not significant.

Roadway Segments based on General Plan Thresholds. Table 18 identifies the project's daily traffic volume contribution to study area roadway segments under the EPAP background condition and resulting Levels of Service. As indicated the projected conditions exceed GBCP minimum standards on Douglas Blvd, although the project will not change the Level of Service occurring on any roadway segment. The project will add traffic to roadways that are deficient under background conditions based on General Plan thresholds. In this case the significance of project impact is based on the criteria included under Placer County Methodology of assessment, and the project contribution has been evaluated accordingly.

The project's incremental change can be described in terms of its change in roadway volume / capacity ratio. As was the case under Existing plus Project conditions, the project's contribution to Douglas Blvd ranges from 0.003 to 0.009 . As these changes are less than the 0.050 increment permitted under Placer County methodology, the project's impact is not significant under this metric.

The second criteria is the "vehicles per lane" (vpl) traffic increase. As was discussed under Existing plus Project conditions, the project adds 30 to 85 vpl at various locations on Douglas Blvd. Because these increments do not exceed the 100 vpl threshold permitted under Placer County methodology, the project's impact is not significant.

## CUMULATIVE IMPACTS

This section addresses cumulative impacts occurring as a result of future development in the South Placer area and regional traffic growth on major roads.

## Background Assumptions / Approach

Regional Traffic Growth. The impacts of numerous approved / pending projects were evaluated within the context of long term cumulative traffic conditions. Placer County is currently updating the GBCP Circulation Element, and as part of that work an updated regional travel demand forecasting model was created. Baseline Year 2015 and Future Year 2036 daily and peak hour model traffic volume forecasts were provided by Placer County for use in this analysis.

Project Land Use. Because the proposed project has been included in the Year 2036 land use assumptions, for this analysis the long term traffic volume forecasts present the Cumulative plus Project scenario. The Cumulative No Project condition was identified by manually subtracting the proposed project's trips.

Methods. An incremental approach was taken to create the traffic volume employed for the analysis. Year 2016 model and Year 2036 model results were compared at intersections and on roadway segments and the incremental different was identified. These increments were then added to the current intersection or segment traffic volumes to create the adjusted future condition. In addition, the future forecasts were manually adjusted at the Douglas Blvd / Granite Estate and Douglas Blvd / Berg Street intersections to account for the local access limitations created by left turn prohibition and resulting u-turns.

## Traffic Volume Forecasts

Figure 8 presents background long term Cumulative No Project traffic volumes at study intersections, while Figure 9 presents volumes with the proposed project.

Future Improvements. Local agencies have identified improvements to be constructed in the future whether Quarry Ridge Professional Office Park proceeds or not.

Placer County Countywide Traffic Mitigation Fee Program. Placer County administers the Countywide Traffic Mitigation Fee Program which requires new development to contribute to the cost of circulation system improvements of county wide benefit. Individual benefit districts have been established. The Placer County roads in this analysis are addressed in the Granite Bay Capital Improvement Program (CIP), and the current list of CIP improvements is presented in Table 19. Improvements to study area locations have been assumed to be installed.

In addition, the City of Roseville intends to add a southbound right turn lane at the Douglas Blvd / Sierra College Blvd intersection, and this improvement has been included in the analysis.

| TABLE 19GRANITE BAY FEE DISTRICT / CIP PROJECTS |  |  |
| :---: | :---: | :---: |
| Street / Intersection | Segment | Description of Improvements |
| Auburn Folsom Rd | Sacramento County to $500^{\prime}$ north of Douglas Blvd | Widen to 4-lanes with Class II bike lanes, intersection improvements |
|  | Douglas Blvd to Joe Rodgers Rd | Class II bike lanes / Curb, Gutter and Sidewalk |
|  | At Douglas Blvd | Intersection Improvements |
|  | At Cavitt-Stallman Rd | New Traffic Signal |
|  | Joe Rodgers Rd to Dick Cook Rd | Traffic flow Improvements (e.g. left turn pockets) |
| Barton Rd | Sacramento County line to Loomis limit | Widen Pavement, Class II bikeway |
|  | At Douglas Blvd | Intersection Improvements (EB right turn lane, SB left turn lane, signal upgrades) |
|  | At East Roseville Parkway | New Traffic Signal |
|  | At Cavitt Stallman Rd | Traffic signal or Roundabout |
| Berg Street | Olive Ranch Rd to Douglas Blvd | Widen Pavement |
| Cavitt-Stallman Rd | Cavitt-Stallman South Rd to Barton Rd | Widen Pavement, Class II Bikeway |
|  | Barton Rd to Auburn Folsom Rd | Widen Pavement, Class II Bikeway |
|  | At Laird Rd | Realign Intersection, ROW |
| Dick Cook Rd | Val Verdi Rd to Auburn Folsom Rd | Widen pavements (per GBCP) |
| Douglas Blvd | Cavitt Stallman Rd south to Sierra College Blvd | Widen to 6-lanes, Class II bike lanes |
|  | At Sierra College Blvd | Additional turn lanes on Douglas Blvd (dual lefts all approaches) Note: City of Roseville anticipates a southbound right turn lane |
| East Roseville Pkwy | At Wellington Way | New Traffic Signal |
| Eureka Rd | Sierra College Blvd to Wellington Way | Widen to 4-lanes with Class II bike lanes |
|  | At Barton Rd | Roundabout or New Traffic Signal |
|  | At Wellington Way | New Traffic Signal |
|  | Wellington Way to Auburn Folsom Rd | Widen pavement, Class II Bike lanes |
|  | At Greyhawk Drive | Intersection improvements (SB left turn lane, EB receiving lane) |
| Laird Rd | Cavitt Stallman Rd to Loomis Town limits | Widen Pavement, Curve Improvements, Class II Bikeway |
| Laird Rd to Val Verde Connector | Connector between Laird Road and Val Verde Rd | Construct 2-lane roadway with shoulders |
| Old Auburn Rd | Sierra College Blvd to Roseville limits | Complete north side of roadway |
| Olive Ranch Rd | Cavitt Stallman Rd to Barton Rd | Widen Pavement / Reconstruct |
| Sierra College Blvd | Sacramento Co to Old Auburn Rd | Widen to 6-lanes, class II bike lanes |
|  | At Cavitt Stallman Rd | Partial Signal |
|  | At Eureka Rd | Extend southbound left turn lane |
|  | Old Auburn Rd to Roseville Pkwy | Sidewalk, Curb \& Gutter |
|  | Eureka Rd to Cavitt Stallman Rd | Sidewalk, Curb 7 Gutter |
| Val Verde Rd | Wells Avenue to Dick Cook Rd | Widen Pavement |
| Wells Avenue | Laird Rd to Val Verde Rd | Widen pavement |
|  | Loomis Town limits to Laird Rd | Widen Pavement |
| Circulation Update | Fee District | Circulation Element Update |
| Minor Improvements | Fee District | Minor Improvements required due to increased traffic |




Granite Estates Dr/ Douglas Blvd

(30) 15

Berg St/ Douglas Blvd


Douglas Blvd/ Auburn Folsom Rd

|  |  |
| :---: | :---: |
| $\begin{array}{r} (45) 65 \\ (345) 255 \\ (175) 75 \end{array} \underset{\sim}{\boldsymbol{\jmath}}$ |  |

Barton Rd/ Eureka Rd
9


Berg St/ Access


YEAR 2036 PLUS QUARRY RIDGE
KD Anderson \& Associates, Inc

## Cumulative No Project Levels of Service

Intersection Level of Service. Table 20 identifies the long term cumulative Level of Service projected at study intersections under the No Project condition. With one exception, these locations will satisfy the adopted minimum LOS standard.

The Douglas Blvd / Woodgrove Way / Quail Oaks Drive intersection is projected to operate at LOS F in the a.m. and p.m. peak hour if no improvements are made. To improve the Level of Service at this location, the Woodgrove Way and Quail Oaks Drive approaches will need to be limited to right turns only, although left turns from Douglas Blvd can be permitted at each direction. This improvement would yield LOS D at the intersection, and LOS D is within the LOS E minimum established by the Granite Bay Community Plan.

Roadway Segment Levels of Service Based on General Plan Thresholds. Table 21 identifies projected daily traffic volumes under the Cumulative No Project condition. The same locations which are already deficient under existing conditions would continue to operate with Level of Service that exceeds the minimum standards of the GBCP. The four lane segments of Douglas Blvd from Cavitt Stallman Road to Auburn Folsom Road would operate at LOS F.

## Cumulative Plus Project Conditions

Intersection Level of Service. Projected cumulative traffic volumes in this area of Granite Bay will increase if the project is developed, and the length of delays experienced during peak hours will increase slightly at study intersections. One location will operate with Level of Service that exceeds minimum standards. As shown in Table 20 without improvements LOS F conditions will remain at the Douglas Blvd / Woodgrove Way / Quail Oaks Drive intersection. Because the minimum LOS E standard is exceeded with and without the project, the significance of the project's impact is determined based on the change in overall delay. In this case, because the incremental change is less than the 2.4 second increment permitted under adopted methodology, the project's impact is not significant, and mitigation is not required.

## TABLE 20

YEAR 2036 PLUS PROJECT PEAK HOUR INTERSECTION LEVELS OF SERVICE

| Intersection | Control | AM Peak Hour |  |  |  | PM Peak Hour |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Year 2036 No Project |  | Year 2036 With Project |  | Year 2036 No Project |  | Year 2036 with Project |  |
|  |  | LOS | Average Delay (sec/veh) | LOS | Average Delay (sec/veh) | LOS | Average Delay (sec/veh) | LOS | Average Delay (sec/veh) |
| Douglas Blvd / Sierra College Blvd | Signal | E | 63.0 | E | 64.5 | E | 71.5 | E | 73.0 |
| Douglas Blvd / Woodgrove Way <br> (overall) <br> Eastbound left turn <br> Westbound left turn <br> Northbound left + thru + right turn <br> Southbound left+thru+right turn | NB/SB Stop | $\begin{gathered} \text { (F) } \\ \mathrm{C} \\ \mathrm{C} \\ \mathrm{~F} \\ \mathrm{C} \end{gathered}$ | $\begin{gathered} (517.0) \\ 20.5 \\ 17.0 \\ >999 \\ 55.5 \end{gathered}$ | $\begin{gathered} (\mathbf{F}) \\ \mathrm{C} \\ \mathrm{C} \\ \mathrm{~F} \\ \mathrm{C} \end{gathered}$ | $\begin{gathered} \mathbf{( 5 1 9 . 0}) \\ 20.5 \\ 17.5 \\ >999 \\ 56.0 \end{gathered}$ | $\begin{gathered} \text { (F) } \\ \mathrm{C} \\ \mathrm{C} \\ \mathrm{~F} \\ \mathrm{~F} \\ \hline \end{gathered}$ | $\begin{gathered} \mathbf{( 7 8 4 . 5 )} \\ 18.5 \\ 24.5 \\ >999 \\ 141.0 \end{gathered}$ | (F) <br> C <br> C <br> F <br> F | $\begin{gathered} \mathbf{( 7 7 3 . 5 )} \\ 19.0 \\ 25.0 \\ >999 \\ 141.5 \\ \hline \end{gathered}$ |
| Douglas Blvd / Seeno Avenue | Signal | B | 15.0 | B | 15.5 | B | 14.5 | B | 14.5 |
| Douglas Blvd / Granite Estates Drive (overall) <br> Westbound left turn <br> Northbound right turn | NB Stop | (C) <br> C <br> C | $\begin{gathered} (19.0) \\ 16.5 \\ 21.0 \end{gathered}$ | (C) <br> C <br> C | $\begin{gathered} (19.5) \\ 17.0 \\ 21.5 \end{gathered}$ | (E) <br> C <br> F | $\begin{gathered} (47.0) \\ 24.5 \\ 56.0 \end{gathered}$ | $\begin{gathered} \text { (E) } \\ \text { D } \\ \text { F } \end{gathered}$ | $\begin{gathered} (47.0) \\ 27.5 \\ 57.5 \end{gathered}$ |
| Douglas Blvd / Berg Street (overall) Eastbound left turn Westbound left turn Northbound right turn Southbound right turn | NB/SB Stop | $\begin{aligned} & \text { (C) } \\ & \text { D } \\ & \text { B } \\ & \mathrm{C} \\ & \mathrm{D} \\ & \hline \end{aligned}$ | $\begin{gathered} (22.0) \\ 23.5 \\ 15.0 \\ 15.0 \\ 27.0 \\ \hline \end{gathered}$ | $\begin{aligned} & \text { (C) } \\ & \text { D } \\ & \text { B } \\ & \mathrm{C} \\ & \mathrm{D} \\ & \hline \end{aligned}$ | $\begin{gathered} (24.0) \\ 26.5 \\ 14.5 \\ 15.0 \\ 28.0 \\ \hline \end{gathered}$ | $\begin{gathered} \text { (C) } \\ \mathrm{C} \\ \mathrm{C} \\ \mathrm{C} \\ \mathrm{C} \\ \hline \end{gathered}$ | $\begin{gathered} (23.5) \\ 25.0 \\ 22.0 \\ 21.5 \\ 23.5 \\ \hline \end{gathered}$ | (D) <br> D <br> C <br> C <br> D | $\begin{gathered} (27.0) \\ 25.5 \\ 22.5 \\ 22.0 \\ 31.5 \\ \hline \end{gathered}$ |
| Douglas Blvd / Barton Road | Signal | Cc | 34.5 | D | 35.0 | C | 33.5 | C | 34.0 |
| Douglas Blvd / Auburn - Folsom Road | Signal | E | 51.5 | E | 52.0 | D | 49.0 | D | 49.0 |
| Barton Road / Eureka Road | Signal | C | 30.0 | C | 30.5 | C | 21.5 | C | 21.5 |
|  | roundabout | C | 16.5 | C | 17.5 | B | 11.5 | B | 11.5 |
| Berg Street / Access <br> (overall) <br> Northbound Left turn <br> Southbound left turn <br> Eastbound left+right turn <br> Westbound left+right turn | EB/WB Stop | (A) <br> A <br> A | $\begin{gathered} (7.5) \\ 7.5 \\ - \\ 8.5 \end{gathered}$ | (A) <br> A <br> A <br> A <br> B | $\begin{gathered} (8.0) \\ 7.5 \\ 7.5 \\ 8.5 \\ 10.0 \\ \hline \end{gathered}$ | (A) <br> A <br> A | $\begin{gathered} (8.5) \\ 7.5 \\ - \\ 9.0 \end{gathered}$ | (A) <br> A <br> A <br> B | $\begin{gathered} (9.5) \\ 7.5 \\ - \\ 9.0 \\ 10.5 \\ \hline \end{gathered}$ |

[^4]| TABLE 21 <br> YEAR 2036 WITH QUARRY RIDGE ROADWAY SEGMENT LEVELS OF SERVICE |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Roadway | Location | Class | Lane | Year 2036 <br> No Project |  | Year 2036 <br> with Quarry Ridge |  |  |  |
|  |  |  |  |  |  | Daily | ume |  | Change in |
|  |  |  |  | Volume | LOS | Project <br> Alone | Total | LOS | $\mathbf{V} / \mathbf{C}$ |
| Douglas Blvd | Sierra College Blvd to Cavitt Stallman Rd | Arterial Moderate Access Control | 6 | 54,380 | F | 320 | 54,700 | F | 0.006 |
|  | Cavitt Stallman Rd to Woodgrove Way | Arterial High <br> Access control | 4 | 51,980 | F | 320 | 52,300 | F | 0.008 |
|  | Woodgrove Way to Seeno Avenue |  | 4 | 50,510 | F | 340 | 50,850 | F | 0.009 |
|  | Seeno Avenue to Berg Street |  | 4 | 50,160 | F | 340 | 50,500 | F | 0.009 |
|  | Berg Street to Barton Rd |  | 4 | 47,560 | F | 190 | 47,750 | F | 0.005 |
|  | Barton Rd to Joe Rodgers Rd |  | 4 | 48,340 | F | 110 | 48,450 | F | 0.003 |
|  | Joe Rodgers Rd to Auburn Folsom Rd |  | 4 | 47,390 | F | 110 | 47,500 | F | 0.003 |
| Berg Street | Olive Ranch Rd to Project | Arterial Low <br> Access Control | 2 | 1,460 | A | 40 | 1,500 | A | 0.003 |
|  | Olive Ranch Rd to Douglas Blvd |  | 2 | 1,420 | A | 530 | 1,950 | A | 0.035 |

Roadway Segments based on General Plan Thresholds. Table 25 identifies the project's daily traffic volume contribution to study area roadway segments under the Year 2036 condition and resulting Levels of Service. As indicated the projected conditions exceed GBCP minimum standards on Douglas Blvd, although the project will not change the Level of Service occurring on any roadway segment. The project will add traffic to roadways that are deficient under background conditions based on General Plan thresholds. In this case the significance of project impact is based on the criteria included under Placer County Methodology of Assessment, and the project contribution has been evaluated accordingly.

The project's incremental change can be described in terms of its change in roadway volume / capacity ratio. As was the case under other scenarios, the project's contribution to Douglas Blvd ranges from 0.003 to 0.009 . As these changes are less than the 0.050 increment permitted under Placer County methodology, the project's impact is not significant under this metric.

The second criteria is the "vehicles per lane" (vpl) traffic increase. As was discussed under Existing plus Project conditions, the project adds 28 to 85 vpl at various locations on Douglas Blvd. Because these increments do not exceed the 100 vpl threshold permitted under Placer County methodology, the project's impact is not significant.

## IMPACTS / MITIGATIONS

Improvements required to mitigate identified deficiencies and reduce project impacts to a less than significant level are summarized in this section.

The Placer County Road Network Traffic Fee Program identifies intersection and roadway improvements needed within various districts in the County. Improvements are intended to be funded in part by the development fee, with State funding, local programs and developer frontage improvements intended to fund the balance of the improvement costs. The project site is located within the Granite Bay Benefit District.

## Existing Conditions

Intersection Level of Service. Two intersections operate with Levels of Service that exceed the GBCP's minimum standards.

The Douglas Blvd / Woodgrove Way / Quail Oaks Drive intersection operates at LOS F. Eliminating side street left turns and through traffic while continuing to allow left turns from Douglas Blvd would yield satisfactory Level of Service (i.e., LOS E or better).

The Eureka Road / Barton Road intersection operates at LOS F in the a.m. peak hour. The Granite Bay Fee District / CIP includes funds for a traffic signal or roundabout at this location. Either of which could yield satisfactory operating conditions (i.e., LOS C or better).

No other intersection improvements have been found to be needed through this analysis to address existing conditions. At other locations satisfactory intersection operations are currently experienced and minimum Level of Service goals of the Granite Bay Community Plan are met.

Roadway Segment Level of Service based on General Plan Thresholds. The four lane segments of Douglas Blvd from Sierra College Blvd to Auburn Folsom Road carry daily traffic volumes that yield LOS F under the Placer County General Plan thresholds. Theoretically the road would need to be widened to six lanes. LOS D would result between Sierra College Blvd and Cavitt Stallman Road, and LOS C would result elsewhere. However, the GBCP does not support a six lane roadway and funding for such an improvement has not been identified.

## Existing Plus Project Conditions

Intersection Level of Service. No additional intersections will have deficient Level of Service as a result of the project. Development of the proposed project will result in significant impact to the Douglas Blvd / Woodgrove Way / Quail Oak Drive intersection under Placer County Methodology of Assessment.

Mitigation T-1. The project proponents shall be responsible for installing a feature in the median opening that will continue to permit eastbound and westbound left turns from Douglas Blvd onto Quail Oaks Drive and onto Woodgrove Way, while prohibiting northbound and southbound thru
traffic across Douglas Blvd as well as left turns onto Douglas Blvd from either approach. Implementation of this mitigation measure will not only result in this impact of the project being less than significant, but will improve the level of service at the intersection from a currently unacceptable LOS of F (with and without the project) to LOS C.

Roadway Segment Level of Service. Development of the proposed project will not result in significant impacts to roadway segments under Placer County Methodology of Assessment. Thus, no mitigations are required based on Roadway Segment Level of Service.

Douglas Blvd Median Openings. The left turn lanes on Douglas Blvd approaching Berg Street (eastbound) and Granite Estates Drive (westbound) have recently been lengthened, and both provide adequate space for waiting queues. Like other locations on Douglas Blvd both require approaching motorists to slow in the \#1 through lane in order to decelerate prior to waiting queues. However, under Existing plus Project conditions the incremental difference in speed between through traffic and vehicles entering the turn lanes satisfies Highway Design Manual guidance. No mitigation is required.

The project will contribute its fair share to the cost of regional circulation system improvements by paying adopted fees and will make frontage and access improvements described herein, and no additional off-site improvements are required to mitigate direct project impacts based on Level of Service.

## Existing Plus Approved / Pending Projects

Intersection Level of Service. Three intersections will operate with Levels of Service that exceed the GBCP's minimum standards.

The Douglas Blvd / Woodgrove Way / Quail Oaks Drive intersection will operate at LOS F. Eliminating side street left turns and through traffic while continuing to allow left turns from Douglas Blvd would yield satisfactory Level of Service (i.e., LOS E or better).

The Douglas Blvd / Granite Estates Drive intersection will operate at an overall LOS F. Because outbound left turns are already permitted no other improvements would reduce the overall length of delays at this location.

The Eureka Road / Barton Road intersection will operate at LOS F. The Granite Bay Fee District / CIP includes funds for a traffic signal or roundabout at this location, and either of which could yield satisfactory operating conditions (i.e., LOS C or better).

Roadway Segment Level of Service based on General Plan Thresholds. The four lane segments of Douglas Blvd from Sierra College Blvd to Auburn Folsom Road continue to carry daily traffic volumes that yield LOS F under the Placer County General Plan thresholds. Theoretically the road would need to be widened to six lanes. LOS E would result between Sierra College Blvd and Cavitt Stallman Road, LOS D would generally result between Cavitt Stallman Road and Joe Rodgers and LOS C would east of Joe Rodgers Road. However, the

GBCP does not support a six lane roadway and funding for such an improvement has not been identified.

Douglas Blvd Median Openings. The left turn lanes on Douglas Blvd approaching Berg Street (eastbound) and Granite Estates Drive (westbound) will provide adequate space for waiting queues. Under Existing plus Approved / Pending Projects conditions the incremental difference in speed between through traffic and vehicles entering the turn lanes will satisfies Highway Design Manual guidance. No improvement is required.

## EPAP Plus Project Conditions

Intersection Level of Service. No additional intersections will have deficient Level of Service as a result of the project. Development of the proposed project will not result in significant impacts to intersections under Placer County Methodology of Assessment. Thus, no mitigations are required based on intersection Level of Service.

Roadway Segment Level of Service. Development of the proposed project will not result in significant impacts to roadway segments under Placer County Methodology of Assessment. Thus, no mitigations are required based on Roadway Segment Level of Service.

Douglas Blvd Median Openings. Under EPAP Plus Project conditions the incremental difference in speed between through traffic and vehicles entering the turn lane at Granite Estates Drive is 23 mph , which exceeds Highway Design Manual guidance. The existing landscaped median could be eliminated and replaced with a longer turn lane to provide more deceleration space.

Mitigation T-2. The project proponents shall be responsible for modifying the existing median on Douglas Blvd to lengthen the westbound left turn lane at Granite Estates Drive

## Cumulative Year 2036 No Project Conditions

Intersections. With anticipated and funded improvements background traffic volumes forecast for the year 2036 will meet minimum GBCP standard at all but one location. The Douglas Blvd / Woodgrove Way / Quail Oaks Drive intersection will operate at Level of Service F, which exceeds the minimum LOS E standard mandated by the Granite Bay Community Plan. To improve the Level of Service at this location, left turns and cross traffic will need to be prohibited. These improvements would result in compliance with current LOS polices.

Roadway Segment Levels of Service Based on General Plan Thresholds. The same locations which are already deficient under Existing conditions would continue to operate with Level of Service that exceeds the minimum standards of the GBCP. The four lane segments of Douglas Blvd from Cavitt Stallman Road to Auburn Folsom Road would operate at LOS F.

## Cumulative Year 2036 Plus Project Conditions

Intersections. Development of the project would result in minor increases in the length of delays projected at study area intersections, but the incremental impact of the project is not judged to be significant under Placer County standards. Thus, while the project should contribute its fair share to the cost of regional circulation improvements by paying adopted traffic impact mitigation fees applicable to the Granite Bay area, no other mitigation is needed based on Level of Service.

Roadway Segments based on General Plan Thresholds. The project will add traffic to roadways that are deficient under background conditions based on General Plan thresholds. However, the project's incremental changes in roadway volume / capacity ratio are less than the 0.050 increment permitted under Placer County methodology, the project's impact is not significant under this metric. The project adds fewer than 100 vehicles per day per lane, and because these increments do not exceed the 100 vpl threshold permitted under Placer County methodology, the project's impact is not significant. No mitigation is required

Douglas Blvd Median Openings. Under Year 2036 Plus Project conditions the incremental difference in speed between through traffic and vehicles entering the turn lane at Granite Estates Drive is 23 mph , which exceeds Highway Design Manual guidance. The existing landscaped median could be eliminated and replaced with a longer turn lane to provide more deceleration space.

Mitigation T-2. The project proponents shall be responsible for modifying the existing median on Douglas Blvd to lengthen the westbound left turn lane at Granite Estates Drive.

## APPENDIX



Sierra College Blvd \& Douglas Blvd


Total Ins \& Outs


Total Volume Per Leg


# National Data and Surveying Services 

## All Vehicles \& Uturns On Unshifted

Bikes \& Peds On Bank 1
Heavy Trucks On Bank $2 \quad$ Unshifted Count $=$ All Vehicles \& Uturns

|  | Quail Oaks Dr / Woodgrove Way Southbound |  |  |  |  | Douglas Blvd Westbound |  |  |  |  | Quail Oaks Dr / Woodgrove Way Northbound |  |  |  |  | Douglas Blvd Eastbound |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| START TIME | LEFT | THRU | RIGHT | UTURNS | APP.TOTAL | LEFT | THRU | RIGHT | UTURNS | APP.TOTAL | LEFT | THRU | RIGHT | UTURNS | APP.TOTAL | LEFT | THRU | RIGHT | UTURNS | APP.TOTAL | Total | Uturns Total |
| 7:00 | 1 | 0 | 12 | 0 | 13 | 15 | 389 | 1 | 0 | 405 | 2 | 0 | 7 | 0 | 9 | 7 | 285 | 13 | 0 | 305 | 732 | 0 |
| 7:15 | 0 | 1 | 10 | 0 | 11 | 28 | 393 | 0 | 0 | 421 | 0 | 0 | 13 | 0 | 13 | 1 | 342 | 8 | 0 | 351 | 796 | 0 |
| 7:30 | 0 | 0 | 19 | 0 | 19 | 17 | 464 | 1 | 1 | 483 | 0 | 0 | 20 | 0 | 20 | 5 | 380 | 8 | 0 | 393 | 915 | 1 |
| 7:45 | 0 | 1 | 19 | 0 | 20 | 9 | 485 | 1 | 0 | 495 | 3 | 0 | 15 | 0 | 18 | 8 | 316 | 11 | 0 | 335 | 868 | 0 |
| Total | 1 | 2 | 60 | 0 | 63 | 69 | 1731 | 3 | 1 | 1804 | 5 | 0 | 55 | 0 | 60 | 21 | 1323 | 40 | 0 | 1384 | 3311 | 1 |
| 8:00 | 0 | 0 | 18 | 0 | 18 | 8 | 457 | 1 | 0 | 466 | 2 | 0 | 10 | 0 | 12 | 7 | 349 | 10 | 0 | 366 | 862 | 0 |
| 8:15 | 0 | 0 | 43 | 0 | 43 | 6 | 414 | 4 | 0 | 424 | 0 | 0 | 12 | 0 | 12 | 19 | 299 | 5 | 0 | 323 | 802 | 0 |
| 8:30 | 0 | 0 | 37 | 0 | 37 | 13 | 466 | 2 | 0 | 481 | 0 | 0 | 5 | 0 | 5 | 5 | 351 | 10 | 0 | 366 | 889 | 0 |
| 8:45 | 1 | 0 | 25 | 0 | 26 | 16 | 413 | 2 | 1 | 432 | 1 | 0 | 16 | 0 | 17 | 7 | 319 | 7 | 2 | 335 | 810 | 3 |
| Total | 1 | 0 | 123 | 0 | 124 | 43 | 1750 | 9 | 1 | 1803 | 3 | 0 | 43 | 0 | 46 | 38 | 1318 | 32 | 2 | 1390 | 3363 | 3 |


| 16:00 | 1 | 0 | 16 | 1 | 18 | 7 | 403 | 2 | 0 | 412 | 1 | 0 | 9 | 0 | 10 | 14 | 472 | 7 | 0 | 493 | 933 | 1 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 16:15 | 0 | 0 | 11 | 0 | 11 | 8 | 407 | 4 | 0 | 419 | 0 | 0 | 11 | 0 | 11 | 10 | 414 | 9 | 1 | 434 | 875 | 1 |
| 16:30 | 0 | 0 | 12 | 0 | 12 | 8 | 477 | 4 | 0 | 489 | 0 | 0 | 8 | 0 | 8 | 9 | 503 | 14 | 2 | 528 | 1037 | 2 |
| 16:45 | 0 | 0 | 11 | 0 | 11 | 9 | 449 | 1 | 0 | 459 | 0 | 0 | 4 | 0 | 4 | 10 | 463 | 12 | 0 | 485 | 959 | 0 |
| Total | 1 | 0 | 50 | 1 | 52 | 32 | 1736 | 11 | 0 | 1779 | 1 | 0 | 32 | 0 | 33 | 43 | 1852 | 42 | 3 | 1940 | 3804 | 4 |
| 17:00 | 0 | 1 | 7 | 0 | 8 | 10 | 447 | 0 | 0 | 457 | 1 | 0 | 12 | 0 | 13 | 8 | 510 | 11 | 1 | 530 | 1008 | 1 |
| 17:15 | 0 | 0 | 9 | 0 | 9 | 5 | 428 | 2 | 0 | 435 | 0 | 0 | 14 | 0 | 14 | 15 | 489 | 19 | 0 | 523 | 981 | 0 |
| 17:30 | 0 | 0 | 10 | 0 | 10 | 7 | 408 | 1 | 0 | 416 | 1 | 0 | 2 | 0 | 3 | 9 | 442 | 12 | 0 | 463 | 892 | 0 |
| 17:45 | 0 | 0 | 11 | 0 | 11 | 9 | 428 | 1 | 0 | 438 | 1 | 0 | 8 | 0 | 9 | 19 | 433 | 11 | 1 | 464 | 922 | 1 |
| Total | 0 | 1 | 37 | 0 | 38 | 31 | 1711 | 4 | 0 | 1746 | 3 | 0 | 36 | 0 | 39 | 51 | 1874 | 53 | 2 | 1980 | 3803 | 2 |
| Grand Total | 3 | 3 | 270 | 1 | 277 | 175 | 6928 | 27 | 2 | 7132 | 12 | 0 | 166 | 0 | 178 | 153 | 6367 | 167 | 7 | 6694 | 14281 | 10 |
| Apprch \% | 1.1\% | 1.1\% | 97.5\% | 0.4\% |  | 2.5\% | 97.1\% | 0.4\% | 0.0\% |  | 6.7\% | 0.0\% | 93.3\% | 0.0\% |  | 2.3\% | 95.1\% | 2.5\% | 0.1\% |  |  |  |
| Total \% | 0.0\% | 0.0\% | 1.9\% | 0.0\% | 1.9\% | 1.2\% | 48.5\% | 0.2\% | 0.0\% | 49.9\% | 0.1\% | 0.0\% | 1.2\% | 0.0\% | 1.2\% | 1.1\% | 44.6\% | 1.2\% | 0.0\% | 46.9\% | 100.0\% |  |


| $\begin{array}{\|c\|} \hline \text { AM PEAK } \\ \text { HOUR } \\ \hline \end{array}$ | Quail Oaks Dr / Woodgrove Way Southbound |  |  |  |  | Douglas Blvd Westbound |  |  |  |  | Quail Oaks Dr / Woodgrove Way Northbound |  |  |  |  | Douglas Blvd Eastbound |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| START TIME | LEFT | THRU | RIGHT | UTURNS | APP.TOTAL | LEFT | THRU | RIGHT | UTURNS | APP.TOTAL | LEFT | THRU | RIGHT | UTURNS | APP.TOTAL | LEFT | THRU | RIGHT | UTURNS | APP.TOTAL | Total |
| Peak Hour Analysis From 07:30 to 08:30 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Peak Hour For Entire Intersection Begins at 07:30 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7:30 | 0 | 0 | 19 | 0 | 19 | 17 | 464 | 1 | 1 | 483 | 0 | 0 | 20 | 0 | 20 | 5 | 380 | 8 | 0 | 393 | 915 |
| 7:45 | 0 | 1 | 19 | 0 | 20 | 9 | 485 | 1 | 0 | 495 | 3 | 0 | 15 | 0 | 18 | 8 | 316 | 11 | 0 | 335 | 868 |
| 8:00 | 0 | 0 | 18 | 0 | 18 | 8 | 457 | 1 | 0 | 466 | 2 | 0 | 10 | 0 | 12 | 7 | 349 | 10 | 0 | 366 | 862 |
| 8:15 | 0 | 0 | 43 | 0 | 43 | 6 | 414 | 4 | 0 | 424 | 0 | 0 | 12 | 0 | 12 | 19 | 299 | 5 | 0 | 323 | 802 |
| Total Volume | 0 | 1 | 99 | 0 | 100 | 40 | 1820 | 7 | 1 | 1868 | 5 | 0 | 57 | 0 | 62 | 39 | 1344 | 34 | 0 | 1417 | 3447 |
| \% App Total | 0.0\% | 1.0\% | 99.0\% | 0.0\% |  | 2.1\% | 97.4\% | 0.4\% | 0.1\% |  | 8.1\% | 0.0\% | 91.9\% | 0.0\% |  | 2.8\% | 94.8\% | 2.4\% | 0.0\% |  |  |
| PHF\| | . 000 | . 250 | . 576 | . 000 | . 581 | . 588 | . 938 | . 438 | . 250 | . 943 | 417 | . 000 | . 713 | . 000 | . 775 | . 513 | . 884 | . 773 | . 000 | . 901 | 942 |
| PM PEAK <br> HOUR | Quail Oaks Dr / Woodgrove Way Southbound |  |  |  |  | Douglas Blvd Westbound |  |  |  |  | Quail Oaks Dr / Woodgrove Way Northbound |  |  |  |  | Douglas Blvd Eastbound |  |  |  |  |  |
| START TIME | LEFT | THRU | RIGHT | UTURNS | APP.TOTAL | LEFT | THRU | RIGHT | UTURNS | APP.TOTAL | LEFT | THRU | RIGHT | UTURNS | APP.TOTAL | LEFT | THRU | RIGHT | UTURNS | APP.TOTAL | Total |
| Peak Hour Analysis From 16:30 to 17:30 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Peak Hour For Entire Intersection Begins at 16:30 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 16:30 | 0 | 0 | 12 | 0 | 12 | 8 | 477 | 4 | 0 | 489 | 0 | 0 | 8 | 0 | 8 | 9 | 503 | 14 | 2 | 528 | 1037 |
| 16:45 | 0 | 0 | 11 | 0 | 11 | 9 | 449 | 1 | 0 | 459 | 0 | 0 | 4 | 0 | 4 | 10 | 463 | 12 | 0 | 485 | 959 |
| 17:00 | 0 | 1 | 7 | 0 | 8 | 10 | 447 | 0 | 0 | 457 | 1 | 0 | 12 | 0 | 13 | 8 | 510 | 11 | 1 | 530 | 1008 |
| 17:15 | 0 | 0 | 9 | 0 | 9 | 5 | 428 | 2 | 0 | 435 | 0 | 0 | 14 | 0 | 14 | 15 | 489 | 19 | 0 | 523 | 981 |
| Total Volume | 0 | 1 | 39 | 0 | 40 | 32 | 1801 | 7 | 0 | 1840 | 1 | 0 | 38 | 0 | 39 | 42 | 1965 | 56 | 3 | 2066 | 3985 |
| \% App Total | 0.0\% | 2.5\% | 97.5\% | 0.0\% |  | 1.7\% | 97.9\% | 0.4\% | 0.0\% |  | 2.6\% | 0.0\% | 97.4\% | 0.0\% |  | 2.0\% | 95.1\% | 2.7\% | 0.1\% |  |  |
| PHF\| | . 000 | . 250 | . 813 | . 000 | 833 | . 800 | . 944 | . 438 | . 000 | . 941 | 250 | . 000 | . 679 | . 000 | . 696 | . 700 | . 963 | . 737 | . 375 | . 975 | 961 |



Total Ins \& Outs


Total Volume Per Leg


# National Data and Surveying Services 



All Vehicles \& Uturns On Unshifted
Bikes \& Peds On Bank 1
Heavy Trucks On Bank 2

|  | Seeno Ave Southbound |  |  |  |  | Douglas Blvd Westbound |  |  |  |  | Seeno Ave Northbound |  |  |  |  | Douglas Blvd Eastbound |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| START TIME | LEFT | THRU | RIGHT | UTURNS | APP.TOTAL | LEFT | THRU | RIGHT | UTURNS | APP.TOTAL | LEFT | THRU | RIGHT | UTURNS | APP.TOTAL | LEFT | THRU | RIGHT | UTURNS | APP.TOTAL | Total | Uturns Total |
| 7:00 | 5 | 0 | 22 | 0 | 27 | 0 | 387 | 4 | 0 | 391 | 0 | 0 | 0 | 0 | 0 | 3 | 278 | 0 | 0 | 281 | 699 | 0 |
| 7:15 | 13 | 0 | 16 | 0 | 29 | 0 | 415 | 1 | 0 | 416 | 0 | 0 | 0 | 0 | 0 | 2 | 358 | 0 | 0 | 360 | 805 | 0 |
| 7:30 | 5 | 0 | 14 | 0 | 19 | 0 | 485 | 5 | 1 | 491 | 0 | 0 | 0 | 0 | 0 | 5 | 398 | 0 | 0 | 403 | 913 | 1 |
| 7:45 | 8 | 0 | 10 | 0 | 18 | 0 | 472 | 6 | 1 | 479 | 0 | 0 | 0 | 0 | 0 | 13 | 318 | 0 | 1 | 332 | 829 | 2 |
| Total | 31 | 0 | 62 | 0 | 93 | 0 | 1759 | 16 | 2 | 1777 | 0 | 0 | 0 | 0 | 0 | 23 | 1352 | 0 | 1 | 1376 | 3246 |  |
| 8:00 | 7 | 0 | 7 | 0 | 14 | 0 | 464 | 25 | 0 | 489 | 0 | 0 | 0 | 0 | 0 | 17 | 337 | 0 | 0 | 354 | 857 | 0 |
| 8:15 | 30 | 0 | 15 | 0 | 45 | 0 | 449 | 46 | 0 | 495 | 0 | 0 | 0 | 0 | 0 | 22 | 303 | 0 | 0 | 325 | 865 | 0 |
| 8:30 | 34 | 0 | 21 | 0 | 55 | 0 | 433 | 6 | 0 | 439 | 0 | 0 | 0 | 0 | 0 | 4 | 350 | 0 | 0 | 354 | 848 | 0 |
| 8:45 | 6 | 0 | 10 | 0 | 16 | 0 | 399 | 2 | 0 | 401 | 0 | 0 | 0 | 0 | 0 | 9 | 322 | 0 | 0 | 331 | 748 | 0 |
| Total | 77 | 0 | 53 | 0 | 130 | 0 | 1745 | 79 | 0 | 1824 | 0 | 0 | 0 | 0 | 0 | 52 | 1312 | 0 | 0 | 1364 | 3318 | 0 |


| 16:00 | 18 | 0 | 8 | 0 | 26 | 0 | 395 | 7 | 1 | 403 | 0 | 0 | 0 | 0 | 0 | 10 | 476 | 0 | 0 | 486 | 915 | 1 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 16:15 | 0 | 0 | 6 | 0 | 6 | 0 | 423 | 5 | 2 | 430 | 0 | 0 | 0 | 0 | 0 | 2 | 425 | 0 | 1 | 428 | 864 | 3 |
| 16:30 | 11 | 0 | 5 | 0 | 16 | 0 | 434 | 5 | 0 | 439 | 0 | 0 | 0 | 0 | 0 | 9 | 471 | 0 | 2 | 482 | 937 | 2 |
| 16:45 | 8 | 0 | 2 | 0 | 10 | 0 | 431 | 7 | 0 | 438 | 0 | 0 | 0 | 0 | 0 | 7 | 441 | 0 | 2 | 450 | 898 | 2 |
| Total | 37 | 0 | 21 | 0 | 58 | 0 | 1683 | 24 | 3 | 1710 | 0 | 0 | 0 | 0 | 0 | 28 | 1813 | 0 | 5 | 1846 | 3614 | 8 |
| 17:00 | 7 | 0 | 9 | 0 | 16 | 0 | 449 | 5 | 0 | 454 | 0 | 0 | 0 | 0 | 0 | 7 | 515 | 0 | 1 | 523 | 993 | 1 |
| 17:15 | 5 | 0 | 12 | 0 | 17 | 0 | 426 | 2 | 0 | 428 | 0 | 0 | 0 | 0 | 0 | 2 | 496 | 0 | 1 | 499 | 944 | 1 |
| 17:30 | 6 | 0 | 8 | 0 | 14 | 0 | 423 | 4 | 0 | 427 | 0 | 0 | 0 | 0 | 0 | 13 | 434 | 0 | 0 | 447 | 888 | 0 |
| 17:45 | 7 | 0 | 5 | 0 | 12 | 0 | 441 | 5 | 1 | 447 | 0 | 0 | 0 | 0 | 0 | 4 | 444 | 0 | 0 | 448 | 907 | 1 |
| Total | 25 | 0 | 34 | 0 | 59 | 0 | 1739 | 16 | 1 | 1756 | 0 | 0 | 0 | 0 | 0 | 26 | 1889 |  | 2 | 1917 | 3732 | 3 |
| Grand Total | 170 | 0 | 170 | 0 | 340 | 0 | 6926 | 135 | 6 | 7067 | 0 | 0 | 0 | 0 | 0 | 129 | 6366 | 0 | 8 | 6503 | 13910 | 14 |
| Apprch \% | 50.0\% | 0.0\% | 50.0\% | 0.0\% |  | 0.0\% | 98.0\% | 1.9\% | 0.1\% |  | 0.0\% | 0.0\% | 0.0\% | 0.0\% |  | 2.0\% | 97.9\% | 0.0\% | 0.1\% |  |  |  |
| Total \% | 1.2\% | 0.0\% | 1.2\% | 0.0\% | 2.4\% | 0.0\% | 49.8\% | 1.0\% | 0.0\% | 50.8\% | 0.0\% | 0.0\% | 0.0\% | 0.0\% | 0.0\% | 0.9\% | 45.8\% | 0.0\% | 0.1\% | 46.8\% | 100.0\% |  |


| AM PEAK HOUR | Seeno Ave Southbound |  |  |  |  | Douglas Blvd Westbound |  |  |  |  | Seeno Ave Northbound |  |  |  |  | Douglas Blvd Eastbound |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| START TIME | LEFT | THRU | RIGHT | UTURNS | APP.TOTAL | LEFT | THRU | RIGHT | UTURNS | APP.TOTAL | LEFT | THRU | RIGHT | UTURNS | APP.TOTAL | LEFT | THRU | RIGHT | UTURNS | APP.TOTAL | Total |
| Peak Hour Analysis From 07:30 to 08:30 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Peak Hour For Entire Intersection Begins at 07:30 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7:30 | 5 | 0 | 14 | 0 | 19 | 0 | 485 | 5 | 1 | 491 | 0 | 0 | 0 | 0 | 0 | 5 | 398 | 0 | 0 | 403 | 913 |
| 7:45 | 8 | 0 | 10 | 0 | 18 | 0 | 472 | 6 | 1 | 479 | 0 | 0 | 0 | 0 | 0 | 13 | 318 | 0 | 1 | 332 | 829 |
| 8:00 | 7 | 0 | 7 | 0 | 14 | 0 | 464 | 25 | 0 | 489 | 0 | 0 | 0 | 0 | 0 | 17 | 337 | 0 | 0 | 354 | 857 |
| 8:15 | 30 | 0 | 15 | 0 | 45 | 0 | 449 | 46 | 0 | 495 | 0 | 0 | 0 | 0 | 0 | 22 | 303 | 0 | 0 | 325 | 865 |
| Total Volume | 50 | 0 | 46 | 0 | 96 | 0 | 1870 | 82 | 2 | 1954 | 0 | 0 | 0 | 0 | 0 | 57 | 1356 | 0 | 1 | 1414 | 3464 |
| \% App Total | 52.1\% | 0.0\% | 47.9\% | 0.0\% |  | 0.0\% | 95.7\% | 4.2\% | 0.1\% |  | 0.0\% | 0.0\% | 0.0\% | 0.0\% |  | 4.0\% | 95.9\% | 0.0\% | 0.1\% |  |  |
| PHF\| | . 417 | . 000 | . 767 | . 000 | . 533 | . 000 | . 964 | . 446 | . 500 | . 987 | . 000 | . 000 | . 000 | . 000 | . 000 | . 648 | . 852 | . 000 | . 250 | . 877 | . 949 |
| PM PEAK HOUR | Southbound |  |  |  |  | Westbound |  |  |  |  | Seeno Ave Northbound |  |  |  |  | Douglas Blvd Eastbound |  |  |  |  |  |
| START TIME | LEFT | THRU | RIGHT | UTURNS | APP.TOTAL | LEFT | THRU |  | UTURNS | APP.TOTAL | LEFT | THRU | RIGHT | UTURNS | APP.TOTAL | LEFT | THRU | RIGHT | UTURNS | APP.TOTAL | Total |
| Peak Hour Analysis From 16:30 to 17:30 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Peak Hour For Entire Intersection Begins at 16:30 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 16:30 | 11 | 0 | 5 | 0 | 16 | 0 | 434 | 5 | 0 | 439 | 0 | 0 | 0 | 0 | 0 | 9 | 471 | 0 | 2 | 482 | 937 |
| 16:45 | 8 | 0 | 2 | 0 | 10 | 0 | 431 | 7 | 0 | 438 | 0 | 0 | 0 | 0 | 0 | 7 | 441 | 0 | 2 | 450 | 898 |
| 17:00 | 7 | 0 | 9 | 0 | 16 | 0 | 449 | 5 | 0 | 454 | 0 | 0 | 0 | 0 | 0 | 7 | 515 | 0 | 1 | 523 | 993 |
| 17:15 | 5 | 0 | 12 | 0 | 17 | 0 | 426 | 2 | 0 | 428 | 0 | 0 | 0 | 0 | 0 | 2 | 496 | 0 | 1 | 499 | 944 |
| Total Volume | 31 | 0 | 28 | 0 | 59 | 0 | 1740 | 19 | 0 | 1759 | 0 | 0 | 0 | 0 | 0 | 25 | 1923 | 0 | 6 | 1954 | 3772 |
| \% App Total | 52.5\% | 0.0\% | 47.5\% | 0.0\% |  | 0.0\% | 98.9\% | 1.1\% | 0.0\% |  | 0.0\% | 0.0\% | 0.0\% | 0.0\% |  | 1.3\% | 98.4\% | 0.0\% | 0.3\% |  |  |
| PHF\| | . 705 | . 000 | . 583 | . 000 | . 868 | . 000 | . 969 | . 679 | . 000 | . 969 | . 000 | . 000 | . 000 | . 000 | . 000 | . 694 | . 933 | . 000 | . 750 | . 934 | . 950 |

Seeno Ave \& Douglas Blvd


Total Ins \& Outs


Total Volume Per Leg



Granite Estates Dr \& Douglas Blvd


Total Ins \& Outs


Total Volume Per Leg


# National Data and Surveying Services 

## All Vehicles \& Uturns On Unshifted

Bikes \& Peds On Bank 1
Heavy Trucks On Bank 2

|  | Berg St Southbound |  |  |  |  | Douglas Blvd Westbound |  |  |  |  | Berg St Northbound |  |  |  |  | Douglas Blvd Eastbound |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| START TIME | LEFT | THRU | RIGHT | UTURNS | APP.TOTAL | LEFT | THRU | RIGHT | UTURNS | APP.TOTAL | LEFT | THRU | RIGHT | UTURNS | APP.TOTAL | LEFT | THRU | RIGHT | UTURNS | APP.TOTAL | Total | Uturns Total |
| 7:00 | 0 | 0 | 7 | 0 | 7 | 5 | 374 | 0 | 2 | 381 | 0 | 0 | 0 | 0 | 0 | 11 | 271 | 0 | 0 | 282 | 670 | 2 |
| 7:15 | 0 | 0 | 17 | 0 | 17 | 9 | 396 | 2 | 1 | 408 | 0 | 0 | 1 | 0 | 1 | 5 | 357 | 0 | 0 | 362 | 788 | 1 |
| 7:30 | 0 | 0 | 13 | 0 | 13 | 5 | 464 | 3 | 0 | 472 | 0 | 0 | 1 | 0 | 1 | 8 | 371 | 1 | 0 | 380 | 866 | 0 |
| 7:45 | 0 | 0 | 20 | 0 | 20 | 12 | 469 | 3 | 1 | 485 | 0 | 0 | 0 | 0 | 0 | 7 | 334 | 3 | 0 | 344 | 849 | 1 |
| Total | 0 | 0 | 57 | 0 | 57 | 31 | 1703 | 8 | 4 | 1746 | 0 | 0 | 2 | 0 | 2 | 31 | 1333 | 4 | 0 | 1368 | 3173 | 4 |
| 8:00 | 0 | 0 | 15 | 0 | 15 | 8 | 450 | 2 | 1 | 461 | 0 | 0 | 1 | 0 | 1 | 12 | 306 | 1 | 2 | 321 | 798 | 3 |
| 8:15 | 0 | 0 | 16 | 0 | 16 | 7 | 451 | 1 | 0 | 459 | 0 | 0 | 0 | 0 | 0 | 9 | 340 | 2 | 0 | 351 | 826 | 0 |
| 8:30 | 0 | 0 | 18 | 0 | 18 | 11 | 442 | 1 | 1 | 455 | 0 | 0 | 1 | 0 | 1 | 5 | 350 | 0 | 0 | 355 | 829 | 1 |
| 8:45 | 0 | 0 | 20 | 0 | 20 | 13 | 351 | 1 | 1 | 366 | 0 | 0 | 4 | 0 | 4 | 12 | 327 | 8 | 1 | 348 | 738 | 2 |
| Total | 0 | 0 | 69 | 0 | 69 | 39 | 1694 | 5 | 3 | 1741 | 0 | 0 | 6 | 0 | 6 | 38 | 1323 | 11 | 3 | 1375 | 3191 | 6 |


| 16:00 | 0 | 0 | 16 | 0 | 16 | 13 | 393 | 4 | 2 | 412 | 0 | 0 | 3 | 0 | 3 | 17 | 443 | 5 | 1 | 466 | 897 | 3 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 16:15 | 0 | 0 | 15 | 0 | 15 | 7 | 384 | 6 | 1 | 398 | 0 | 0 | 3 | 0 | 3 | 7 | 427 | 8 | 0 | 442 | 858 | 1 |
| 16:30 | 0 | 0 | 8 | 0 | 8 | 8 | 425 | 1 | 2 | 436 | 0 | 0 | 4 | 0 | 4 | 8 | 443 | 9 | 1 | 461 | 909 | 3 |
| 16:45 | 0 | 0 | 10 | 0 | 10 | 10 | 412 | 1 | 1 | 424 | 0 | 0 | 2 | 0 | 2 | 14 | 426 | 4 | 4 | 448 | 884 | 5 |
| Total | 0 | 0 | 49 | 0 | 49 | 38 | 1614 | 12 | 6 | 1670 | 0 | 0 | 12 | 0 | 12 | 46 | 1739 | 26 | 6 | 1817 | 3548 | 12 |
| 17:00 | 0 | 0 | 16 | 0 | 16 | 13 | 439 | 2 | 0 | 454 | 0 | 0 | 2 | 0 | 2 | 10 | 479 | 7 | 3 | 499 | 971 | 3 |
| 17:15 | 0 | 0 | 14 | 0 | 14 | 5 | 396 | 6 | 1 | 408 | 0 | 0 | 3 | 0 | 3 | 24 | 467 | 5 | 4 | 500 | 925 | 5 |
| 17:30 | 0 | 0 | 15 | 0 | 15 | 13 | 396 | 5 | 1 | 415 | 0 | 0 | 3 | 0 | 3 | 12 | 423 | 7 | 5 | 447 | 880 | 6 |
| 17:45 | 0 | 0 | 25 | 0 | 25 | 20 | 417 | 4 | 0 | 441 | 0 | 0 | 2 | 0 | 2 | 15 | 413 | 3 | 2 | 433 | 901 | 2 |
| Total | 0 | 0 | 70 | 0 | 70 | 51 | 1648 | 17 | 2 | 1718 | 0 | 0 | 10 | 0 | 10 | 61 | 1782 | 22 | 14 | 1879 | 3677 | 16 |
| Grand Total | 0 | 0 | 245 | 0 | 245 | 159 | 6659 | 42 | 15 | 6875 | 0 | 0 | 30 | 0 | 30 | 176 | 6177 | 63 | 23 | 6439 | 13589 | 38 |
| Apprch \% | 0.0\% | 0.0\% | 100.0\% | 0.0\% |  | 2.3\% | 96.9\% | 0.6\% | 0.2\% |  | 0.0\% | 0.0\% | 100.0\% | 0.0\% |  | 2.7\% | 95.9\% | 1.0\% | 0.4\% |  |  |  |
| Total \% | 0.0\% | 0.0\% | 1.8\% | 0.0\% | 1.8\% | 1.2\% | 49.0\% | 0.3\% | 0.1\% | 50.6\% | 0.0\% | 0.0\% | 0.2\% | 0.0\% | 0.2\% | 1.3\% | 45.5\% | 0.5\% | 0.2\% | 47.4\% | 100.0\% |  |


| $\begin{array}{\|c\|} \hline \text { AM PEAK } \\ \text { HOUR } \\ \hline \end{array}$ | Berg St Southbound |  |  |  |  | Douglas Blvd Westbound |  |  |  |  | Berg St Northbound |  |  |  |  | Douglas Blvd Eastbound |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| START TIME | LEFT | THRU | RIGHT | UTURNS | APP.TOTAL | LEFT | THRU | RIGHT | UTURNS | APP.TOTAL | LEFT | THRU | RIGHT | UTURNS | APP.TOTAL | LEFT | THRU | RIGHT | UTURNS | APP.TOTAL | Total |
| Peak Hour Analysis From 07:30 to 08:30 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Peak Hour For Entire Intersection Begins at 07:30 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7:30 | 0 | 0 | 13 | 0 | 13 | 5 | 464 | 3 | 0 | 472 | 0 | 0 | 1 | 0 | 1 | 8 | 371 | 1 | 0 | 380 | 866 |
| 7:45 | 0 | 0 | 20 | 0 | 20 | 12 | 469 | 3 | 1 | 485 | 0 | 0 | 0 | 0 | 0 | 7 | 334 | 3 | 0 | 344 | 849 |
| 8:00 | 0 | 0 | 15 | 0 | 15 | 8 | 450 | 2 | 1 | 461 | 0 | 0 | 1 | 0 | 1 | 12 | 306 | 1 | 2 | 321 | 798 |
| 8:15 | 0 | 0 | 16 | 0 | 16 | 7 | 451 | 1 | 0 | 459 | 0 | 0 | 0 | 0 | 0 | 9 | 340 | 2 | 0 | 351 | 826 |
| Total Volume | 0 | 0 | 64 | 0 | 64 | 32 | 1834 | 9 | 2 | 1877 | 0 | 0 | 2 | 0 | 2 | 36 | 1351 | 7 | 2 | 1396 | 3339 |
| \% App Total | 0.0\% | 0.0\% | 100.0\% | 0.0\% |  | 1.7\% | 97.7\% | 0.5\% | 0.1\% |  | 0.0\% | 0.0\% | 100.0\% | 0.0\% |  | 2.6\% | 96.8\% | 0.5\% | 0.1\% |  |  |
| PHF\| | . 000 | . 000 | . 800 | . 000 | . 800 | . 667 | . 978 | . 750 | . 500 | . 968 | . 000 | . 000 | . 500 | . 000 | . 500 | . 750 | . 910 | . 583 | . 250 | . 918 | . 964 |
| PM PEAK HOUR | Berg St Southbound |  |  |  |  | Douglas Blvd Westbound |  |  |  |  | Berg St Northbound |  |  |  |  | Douglas Blvd Eastbound |  |  |  |  |  |
| START TIME | LEFT | THRU | RIGHT | UTURNS | APP.TOTAL | LEFT | THRU | RIGHT | UTURNS | APP.TOTAL | LEFT | THRU | RIGHT | UTURNS | APP.TOTAL | LEFT | THRU | RIGHT | UTURNS | APP.TOTAL | Total |
| Peak Hour Analysis From 16:30 to 17:30 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Peak Hour For Entire Intersection Begins at 16:30 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 16:30 | 0 | 0 | 8 | 0 | 8 | 8 | 425 | 1 | 2 | 436 | 0 | 0 | 4 | 0 | 4 | 8 | 443 | 9 | 1 | 461 | 909 |
| 16:45 | 0 | 0 | 10 | 0 | 10 | 10 | 412 | 1 | 1 | 424 | 0 | 0 | 2 | 0 | 2 | 14 | 426 | 4 | 4 | 448 | 884 |
| 17:00 | 0 | 0 | 16 | 0 | 16 | 13 | 439 | 2 | 0 | 454 | 0 | 0 | 2 | 0 | 2 | 10 | 479 | 7 | 3 | 499 | 971 |
| 17:15 | 0 | 0 | 14 | 0 | 14 | 5 | 396 | 6 | 1 | 408 | 0 | 0 | 3 | 0 | 3 | 24 | 467 | 5 | 4 | 500 | 925 |
| Total Volume | 0 | 0 | 48 | 0 | 48 | 36 | 1672 | 10 | 4 | 1722 | 0 | 0 | 11 | 0 | 11 | 56 | 1815 | 25 | 12 | 1908 | 3689 |
| \% App Total | 0.0\% | 0.0\% | 100.0\% | 0.0\% |  | 2.1\% | 97.1\% | 0.6\% | 0.2\% |  | 0.0\% | 0.0\% | 100.0\% | 0.0\% |  | 2.9\% | 95.1\% | 1.3\% | 0.6\% |  |  |
| PHF\| | . 000 | . 000 | . 750 | . 000 | . 750 | . 692 | . 952 | . 417 | . 500 | . 948 | . 000 | . 000 | . 68 | . 000 | 688 | 583 | . 947 | 694 | . 750 | 954 | 950 |

Berg St \& Douglas Blvd


Total Ins \& Outs


Total Volume Per Leg


# National Data and Surveying Services 

## City of Granite Bay <br> All Vehicles \& Uturns On Unshifted

Bikes \& Peds On Bank 1
Unshifted Count = All Vehicles \& Uturns

|  | Barton Rd Southbound |  |  |  |  | Douglas Blvd Westbound |  |  |  |  | Barton Rd Northbound |  |  |  |  | Douglas Blvd Eastbound |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| START TIME | LEFT | THRU | RIGHT | UTURNS | APP.TOTAL | LEFT | THRU | RIGHT | UTURNS | APP.TOTAL | LEFT | THRU | RIGHT | UTURNS | APP.TOTAL | LEFT | THRU | RIGHT | UTURNS | APP.TOTAL | Total | Uturns Total |
| 7:00 | 29 | 28 | 10 | 0 | 67 | 40 | 309 | 31 | 0 | 380 | 47 | 7 | 7 | 0 | 61 | 2 | 235 | 22 | 1 | 260 | 768 | 1 |
| 7:15 | 31 | 52 | 13 | 0 | 96 | 65 | 354 | 22 | 0 | 441 | 38 | 18 | 11 | 0 | 67 | 6 | 325 | 37 | 0 | 368 | 972 | 0 |
| 7:30 | 42 | 25 | 8 | 0 | 75 | 26 | 405 | 31 | 0 | 462 | 70 | 36 | 24 | 0 | 130 | 5 | 316 | 36 | 2 | 359 | 1026 | 2 |
| 7:45 | 24 | 17 | 6 | 0 | 47 | 19 | 422 | 31 | 0 | 472 | 65 | 25 | 30 | 0 | 120 | 11 | 284 | 28 | 4 | 327 | 966 | 4 |
| Total | 126 | 122 | 37 | 0 | 285 | 150 | 1490 | 115 | 0 | 1755 | 220 | 86 | 72 | 0 | 378 | 24 | 1160 | 123 | 7 | 1314 | 3732 | 7 |
| 8:00 | 40 | 22 | 7 | 1 | 70 | 23 | 383 | 30 | 1 | 437 | 42 | 19 | 11 | 0 | 72 | 10 | 262 | 29 | 3 | 304 | 883 | 5 |
| 8:15 | 38 | 27 | 15 | 0 | 80 | 17 | 387 | 37 | 0 | 441 | 49 | 21 | 17 | 0 | 87 | 14 | 275 | 45 | 0 | 334 | 942 | 0 |
| 8:30 | 30 | 18 | 11 | 0 | 59 | 28 | 388 | 37 | 0 | 453 | 44 | 21 | 15 | 0 | 80 | 10 | 318 | 43 | 1 | 372 | 964 | 1 |
| 8:45 | 28 | 21 | 5 | 0 | 54 | 26 | 293 | 34 | 0 | 353 | 39 | 13 | 23 | 0 | 75 | 11 | 259 | 34 | 1 | 305 | 787 | 1 |
| Total | 136 | 88 |  |  | 263 | 94 | 1451 | 138 | 1 | 1684 | 174 | 74 | 66 | 0 | 314 | 45 | 1114 | 151 | 5 | 1315 | 3576 | 7 |


| 16:00 | 35 | 21 | 9 | 0 | 65 | 18 | 336 | 37 | 0 | 391 | 32 | 19 | 24 | 0 | 75 | 11 | 372 | 57 | 0 | 440 | 971 | 0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 16:15 | 34 | 18 | 10 | 0 | 62 | 22 | 338 | 50 | 2 | 412 | 28 | 17 | 26 | 0 | 71 | 14 | 347 | 62 | 0 | 423 | 968 | 2 |
| 16:30 | 30 | 18 | 15 | 0 | 63 | 26 | 391 | 38 | 2 | 457 | 36 | 21 | 24 | 0 | 81 | 19 | 390 | 41 | 0 | 450 | 1051 | 2 |
| 16:45 | 35 | 27 | 12 | 0 | 74 | 14 | 362 | 33 | 2 | 411 | 31 | 10 | 34 | 0 | 75 | 7 | 365 | 51 | 0 | 423 | 983 | 2 |
| Total | 134 | 84 | 46 | 0 | 264 | 80 | 1427 | 158 | 6 | 1671 | 127 | 67 | 108 | 0 | 302 | 51 | 1474 | 211 | 0 | 1736 | 3973 | 6 |
| 17:00 | 34 | 17 | 18 | 0 | 69 | 21 | 390 | 44 | 2 | 457 | 34 | 22 | 23 | 0 | 79 | 5 | 414 | 51 | 4 | 474 | 1079 | 6 |
| 17:15 | 48 | 28 | 11 | 0 | 87 | 19 | 360 | 50 | 6 | 435 | 31 | 22 | 21 | 0 | 74 | 10 | 398 | 56 | 0 | 464 | 1060 | 6 |
| 17:30 | 50 | 34 | 8 | 0 | 92 | 27 | 368 | 42 | 0 | 437 | 27 | 18 | 20 | 0 | 65 | 11 | 359 | 53 | 5 | 428 | 1022 | 5 |
| 17:45 | 26 | 19 | 11 | 0 | 56 | 33 | 381 | 47 | 1 | 462 | 39 | 14 | 16 | 0 | 69 | 11 | 357 | 50 | 0 | 418 | 1005 | 1 |
| Total | 158 | 98 | 48 | 0 | 304 | 100 | 1499 | 183 | 9 | 1791 | 131 | 76 | 80 | 0 | 287 | 37 | 1528 | 210 | 9 | 1784 | 4166 | 18 |
| Grand Total | 554 | 392 | 169 | 1 | 1116 | 424 | 5867 | 594 | 16 | 6901 | 652 | 303 | 326 | 0 | 1281 | 157 | 5276 | 695 | 21 | 6149 | 15447 | 38 |
| Apprch \% | 49.6\% | 35.1\% | 15.1\% | 0.1\% |  | 6.1\% | 85.0\% | 8.6\% | 0.2\% |  | 50.9\% | 23.7\% | 25.4\% | 0.0\% |  | 2.6\% | 85.8\% | 11.3\% | 0.3\% |  |  |  |
| Total \% | 3.6\% | 2.5\% | 1.1\% | 0.0\% | 7.2\% | 2.7\% | 38.0\% | 3.8\% | 0.1\% | 44.7\% | 4.2\% | 2.0\% | 2.1\% | 0.0\% | 8.3\% | 1.0\% | 34.2\% | 4.5\% | 0.1\% | 39.8\% | 100.0\% |  |


| $\begin{array}{\|c\|} \hline \text { AM PEAK } \\ \text { HOUR } \\ \hline \end{array}$ | Barton Rd Southbound |  |  |  |  | Douglas Blvd Westbound |  |  |  |  | Barton Rd Northbound |  |  |  |  | Douglas Blvd Eastbound |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| START TIME | LEFT | THRU | RIGHT | UTURNS | APP.TOTAL | LEFT | THRU | RIGHT | UTURNS | APP.TOTAL | LEFT | THRU | RIGHT | UTURNS | APP.TOTAL | LEFT | THRU | RIGHT | UTURNS | APP.TOTAL | Total |
| Peak Hour Analysis From 07:15 to 08:15 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Peak Hour For Entire Intersection Begins at 07:15 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7:15 | 31 | 52 | 13 | 0 | 96 | 65 | 354 | 22 | 0 | 441 | 38 | 18 | 11 | 0 | 67 | 6 | 325 | 37 | 0 | 368 | 972 |
| 7:30 | 42 | 25 | 8 | 0 | 75 | 26 | 405 | 31 | 0 | 462 | 70 | 36 | 24 | 0 | 130 | 5 | 316 | 36 | 2 | 359 | 1026 |
| 7:45 | 24 | 17 | 6 | 0 | 47 | 19 | 422 | 31 | 0 | 472 | 65 | 25 | 30 | 0 | 120 | 11 | 284 | 28 | 4 | 327 | 966 |
| 8:00 | 40 | 22 | 7 |  | 70 | 23 | 383 | 30 | 1 | 437 | 42 | 19 | 11 | 0 | 72 | 10 | 262 | 29 | 3 | 304 | 883 |
| Total Volume | 137 | 116 | 34 | , | 288 | 133 | 1564 | 114 | 1 | 1812 | 215 | 98 | 76 | 0 | 389 | 32 | 1187 | 130 | 9 | 1358 | 3847 |
| \% App Total | 47.6\% | 40.3\% | 11.8\% | 0.3\% |  | 7.3\% | 86.3\% | 6.3\% | 0.1\% |  | 55.3\% | 25.2\% | 19.5\% | 0.0\% |  | 2.4\% | 87.4\% | 9.6\% | 0.7\% |  |  |
| PHF\| | . 815 | . 558 | . 654 | . 250 | . 750 | . 512 | . 927 | . 919 | . 250 | . 960 | . 768 | . 681 | . 633 | . 000 | . 748 | . 727 | . 913 | . 878 | . 563 | . 923 | . 937 |
| PM PEAK <br> HOUR | Barton Rd Southbound |  |  |  |  | Douglas Blvd Westbound |  |  |  |  | Barton Rd Northbound |  |  |  |  | Douglas Blvd Eastbound |  |  |  |  |  |
| START TIME | LEFT | THRU | RIGHT | UTURNS | APP.TOTAL | LEFT | THRU | RIGHT | UTURNS | APP.TOTAL | LEFT | THRU | RIGHT | UTURNS | APP.TOTAL | LEFT | THRU | RIGHT | UTURNS | APP.TOTAL | Total |
| Peak Hour Analysis From 16:30 to 17:30 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Peak Hour For Entire Intersection Begins at 16:30 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 16:30 | 30 | 18 | 15 | 0 | 63 | 26 | 391 | 38 | 2 | 457 | 36 | 21 | 24 | 0 | 81 | 19 | 390 | 41 | 0 | 450 | 1051 |
| 16:45 | 35 | 27 | 12 | 0 | 74 | 14 | 362 | 33 | 2 | 411 | 31 | 10 | 34 | 0 | 75 | 7 | 365 | 51 | 0 | 423 | 983 |
| 17:00 | 34 | 17 | 18 | 0 | 69 | 21 | 390 | 44 | 2 | 457 | 34 | 22 | 23 | 0 | 79 | 5 | 414 | 51 | 4 | 474 | 1079 |
| 17:15 | 48 | 28 | 11 | 0 | 87 | 19 | 360 | 50 | 6 | 435 | 31 | 22 | 21 | 0 | 74 | 10 | 398 | 56 | 0 | 464 | 1060 |
| Total Volume | 147 | 90 | 56 | 0 | 293 | 80 | 1503 | 165 | 12 | 1760 | 132 | 75 | 102 | 0 | 309 | 41 | 1567 | 199 | 4 | 1811 | 4173 |
| \% App Total | 50.2\% | 30.7\% | 19.1\% | 0.0\% |  | 4.5\% | 85.4\% | 9.4\% | 0.7\% |  | 42.7\% | 24.3\% | 33.0\% | 0.0\% |  | 2.3\% | 86.5\% | 11.0\% | 0.2\% |  |  |
| PHF\| | . 766 | . 804 | . 778 | . 000 | . 842 | . 769 | . 961 | . 825 | . 500 | . 963 | . 917 | . 852 | . 750 | . 000 | . 954 | . 539 | . 946 | . 888 | . 250 | . 955 | . 967 |

Barton Rd \& Douglas Blvd


Total Ins \& Outs


Total Volume Per Leg


# National Data and Surveying Services 

## City of Granite Bay <br> All Vehicles \& Uturns On Unshifted

Bikes \& Peds On Bank 1
Unshifted Count = All Vehicles \& Uturns

|  | Auburn-Folsom Rd Southbound |  |  |  |  | Douglas Blvd Westbound |  |  |  |  | Auburn-Folsom Rd Northbound |  |  |  |  | Douglas Blvd Eastbound |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| START TIME | LEFT | THRU | RIGHT | UTURNS | APP.TOTAL | LEFT | THRU | RIGHT | UTURNS | APP.TOTAL | LEFT | THRU | RIGHT | UTURNS | APP.TOTAL | LEFT | THRU | RIGHT | UTURNS | APP.TOTAL | Total | Uturns Total |
| 7:00 | 16 | 135 | 42 | 0 | 193 | 22 | 69 | 10 | 0 | 101 | 257 | 78 | 9 | 0 | 344 | 20 | 19 | 212 | 0 | 251 | 889 | 0 |
| 7:15 | 20 | 167 | 69 | 0 | 256 | 23 | 64 | 27 | 0 | 114 | 259 | 75 | 12 | 0 | 346 | 27 | 24 | 260 | 0 | 311 | 1027 | 0 |
| 7:30 | 14 | 177 | 57 | 0 | 248 | 21 | 64 | 18 | 0 | 103 | 299 | 85 | 14 | 0 | 398 | 24 | 34 | 306 | 0 | 364 | 1113 | 0 |
| 7:45 | 23 | 121 | 64 | 0 | 208 | 13 | 64 | 24 | 0 | 101 | 326 | 101 | 7 | 0 | 434 | 49 | 32 | 246 | 0 | 327 | 1070 | 0 |
| Total | 73 | 600 | 232 | 0 | 905 | 79 | 261 | 79 | 0 | 419 | 1141 | 339 | 42 | 0 | 1522 | 120 | 109 | 1024 | 0 | 1253 | 4099 | 0 |
| 8:00 | 23 | 147 | 69 | 0 | 239 | 17 | 59 | 27 | 0 | 103 | 288 | 80 | 9 | 0 | 377 | 36 | 35 | 210 | 0 | 281 | 1000 | 0 |
| 8:15 | 23 | 135 | 68 | 0 | 226 | 20 | 65 | 16 | 0 | 101 | 273 | 98 | 12 | 0 | 383 | 35 | 53 | 194 | 0 | 282 | 992 | 0 |
| 8:30 | 26 | 112 | 61 | 0 | 199 | 23 | 56 | 20 | 0 | 99 | 279 | 74 | 4 | 0 | 357 | 31 | 50 | 219 | 0 | 300 | 955 | 0 |
| 8:45 | 24 | 94 | 58 | 0 | 176 | 21 | 59 | 22 | 0 | 102 | 206 | 85 | 11 | 0 | 302 | 41 | 49 | 206 | 0 | 296 | 876 | 0 |
| Total | 96 | 488 | 256 | 0 | 840 | 81 | 239 | 85 | 0 | 405 | 1046 | 337 | 36 | 0 | 1419 | 143 | 187 | 829 | 0 | 1159 | 3823 | 0 |


| 16:00 | 28 | 109 | 57 | 0 | 194 | 15 | 45 | 23 | 0 | 83 | 269 | 165 | 17 | 0 | 451 | 52 | 87 | 220 | 0 | 359 | 1087 | 0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 16:15 | 31 | 100 | 43 | 0 | 174 | 23 | 61 | 25 | 0 | 109 | 290 | 155 | 18 | 0 | 463 | 51 | 70 | 259 | 0 | 380 | 1126 | 0 |
| 16:30 | 30 | 115 | 57 | 0 | 202 | 15 | 63 | 24 | 0 | 102 | 303 | 182 | 21 | 0 | 506 | 45 | 59 | 284 | 0 | 388 | 1198 | 0 |
| 16:45 | 34 | 94 | 45 | 0 | 173 | 19 | 57 | 27 | 0 | 103 | 270 | 152 | 19 | 0 | 441 | 58 | 72 | 259 | 0 | 389 | 1106 | 0 |
| Total | 123 | 418 | 202 | 0 | 743 | 72 | 226 | 99 | 0 | 397 | 1132 | 654 | 75 | 0 | 1861 | 206 | 288 | 1022 | 0 | 1516 | 4517 | 0 |
| 17:00 | 26 | 119 | 42 | 0 | 187 | 15 | 61 | 24 | 0 | 100 | 292 | 170 | 18 | 0 | 480 | 60 | 64 | 281 | 0 | 405 | 1172 | 0 |
| 17:15 | 21 | 112 | 57 | 0 | 190 | 8 | 54 | 23 | 0 | 85 | 311 | 185 | 22 | 0 | 518 | 48 | 74 | 284 | 0 | 406 | 1199 | 0 |
| 17:30 | 32 | 129 | 53 | 0 | 214 | 21 | 51 | 23 | 0 | 95 | 269 | 144 | 22 | 0 | 435 | 64 | 68 | 264 | 0 | 396 | 1140 | 0 |
| 17:45 | 28 | 88 | 44 | 0 | 160 | 20 | 63 | 18 | 0 | 101 | 320 | 163 | 18 | 0 | 501 | 56 | 68 | 249 | 0 | 373 | 1135 | 0 |
| Total | 107 | 448 | 196 | 0 | 751 | 64 | 229 | 88 | 0 | 381 | 1192 | 662 | 80 | 0 | 1934 | 228 | 274 | 1078 | 0 | 1580 | 4646 | 0 |
| Grand Total | 399 | 1954 | 886 | 0 | 3239 | 296 | 955 | 351 | 0 | 1602 | 4511 | 1992 | 233 | 0 | 6736 | 697 | 858 | 3953 | 0 | 5508 | 17085 | 0 |
| Apprch \% | 12.3\% | 60.3\% | 27.4\% | 0.0\% |  | 18.5\% | 59.6\% | 21.9\% | 0.0\% |  | 67.0\% | 29.6\% | 3.5\% | 0.0\% |  | 12.7\% | 15.6\% | 71.8\% | 0.0\% |  |  |  |
| Total \% | 2.3\% | 11.4\% | 5.2\% | 0.0\% | 19.0\% | 1.7\% | 5.6\% | 2.1\% | 0.0\% | 9.4\% | 26.4\% | 11.7\% | 1.4\% | 0.0\% | 39.4\% | 4.1\% | 5.0\% | 23.1\% | 0.0\% | 32.2\% | 100.0\% |  |


| $\begin{array}{\|c\|} \hline \text { AM PEAK } \\ \text { HOUR } \\ \hline \end{array}$ | Auburn-Folsom Rd Southbound |  |  |  |  | Douglas Blvd Westbound |  |  |  |  | Auburn-Folsom Rd Northbound |  |  |  |  | Douglas Blvd Eastbound |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| START TIME | LEFT | THRU | RIGHT | UTURNS | APP.TOTAL | LEFT | THRU | RIGHT | UTURNS | APP.TOTAL | LEFT | THRU | RIGHT | UTURNS | APP.TOTAL | LEFT | THRU | RIGHT | UTURNS | APP.TOTAL | Total |
| Peak Hour Analysis From 07:15 to 08:15 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Peak Hour For Entire Intersection Begins at 07:15 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7:15 | 20 | 167 | 69 | 0 | 256 | 23 | 64 | 27 | 0 | 114 | 259 | 75 | 12 | 0 | 346 | 27 | 24 | 260 | 0 | 311 | 1027 |
| 7:30 | 14 | 177 | 57 | 0 | 248 | 21 | 64 | 18 | 0 | 103 | 299 | 85 | 14 | 0 | 398 | 24 | 34 | 306 | 0 | 364 | 1113 |
| 7:45 | 23 | 121 | 64 | 0 | 208 | 13 | 64 | 24 | 0 | 101 | 326 | 101 | 7 | 0 | 434 | 49 | 32 | 246 | 0 | 327 | 1070 |
| 8:00 | 23 | 147 | 69 | 0 | 239 | 17 | 59 | 27 | 0 | 103 | 288 | 80 | 9 | 0 | 377 | 36 | 35 | 210 | 0 | 281 | 1000 |
| Total Volume | 80 | 612 | 259 | 0 | 951 | 74 | 251 | 96 | 0 | 421 | 1172 | 341 | 42 | 0 | 1555 | 136 | 125 | 1022 | 0 | 1283 | 4210 |
| \% App Total | 8.4\% | 64.4\% | 27.2\% | 0.0\% |  | 17.6\% | 59.6\% | 22.8\% | 0.0\% |  | 75.4\% | 21.9\% | 2.7\% | 0.0\% |  | 10.6\% | 9.7\% | 79.7\% | 0.0\% |  |  |
| PHF\| | . 870 | . 864 | . 938 | . 000 | . 929 | . 804 | . 980 | . 889 | . 000 | . 923 | . 899 | . 844 | . 750 | . 000 | . 896 | . 694 | . 893 | . 835 | . 000 | . 881 | . 946 |
| $\begin{array}{\|c\|} \hline \text { PM PEAK } \\ \text { HOUR } \\ \hline \end{array}$ | Auburn-Folsom Rd Southbound |  |  |  |  | Douglas Blvd Westbound |  |  |  |  | Auburn-Folsom Rd Northbound |  |  |  |  | Douglas Blvd Eastbound |  |  |  |  |  |
| START TIME | LEFT | THRU | RIGHT | UTURNS | APP.TOTAL | LEFT | THRU | RIGHT | UTURNS | APP.TOTAL | LEFT | THRU | RIGHT | UTURNS | APP.TOTAL | LEFT | THRU | RIGHT | UTURNS | APP.TOTAL | Total |
| Peak Hour Analysis From 16:30 to 17:30 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Peak Hour For Entire Intersection Begins at 16:30 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 16:30 | 30 | 115 | 57 | 0 | 202 | 15 | 63 | 24 | 0 | 102 | 303 | 182 | 21 | 0 | 506 | 45 | 59 | 284 | 0 | 388 | 1198 |
| 16:45 | 34 | 94 | 45 | 0 | 173 | 19 | 57 | 27 | 0 | 103 | 270 | 152 | 19 | 0 | 441 | 58 | 72 | 259 | 0 | 389 | 1106 |
| 17:00 | 26 | 119 | 42 | 0 | 187 | 15 | 61 | 24 | 0 | 100 | 292 | 170 | 18 | 0 | 480 | 60 | 64 | 281 | 0 | 405 | 1172 |
| 17:15 | 21 | 112 | 57 | 0 | 190 | 8 | 54 | 23 | 0 | 85 | 311 | 185 | 22 | 0 | 518 | 48 | 74 | 284 | 0 | 406 | 1199 |
| Total Volume | 111 | 440 | 201 | 0 | 752 | 57 | 235 | 98 | 0 | 390 | 1176 | 689 | 80 | 0 | 1945 | 211 | 269 | 1108 | 0 | 1588 | 4675 |
| \% App Total | 14.8\% | 58.5\% | 26.7\% | 0.0\% |  | 14.6\% | 60.3\% | 25.1\% | 0.0\% |  | 60.5\% | 35.4\% | 4.1\% | 0.0\% |  | 13.3\% | 16.9\% | 69.8\% | 0.0\% |  |  |
| PHF\| | 816 | . 924 | . 882 | . 000 | . 931 | . 750 | . 933 | . 907 | . 000 | . 947 | . 945 | . 931 | . 909 | . 000 | . 939 | . 879 | . 909 | . 975 | . 000 | . 978 | . 975 |

Auburn-Folsom Rd \& Douglas Blvd


Total Ins \& Outs


Total Volume Per Leg


## National Data and Surveying Services

## City of Granite Bay <br> All Vehicles \& Uturns On Unshifted

Bikes \& Peds On Bank 1
Unshifted Count = All Vehicles \& Uturns

|  | Auburn Folsom Rd Southbound |  |  |  |  | Eureka Dr Westbound |  |  |  |  | Auburn Folsom Rd Northbound |  |  |  |  | Eureka Dr Eastbound |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| START TIME | LEFT | THRU | RIGHT | UTURNS | APP.TOTAL | LEFT | THRU | RIGHT | UTURNS | APP.TOTAL | LEFT | THRU | RIGHT | UTURNS | APP.TOTAL | LEFT | THRU | RIGHT | UTURNS | APP.TOTAL | Total | Uturns Total |
| 7:00 | 0 | 357 | 41 | 0 | 398 | 1 | 1 | 0 | 0 | 2 | 26 | 308 | 0 | 0 | 334 | 13 | 0 | 24 | 0 | 37 | 771 | 0 |
| 7:15 | 0 | 408 | 53 | 0 | 461 | 0 | 1 | 0 | 0 | 1 | 29 | 370 | 0 | 0 | 399 | 29 | 1 | 35 | 0 | 65 | 926 | 0 |
| 7:30 | 2 | 449 | 52 | 0 | 503 | 0 | 0 | 1 | 0 | 1 | 55 | 371 | 0 | 0 | 426 | 62 | 1 | 41 | 0 | 104 | 1034 | 0 |
| 7:45 | 0 | 390 | 47 | 0 | 437 | 0 | 0 | 1 | 0 | 1 | 52 | 356 | 0 | 0 | 408 | 17 | 0 | 31 | 0 | 48 | 894 | 0 |
| Total | 2 | 1604 | 193 | 0 | 1799 | 1 | 2 | 2 | 0 | 5 | 162 | 1405 | 0 | 0 | 1567 | 121 | 2 | 131 | 0 | 254 | 3625 | 0 |
| 8:00 | 0 | 355 | 21 | 0 | 376 | 0 | 0 | 0 | 0 | 0 | 44 | 342 | 0 | 0 | 386 | 13 | 0 | 21 | 0 | 34 | 796 | 0 |
| 8:15 | 0 | 344 | 15 | 3 | 362 | 2 | 0 | 1 | 0 | 3 | 29 | 334 | 0 | 0 | 363 | 15 | 1 | 30 | 0 | 46 | 774 | 3 |
| 8:30 | 1 | 316 | 27 | 2 | 346 | 0 | 2 | 0 | 0 | 2 | 26 | 346 | 0 | 1 | 373 | 13 | 1 | 30 | 0 | 44 | 765 | 3 |
| 8:45 | 1 | 309 | 21 | 2 | 333 | 0 | 1 | 0 | 0 | 1 | 29 | 299 | 0 | 1 | 329 | 22 | 0 | 19 | 0 | 41 | 704 | 3 |
| Total | 2 | 1324 | 84 | 7 | 1417 | 2 | 3 | 1 | 0 | 6 | 128 | 1321 | 0 | 2 | 1451 | 63 | 2 | 100 | 0 | 165 | 3039 | 9 |


| 16:00 | 2 | 323 | 20 | 0 | 345 | 0 | 0 | 0 | 0 | 0 | 33 | 460 | 0 | 0 | 493 | 24 | 0 | 55 | 0 | 79 | 917 | 0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 16:15 | 0 | 398 | 25 | 2 | 425 | 0 | 0 | 0 | 0 | 0 | 32 | 448 | 0 | 2 | 482 | 13 | 0 | 46 | 0 | 59 | 966 | 4 |
| 16:30 | 0 | 376 | 19 | 5 | 400 | 0 | 0 | 0 | 0 | 0 | 36 | 464 | 0 | 0 | 500 | 10 | 0 | 51 | 0 | 61 | 961 | 5 |
| 16:45 | 1 | 365 | 16 | 4 | 386 | 0 | 0 | 0 | 0 | 0 | 24 | 457 | 0 | 1 | 482 | 21 | 0 | 55 | 0 | 76 | 944 | 5 |
| Total | 3 | 1462 | 80 | 11 | 1556 | 0 | 0 | 0 | 0 | 0 | 125 | 1829 | 0 | 3 | 1957 | 68 | 0 | 207 | 0 | 275 | 3788 | 14 |
| 17:00 | 0 | 381 | 24 | 1 | 406 | 0 | 0 | 0 | 0 | 0 | 25 | 468 | 0 | 1 | 494 | 15 | 0 | 41 | 0 | 56 | 956 | 2 |
| 17:15 | 1 | 408 | 16 | 3 | 428 | 0 | 0 | 1 | 0 | 1 | 32 | 471 | 0 | 0 | 503 | 19 | 1 | 74 | 0 | 94 | 1026 | 3 |
| 17:30 | 0 | 407 | 25 | 0 | 432 | 0 | 0 | 1 | 0 | 1 | 31 | 455 | 1 | 0 | 487 | 11 | 0 | 72 | 0 | 83 | 1003 | 0 |
| 17:45 | 0 | 329 | 27 | 1 | 357 | 0 | 0 | 0 | 0 | 0 | 26 | 466 | 0 | 0 | 492 | 12 | 0 | 43 | 0 | 55 | 904 | 1 |
| Total | 1 | 1525 | 92 | 5 | 1623 | 0 | 0 | 2 | 0 | 2 | 114 | 1860 | 1 | 1 | 1976 | 57 | 1 | 230 | 0 | 288 | 3889 | 6 |
| Grand Total | 8 | 5915 | 449 | 23 | 6395 | 3 | 5 | 5 | 0 | 13 | 529 | 6415 | 1 | 6 | 6951 | 309 | 5 | 668 | 0 | 982 | 14341 | 29 |
| Apprch \% | 0.1\% | 92.5\% | 7.0\% | 0.4\% |  | 23.1\% | 38.5\% | 38.5\% | 0.0\% |  | 7.6\% | 92.3\% | 0.0\% | 0.1\% |  | 31.5\% | 0.5\% | 68.0\% | 0.0\% |  |  |  |
| Total \% | 0.1\% | 41.2\% | 3.1\% | 0.2\% | 44.6\% | 0.0\% | 0.0\% | 0.0\% | 0.0\% | 0.1\% | 3.7\% | 44.7\% | 0.0\% | 0.0\% | 48.5\% | 2.2\% | 0.0\% | 4.7\% | 0.0\% | 6.8\% | 100.0\% |  |


| AM PEAK HOUR | Auburn Folsom Rd Southbound |  |  |  |  | Eureka Dr Westbound |  |  |  |  | Auburn Folsom Rd Northbound |  |  |  |  | Eureka Dr Eastbound |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| START TIME | LEFT | THRU | RIGHT | UTURNS | APP.TOTAL | LEFT | THRU | RIGHT | UTURNS | APP.TOTAL | LEFT | THRU | RIGHT | UTURNS | APP.TOTAL | LEFT | THRU | RIGHT | UTURNS | APP.TOTAL | Total |
| Peak Hour Analysis From 07:15 to 08:15 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Peak Hour For Entire Intersection Begins at 07:15 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7:15 | 0 | 408 | 53 | 0 | 461 | 0 | 1 | 0 | 0 | 1 | 29 | 370 | 0 | 0 | 399 | 29 | 1 | 35 | 0 | 65 | 926 |
| 7:30 | 2 | 449 | 52 | 0 | 503 | 0 | 0 | 1 | 0 | 1 | 55 | 371 | 0 | 0 | 426 | 62 | 1 | 41 | 0 | 104 | 1034 |
| 7:45 | 0 | 390 | 47 | 0 | 437 | 0 | 0 | 1 | 0 | 1 | 52 | 356 | 0 | 0 | 408 | 17 | 0 | 31 | 0 | 48 | 894 |
| 8:00 | 0 | 355 | 21 | 0 | 376 | 0 | 0 | 0 | 0 | 0 | 44 | 342 | 0 | 0 | 386 | 13 | 0 | 21 | 0 | 34 | 796 |
| Total Volume | 2 | 1602 | 173 | 0 | 1777 | 0 | 1 | 2 | 0 | 3 | 180 | 1439 | 0 | 0 | 1619 | 121 | 2 | 128 | 0 | 251 | 3650 |
| \% App Total | 0.1\% | 90.2\% | 9.7\% | 0.0\% |  | 0.0\% | 33.3\% | 66.7\% | 0.0\% |  | 11.1\% | 88.9\% | 0.0\% | 0.0\% |  | 48.2\% | 0.8\% | 51.0\% | 0.0\% |  |  |
| PHF\| | . 250 | . 892 | . 816 | . 000 | . 883 | . 000 | . 250 | . 500 | . 000 | . 750 | . 818 | . 970 | . 000 | . 000 | . 950 | . 488 | . 500 | . 780 | . 000 | . 603 | 882 |
| PM PEAK HOUR | Auburn Folsom Rd Southbound |  |  |  |  | Eureka Dr Westbound |  |  |  |  | Auburn Folsom Rd Northbound |  |  |  |  | Eureka Dr Eastbound |  |  |  |  |  |
| START TIME | LEFT | THRU | RIGHT | UTURNS | APP.TOTAL | LEFT | THRU | RIGHT | UTURNS | APP.TOTAL | LEFT | THRU | RIGHT | UTURNS | APP.TOTAL | LEFT | THRU | RIGHT | UTURNS | APP.TOTAL | Total |
| Peak Hour Analysis From 16:45 to 17:45 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Peak Hour For Entire Intersection Begins at 16:45 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 16:45 | 1 | 365 | 16 | 4 | 386 | 0 | 0 | 0 | 0 | 0 | 24 | 457 | 0 | 1 | 482 | 21 | 0 | 55 | 0 | 76 | 944 |
| 17:00 | 0 | 381 | 24 | 1 | 406 | 0 | 0 | 0 | 0 | 0 | 25 | 468 | 0 | 1 | 494 | 15 | 0 | 41 | 0 | 56 | 956 |
| 17:15 | 1 | 408 | 16 | 3 | 428 | 0 | 0 | 1 | 0 | 1 | 32 | 471 | 0 | 0 | 503 | 19 | 1 | 74 | 0 | 94 | 1026 |
| 17:30 | 0 | 407 | 25 | 0 | 432 | 0 | 0 | 1 | 0 | 1 | 31 | 455 | I | 0 | 487 | 11 | 0 | 72 | 0 | 83 | 1003 |
| Total Volume | 2 | 1561 | 81 | 8 | 1652 | 0 | 0 | 2 | 0 | 2 | 112 | 1851 | 1 | 2 | 1966 | 66 | , | 242 | 0 | 309 | 3929 |
| \% App Total | 0.1\% | 94.5\% | 4.9\% | 0.5\% |  | 0.0\% | 0.0\% | 100.0\% | 0.0\% |  | 5.7\% | 94.2\% | 0.1\% | 0.1\% |  | 21.4\% | 0.3\% | 78.3\% | 0.0\% |  |  |
| PHF\| | . 500 | . 956 | . 810 | . 500 | . 956 | . 000 | . 000 | . 500 | . 000 | . 500 | . 875 | . 982 | . 250 | . 500 | . 977 | . 786 | . 250 | . 818 | . 000 | . 822 | . 957 |

Auburn Folsom Rd \& Eureka Dr


Total Ins \& Outs


Total Volume Per Leg


VOLUME
Douglas Blvd Bet. Sierra College Blvd \& Cavitt Stallman Rd

Day: Thursday
Date: 5/18/2017

City: Granite Bay
Project \#: CA17_7442_001



VOLUME
Douglas Blvd Bet. Cavitt Stallman Rd \& Quail Oaks Dr

Day: Thursday
Date: 5/18/2017

City: Granite Bay
Project \#: CA17_7442_002



VOLUME
Douglas Blvd Bet. Seeno Ave \& Berg St

Day: Thursday
Date: 5/18/2017

City: Granite Bay
Project \#: CA17_7442_004


| Prepared by NDS/ATD |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Project \#: CA17_7442_004 |  |  |  |  |  |  | City: Granite Bay |  |  |  |  |  |  |  |  |  |  |
| Location: Douglas Blvd Bet. Seeno Ave \& Berg St |  |  |  |  |  |  |  | Date: 5/18/2017 |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

VOLUME
Douglas Blvd Bet. Berg St \& Barton Rd

Day: Thursday
Date: 5/18/2017

City: Granite Bay
Project \#: CA17_7442_005



VOLUME
Douglas Blvd Bet. Barton Rd \& Joe Rodgers Rd

Day: Thursday
Date: 5/18/2017

City: Granite Bay
Project \#: CA17_7442_006



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | ＊＊ | 444 | 「 | ＊＊ | 444 | F | ＊＊ | 444 | 「 | ＊＊ | 衡 |  |
| Traffic Volume（veh／h） | 184 | 1156 | 172 | 226 | 1685 | 113 | 438 | 811 | 125 | 208 | 581 | 171 |
| Future Volume（veh／h） | 184 | 1156 | 172 | 226 | 1685 | 113 | 438 | 811 | 125 | 208 | 581 | 171 |
| Initial Q（Qb），veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 0.99 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 0.99 |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow，veh／h／ln | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 |
| Adj Flow Rate，veh／h | 200 | 1257 | 60 | 246 | 1832 | 0 | 476 | 882 | 0 | 226 | 632 | 138 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh，\％ | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap，veh／h | 259 | 1659 | 508 | 533 | 2149 |  | 531 | 1298 |  | 288 | 773 | 166 |
| Arrive On Green | 0.07 | 0.32 | 0.32 | 0.15 | 0.42 | 0.00 | 0.20 | 0.34 | 0.00 | 0.08 | 0.18 | 0.18 |
| Sat Flow，veh／h | 3456 | 5106 | 1564 | 3456 | 5106 | 1585 | 3456 | 5106 | 1585 | 3456 | 4202 | 903 |
| Grp Volume（v），veh／h | 200 | 1257 | 60 | 246 | 1832 | 0 | 476 | 882 | 0 | 226 | 510 | 260 |
| Grp Sat Flow（s），veh／h／ln | 1728 | 1702 | 1564 | 1728 | 1702 | 1585 | 1728 | 1702 | 1585 | 1728 | 1702 | 1701 |
| Q Serve（g＿s），s | 6.8 | 26.5 | 2.1 | 7.8 | 38.9 | 0.0 | 16.1 | 17.8 | 0.0 | 7.7 | 17.3 | 17.7 |
| Cycle Q Clear（g＿c），s | 6.8 | 26.5 | 2.1 | 7.8 | 38.9 | 0.0 | 16.1 | 17.8 | 0.0 | 7.7 | 17.3 | 17.7 |
| Prop In Lane | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 0.53 |
| Lane Grp Cap（c），veh／h | 259 | 1659 | 508 | 533 | 2149 |  | 531 | 1298 |  | 288 | 626 | 313 |
| V／C Ratio（X） | 0.77 | 0.76 | 0.12 | 0.46 | 0.85 |  | 0.90 | 0.68 |  | 0.79 | 0.81 | 0.83 |
| Avail Cap（c＿a），veh／h | 461 | 1659 | 508 | 533 | 2149 |  | 605 | 1298 |  | 605 | 681 | 340 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.33 | 1.33 | 1.33 | 1.00 | 1.00 | 1.00 |
| Upstream Filter（l） | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay（d），s／veh | 54.5 | 36.3 | 12.0 | 46.2 | 31.4 | 0.0 | 46.8 | 35.5 | 0.0 | 53.9 | 47.0 | 47.2 |
| Incr Delay（d2），s／veh | 1.9 | 3.3 | 0.5 | 0.2 | 3.6 | 0.0 | 13.8 | 1.6 | 0.0 | 1.8 | 7.6 | 15.9 |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ（50\％），veh／In | 3.0 | 11.0 | 1.2 | 3.3 | 15.7 | 0.0 | 7.4 | 6.8 | 0.0 | 3.3 | 7.8 | 8.6 |
| Unsig．Movement Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay（d），s／veh | 56.3 | 39.6 | 12.4 | 46.4 | 35.0 | 0.0 | 60.6 | 37.1 | 0.0 | 55.8 | 54.6 | 63.1 |
| LnGrp LOS | E | D | B | D | C |  | E | D |  | E | D | E |
| Approach Vol，veh／h |  | 1517 |  |  | 2078 | A |  | 1358 | A |  | 996 |  |
| Approach Delay，s／veh |  | 40.7 |  |  | 36.3 |  |  | 45.4 |  |  | 57.1 |  |
| Approach LOS |  | D |  |  | D |  |  | D |  |  | E |  |


| Timer－Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Phs Duration（G＋Y＋Rc），s | 24.5 | 45.0 | 22.4 | 28.1 | 13.0 | 56.5 | 14.0 | 36.5 |
| Change Period（Y＋Rc），s | 6.0 | 6.0 | 4.0 | 6.0 | 4.0 | 6.0 | 4.0 | 6.0 |
| Max Green Setting（Gmax），s | 14.0 | 39.0 | 21.0 | 24.0 | 16.0 | 39.0 | 21.0 | 24.0 |
| Max Q Clear Time（g＿c＋I1），s | 9.8 | 28.5 | 18.1 | 19.7 | 8.8 | 40.9 | 9.7 | 19.8 |
| Green Ext Time（p＿c），s | 0.2 | 7.2 | 0.3 | 2.3 | 0.2 | 0.0 | 0.3 | 2.4 |

## Intersection Summary

| HCM 6th Ctrl Delay | 43.0 |
| :--- | ---: |
| HCM 6th LOS | D |

## Notes

User approved pedestrian interval to be less than phase max green．
Unsignalized Delay for［NBR，WBR］is excluded from calculations of the approach delay and intersection delay．

| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \＃ | 44 | F | \＃ | 中 ${ }^{\text {a }}$ |  |  | $\uparrow$ | 「 |  | $\uparrow$ | 「 |
| Traffic Vol，veh／h | 39 | 1361 | 34 | 41 | 1839 | 7 | 5 | 0 | 57 | 0 | 1 | 99 |
| Future Vol，veh／h | 39 | 1361 | 34 | 41 | 1839 | 7 | 5 | 0 | 57 | 0 | 1 | 99 |
| Conflicting Peds，\＃／hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | － | － | None | － | － | None | － | － | None | － | － | None |
| Storage Length | 150 | － | 100 | 175 | － | － | － | － | 125 | － | － | 25 |
| Veh in Median Storage，\＃ | － | 0 | － | － | 0 | － | － | 0 | － | － | 0 | － |
| Grade，\％ | － | 0 | － | － | 0 | － | － | 0 | － | － | 0 | － |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles，\％ | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 42 | 1479 | 37 | 45 | 1999 | 8 | 5 | 0 | 62 | 0 | 1 | 108 |


| Major／Minor | Major1 |  |  |  | Major2 |  |  | Minor1 |  |  | Minor2 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 2007 | 0 | 0 |  | 1516 | 0 | 0 | 2653 | 3660 | 740 | 2917 | 3693 | 1004 |
| Stage 1 |  | － | － |  | － | － |  | 1563 | 1563 | － | 2093 | 2093 | － |
| Stage 2 |  | － | － |  | － | － | － | 1090 | 2097 | － | 824 | 1600 |  |
| Critical Hdwy | 4.14 | － | － |  | 4.14 | － | － | 7.54 | 6.54 | 6.94 | 7.54 | 6.54 | 6.94 |
| Critical Hdwy Stg 1 |  | － | － |  |  | － |  | 6.54 | 5.54 | － | 6.54 | 5.54 | － |
| Critical Hdwy Stg 2 | － | － | － |  | － | － |  | 6.54 | 5.54 | － | 6.54 | 5.54 | － |
| Follow－up Hdwy | 2.22 | － | － |  | 2.22 | － | － | 3.52 | 4.02 | 3.32 | 3.52 | 4.02 | 3.32 |
| Pot Cap－1 Maneuver | 281 | － | － |  | 437 | － | － | 11 | 5 | 359 | 7 | 5 | 240 |
| Stage 1 |  | － | － |  |  |  |  | 117 | 171 | － | 54 | 92 |  |
| Stage 2 | － | － | － |  | － | － |  | 230 | 92 | － | 333 | 164 | － |
| Platoon blocked，\％ |  | － | － |  |  | － | － |  |  |  |  |  |  |
| Mov Cap－1 Maneuver | 281 | － | － |  | 437 | － |  | $\sim 4$ | 4 | 359 | 5 | 4 | 240 |
| Mov Cap－2 Maneuver | － | － | － |  | － | － |  | $\sim 4$ | 4 | － | 5 | 4 | － |
| Stage 1 | － | － |  |  | － |  |  | 100 | 146 | － | 46 | 83 |  |
| Stage 2 | － | － |  |  | － |  |  | 112 | 83 | － | 234 | 140 | － |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Approach | EB |  |  |  | WB |  |  | NB |  |  | SB |  |  |
| HCM Control Delay，s | 0.5 |  |  |  | 0.3 |  |  | 155.4 |  |  | 42.4 |  |  |
| HCM LOS |  |  |  |  |  |  |  | F |  |  | E |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Minor Lane／Major Mvmt | NBLn1 | NBLn2 | EBL | EBT | EBR | WBL | WBT | WBR | SBLn1 | SBLn2 |  |  |  |
| Capacity（veh／h） | 4 | 359 | 281 | － | － | 437 | － | － | 4 | 240 |  |  |  |
| HCM Lane V／C Ratio | 1.359 | 0.173 | 0.151 | － | － | 0.102 | － | － | 0.272 | 0.448 |  |  |  |
| HCM Control Delay（s） | \＄ 1731.9 | 17.1 | 20.1 | － | － | 14.2 | － |  | 111.1 | 31.6 |  |  |  |
| HCM Lane LOS | F | C | C |  |  | B | － | － | F | D |  |  |  |
| HCM 95th \％tile Q（veh） | 1.5 | 0.6 | 0.5 |  | － | 0.3 | － | － | 0.5 | 2.2 |  |  |  |
| Notes |  |  |  |  |  |  |  |  |  |  |  |  |  |
| $\sim$ Volume exceeds cap | \＄：Delay exceeds 300s |  |  |  | ＋：Computation Not Defined |  |  |  | ＊：All major volume in platoon |  |  |  |  |


|  | $y$ | $\rightarrow$ |  | 5 | $\dagger$ |  |  | 4 | $\uparrow$ | $p$ | $t$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBU | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT |
| Lane Configurations | \# | 个t |  |  | * | 性 |  |  |  |  |  | $\uparrow$ |
| Traffic Volume (veh/h) | 58 | 1361 | 0 | 2 | - | 1840 | 82 | 0 | 0 | 0 | 50 | 0 |
| Future Volume (veh/h) | 58 | 1361 | 0 | 2 | 0 | 1840 | 82 | 0 | 0 | 0 | 50 | 0 |
| Initial Q (Qb), veh | 0 | 0 | 0 |  | 0 | 0 | 0 |  |  |  | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 |  | 1.00 |  | 1.00 |  | 0.98 |  |  |  | 1.00 |  |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 |  |  |  | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  |  | No |  |  |  |  |  | No |
| Adj Sat Flow, veh/h/ln | 1870 | 1870 | 1870 |  | 1870 | 1870 | 1870 |  |  |  | 1870 | 1870 |
| Adj Flow Rate, veh/h | 63 | 1479 | 0 |  | 0 | 2000 | 87 |  |  |  | 54 | 0 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 |  | 0.92 | 0.92 | 0.92 |  |  |  | 0.92 | 0.92 |
| Percent Heavy Veh, \% | 2 | 2 | 2 |  | 2 | 2 | 2 |  |  |  | 2 | 2 |
| Cap, veh/h | 80 | 2906 | 0 |  | 3 | 2529 | 109 |  |  |  | 80 | 0 |
| Arrive On Green | 0.05 | 0.82 | 0.00 |  | 0.00 | 0.73 | 0.73 |  |  |  | 0.04 | 0.00 |
| Sat Flow, veh/h | 1781 | 3647 | 0 |  | 1781 | 3467 | 150 |  |  |  | 1781 | 0 |
| Grp Volume(v), veh/h | 63 | 1479 | 0 |  | 0 | 1017 | 1070 |  |  |  | 54 | 0 |
| Grp Sat Flow(s),veh/h/ln | 1781 | 1777 | 0 |  | 1781 | 1777 | 1840 |  |  |  | 1781 | 0 |
| Q Serve(g_s), s | 2.4 | 9.0 | 0.0 |  | 0.0 | 25.0 | 26.0 |  |  |  | 2.1 | 0.0 |
| Cycle Q Clear (g_c), s | 2.4 | 9.0 | 0.0 |  | 0.0 | 25.0 | 26.0 |  |  |  | 2.1 | 0.0 |
| Prop In Lane | 1.00 |  | 0.00 |  | 1.00 |  | 0.08 |  |  |  | 1.00 |  |
| Lane Grp Cap(c), veh/h | 80 | 2906 | 0 |  | 3 | 1296 | 1342 |  |  |  | 80 | 0 |
| V/C Ratio(X) | 0.79 | 0.51 | 0.00 |  | 0.00 | 0.78 | 0.80 |  |  |  | 0.68 | 0.00 |
| Avail Cap(c_a), veh/h | 592 | 3440 | 0 |  | 335 | 1720 | 1781 |  |  |  | 875 | 0 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 |  |  |  | 1.00 | 1.00 |
| Upstream Filter(l) | 1.00 | 1.00 | 0.00 |  | 0.00 | 1.00 | 1.00 |  |  |  | 1.00 | 0.00 |
| Uniform Delay (d), s/veh | 32.7 | 2.0 | 0.0 |  | 0.0 | 5.9 | 6.1 |  |  |  | 32.6 | 0.0 |
| Incr Delay (d2), s/veh | 6.2 | 0.1 | 0.0 |  | 0.0 | 1.8 | 1.9 |  |  |  | 3.7 | 0.0 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 |  |  |  | 0.0 | 0.0 |
| \%ile BackOfQ(50\%),veh/ln | 1.1 | 0.1 | 0.0 |  | 0.0 | 3.5 | 3.8 |  |  |  | 1.0 | 0.0 |
| Unsig. Movement Delay, s/veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay (d),s/veh | 38.9 | 2.1 | 0.0 |  | 0.0 | 7.7 | 8.0 |  |  |  | 36.2 | 0.0 |
| LnGrp LOS | D | A | A |  | A | A | A |  |  |  | D | A |
| Approach Vol, veh/h |  | 1542 |  |  |  | 2087 |  |  |  |  |  | 68 |
| Approach Delay, s/veh |  | 3.6 |  |  |  | 7.9 |  |  |  |  |  | 35.4 |
| Approach LOS |  | A |  |  |  | A |  |  |  |  |  | D |
| Timer - Assigned Phs | 1 | 2 |  | 4 | 5 | 6 |  |  |  |  |  |  |
| Phs Duration ( $\mathrm{G}+\mathrm{Y}+\mathrm{Rc}$ ), s | 6.1 | 56.5 |  | 6.6 | 0.0 | 62.6 |  |  |  |  |  |  |
| Change Period ( $\mathrm{Y}+\mathrm{Rc}$ ), s | 3.0 | 6.0 |  | 3.5 | 3.0 | 6.0 |  |  |  |  |  |  |
| Max Green Setting (Gmax), s | 23.0 | 67.0 |  | 34.0 | 13.0 | 67.0 |  |  |  |  |  |  |
| Max Q Clear Time (g_c+1), s | 4.4 | 28.0 |  | 4.1 | 0.0 | 11.0 |  |  |  |  |  |  |
| Green Ext Time (p_c), s | 0.0 | 22.4 |  | 0.2 | 0.0 | 14.2 |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 6th Ctrl Delay |  |  | 6.6 |  |  |  |  |  |  |  |  |  |
| HCM 6th LOS |  |  | A |  |  |  |  |  |  |  |  |  |
| Notes |  |  |  |  |  |  |  |  |  |  |  |  |

User approved ignoring U-Turning movement.

|  | $\downarrow$ |
| :---: | :---: |
| Movement | SBR |
| Lanefonfigurations | 7 |
| Traffic Volume (veh/h) | 46 |
| Future Volume (veh/h) | 46 |
| Initial Q (Qb), veh | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 |
| Parking Bus, Adj | 1.00 |
| Work Zone On Approach |  |
| Adj Sat Flow, veh/h/ln | 1870 |
| Adj Flow Rate, veh/h | 14 |
| Peak Hour Factor | 0.92 |
| Percent Heavy Veh, \% | 2 |
| Cap, veh/h | 71 |
| Arrive On Green | 0.04 |
| Sat Flow, veh/h | 1585 |
| Grp Volume(v), veh/h | 14 |
| Grp Sat Flow(s), veh/h/ln | 1585 |
| Q Serve(g_s), s | 0.6 |
| Cycle Q Clear(g_c), s | 0.6 |
| Prop In Lane | 1.00 |
| Lane Grp Cap(c), veh/h | 71 |
| V/C Ratio(X) | 0.20 |
| Avail Cap(c_a), veh/h | 779 |
| HCM Platoon Ratio | 1.00 |
| Upstream Filter(I) | 1.00 |
| Uniform Delay (d), s/veh | 31.8 |
| Incr Delay (d2), s/veh | 0.5 |
| Initial Q Delay(d3),s/veh | 0.0 |
| \%ile BackOfQ(50\%),veh/ln | 0.0 |
| Unsig. Movement Delay, s/veh |  |
| LnGrp Delay(d),s/veh | 32.3 |
| LnGrp LOS | C |
| Approach Vol, veh/h |  |
| Approach Delay, s/veh |  |
| Approach LOS |  |
| Timer - Assigned Phs |  |


| Intersection |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 0.2 |  |  |  |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL |  |
| Lane Configurations | 性 |  | ${ }_{1}$ | 44 |  | 「 |
| Traffic Vol, veh/h | 1441 | 23 | 16 | 1882 | 0 | 24 |
| Future Vol, veh/h | 1441 | 23 | 16 | 1882 | 0 | 24 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | 200 | - | - | 0 |
| Veh in Median Storage, | \# 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 1566 | 25 | 17 | 2046 | 0 | 26 |


| Major/Minor | Major1 | Major2 |  |  |  |  |  | Minor1 |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | :---: | :---: | :---: |
| Conflicting Flow All | 0 | 0 | 1591 | 0 | - | 796 |  |  |  |
| $\quad$ Stage 1 | - | - | - | - | - | - |  |  |  |
| $\quad$ Stage 2 | - | - | - | - | - | - |  |  |  |
| Critical Hdwy | - | - | 4.14 | - | - | 6.94 |  |  |  |
| Critical Hdwy Stg 1 | - | - | - | - | - | - |  |  |  |
| Critical Hdwy Stg 2 | - | - | - | - | - | - |  |  |  |
| Follow-up Hdwy | - | - | 2.22 | - | - | 3.32 |  |  |  |
| Pot Cap-1 Maneuver | - | - | 408 | - | 0 | 330 |  |  |  |
| $\quad$ Stage 1 | - | - | - | - | 0 | - |  |  |  |
| $\quad$ Stage 2 | - | - | - | - | 0 | - |  |  |  |
| Platoon blocked, \% | - | - |  | - |  |  |  |  |  |
| Mov Cap-1 Maneuver | - | - | 408 | - | - | 330 |  |  |  |
| Mov Cap-2 Maneuver | - | - | - | - | - | - |  |  |  |
| Stage 1 | - | - | - | - | - | - |  |  |  |
| Stage 2 | - | - | - | - | - | - |  |  |  |


| Approach | EB | WB | NB |
| :--- | :---: | :---: | :---: |
| HCM Control Delay, s | 0 | 0.1 | 16.8 |
| HCM LOS |  | C |  |


| Minor Lane/Major Mvmt | NBLn1 | EBT | EBR | WBL | WBT |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 330 | - | - | 408 | - |
| HCM Lane V/C Ratio | 0.079 | - | -0.043 | - |  |
| HCM Control Delay (s) | 16.8 | - | - | 14.2 | - |
| HCM Lane LOS | C | - | - | B | - |
| HCM 95th \%tile Q(veh) | 0.3 | - | - | 0.1 | - |


| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay，s／veh | 0.8 |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \％ | 个t |  | \％ | 性 |  |  |  | 「 |  |  | F |
| Traffic Vol，veh／h | 38 | 1351 | 7 | 34 | 1834 | 9 | 0 | 0 | 2 | 0 | 0 | 64 |
| Future Vol，veh／h | 38 | 1351 | 7 | 34 | 1834 | 9 | 0 | 0 | 2 | 0 | 0 | 64 |
| Conflicting Peds，\＃／hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | － | － | None | － | － | None | － | － | None | － |  | None |
| Storage Length | 250 | － | － | 325 | － | － | － | － | 0 | － | － | 0 |
| Veh in Median Storage，\＃ | － | 0 | － | － | 0 | － | － | 0 | － | － | 0 | － |
| Grade，\％ | － | 0 | － | － | 0 | － | － | 0 | － | － | 0 | － |
| Peak Hour Factor | 96 | 96 | 96 | 96 | 96 | 96 | 96 | 96 | 96 | 96 | 96 | 96 |
| Heavy Vehicles，\％ | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| Mumt Flow | 40 | 1407 | 7 | 35 | 1910 | 9 | 0 | 0 | 2 | 0 | 0 | 67 |

 Stage 2

| Approach | EB | WB | NB | SB |
| :--- | :---: | :---: | :---: | :---: |
| HCM Control Delay，s | 0.5 | 0.2 | 14.5 | 23.7 |
| HCM LOS |  |  | B | C |


| Minor Lane／Major Mvmt | NBLn1 | EBL | EBT | EBR | WBL | WBT | WBR SBLn1 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Capacity（veh／h） | 380 | 308 | - | -483 | - | -259 |  |
| HCM Lane V／C Ratio | 0.005 | 0.129 | - | -0.073 | - | -0.257 |  |
| HCM Control Delay（s） | 14.5 | 18.4 | - | - | 13 | - | -23.7 |
| HCM Lane LOS | B | C | - | - | B | - | - |
| HCM 95th \％otlie Q（veh） | 0 | 0.4 | - | - | 0.2 | - | - |


| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | ＊ | 中 ${ }^{\text {a }}$ |  | ＊ | 44 | 「 | ${ }^{1}$ | $\uparrow$ | 「 |  | $\uparrow$ | 7 |
| Traffic Volume（veh／h） | 41 | 1187 | 130 | 134 | 1564 | 114 | 215 | 98 | 76 | 137 | 116 | 34 |
| Future Volume（veh／h） | 41 | 1187 | 130 | 134 | 1564 | 114 | 215 | 98 | 76 | 137 | 116 | 34 |
| Initial Q（Qb），veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 1.00 | 1.00 |  | 0.98 | 1.00 |  | 1.00 | 1.00 |  | 0.99 |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow，veh／h／ln | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 |
| Adj Flow Rate，veh／h | 44 | 1263 | 131 | 143 | 1664 | 76 | 166 | 191 | 0 | 146 | 123 | 7 |
| Peak Hour Factor | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 |
| Percent Heavy Veh，\％ | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| Cap，veh／h | 56 | 1367 | 141 | 175 | 1733 | 755 | 220 | 231 |  | 166 | 140 | 263 |
| Arrive On Green | 0.03 | 0.42 | 0.42 | 0.10 | 0.48 | 0.48 | 0.12 | 0.12 | 0.00 | 0.17 | 0.17 | 0.17 |
| Sat Flow，veh／h | 1795 | 3276 | 339 | 1795 | 3582 | 1562 | 1795 | 1885 | 1598 | 996 | 839 | 1576 |
| Grp Volume（v），veh／h | 44 | 688 | 706 | 143 | 1664 | 76 | 166 | 191 | 0 | 269 | 0 | 7 |
| Grp Sat Flow（s），veh／h／ln | 1795 | 1791 | 1824 | 1795 | 1791 | 1562 | 1795 | 1885 | 1598 | 1835 | 0 | 1576 |
| Q Serve（g＿s），s | 2.2 | 33.1 | 33.4 | 7.1 | 40.7 | 2.4 | 8.1 | 9.0 | 0.0 | 13.0 | 0.0 | 0.3 |
| Cycle Q Clear（g＿c），s | 2.2 | 33.1 | 33.4 | 7.1 | 40.7 | 2.4 | 8.1 | 9.0 | 0.0 | 13.0 | 0.0 | 0.3 |
| Prop In Lane | 1.00 |  | 0.19 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 0.54 |  | 1.00 |
| Lane Grp Cap（c），veh／h | 56 | 747 | 761 | 175 | 1733 | 755 | 220 | 231 |  | 306 | 0 | 263 |
| V／C Ratio（X） | 0.79 | 0.92 | 0.93 | 0.81 | 0.96 | 0.10 | 0.75 | 0.83 |  | 0.88 | 0.00 | 0.03 |
| Avail Cap（c＿a），veh／h | 296 | 788 | 802 | 395 | 1773 | 773 | 395 | 415 |  | 404 | 0 | 347 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter（l） | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 0.00 | 1.00 |
| Uniform Delay（d），s／veh | 43.7 | 25.1 | 25.2 | 40.2 | 22.6 | 12.7 | 38.6 | 39.0 | 0.0 | 37.0 | 0.0 | 31.7 |
| Incr Delay（d2），s／veh | 8.7 | 15.2 | 15.8 | 3.5 | 12.9 | 0.0 | 2.0 | 2.9 | 0.0 | 13.2 | 0.0 | 0.0 |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ（50\％），veh／In | 1.1 | 15.1 | 15.6 | 3.1 | 17.5 | 0.7 | 3.6 | 4.2 | 0.0 | 6.8 | 0.0 | 0.1 |
| Unsig．Movement Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay（d），s／veh | 52.5 | 40.3 | 41.0 | 43.7 | 35.6 | 12.8 | 40.5 | 41.8 | 0.0 | 50.2 | 0.0 | 31.7 |
| LnGrp LOS | D | D | D | D | D | B | D | D |  | D | A | C |
| Approach Vol，veh／h |  | 1438 |  |  | 1883 |  |  | 357 | A |  | 276 |  |
| Approach Delay，s／veh |  | 41.0 |  |  | 35.3 |  |  | 41.2 |  |  | 49.7 |  |
| Approach LOS |  | D |  |  | D |  |  | D |  |  | D |  |


| Timer－Assigned Phs | 1 | 2 | 4 | 5 | 6 | 8 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Phs Duration（G＋Y＋Rc），s | 11.9 | 43.9 | 19.6 | 5.8 | 50.0 | 15.5 |
| Change Period（Y＋Rc），s | 3.0 | 6.0 | 4.4 | 3.0 | 6.0 | 4.4 |
| Max Green Setting（Gmax），s | 20.0 | 40.0 | 20.0 | 15.0 | 45.0 | 20.0 |
| Max Q Clear Time（g＿c＋11），s | 9.1 | 35.4 | 15.0 | 4.2 | 42.7 | 11.0 |
| Green Ext Time（p＿c），s | 0.0 | 1.4 | 0.2 | 0.0 | 1.3 | 0.1 |

## Intersection Summary

| HCM 6th Ctrl Delay | 38.9 |
| :--- | ---: |
| HCM 6th LOS | D |

## Notes

User approved pedestrian interval to be less than phase max green．
User approved volume balancing among the lanes for turning movement．
Unsignalized Delay for［NBR］is excluded from calculations of the approach delay and intersection delay．

| 4 | $\rightarrow$ | $\geqslant$ | 1 |  | 4 | $4$ | $\dagger$ | $p$ | $\pm$ | $\frac{1}{1}$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations＊／ | 44 | 「 | ＊ | 44 | T | ${ }^{*}$ | ¢ $\uparrow$ | 「 | ＊ | 44 | 「 |
| Traffic Volume（veh／h） 136 | 125 | 1022 | 74 | 251 | 96 | 1172 | 341 | 42 | 80 | 612 | 259 |
| Future Volume（veh／h） 136 | 125 | 1022 | 74 | 251 | 96 | 1172 | 341 | 42 | 80 | 612 | 259 |
| Initial Q（Qb），veh 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus，Adj 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow，veh／h／ln 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 |
| Adj Flow Rate，veh／h 151 | 139 | 0 | 82 | 279 | 0 | 1302 | 379 | 0 | 89 | 680 | 0 |
| Peak Hour Factor 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Percent Heavy Veh，\％ 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| Cap，veh／h 183 | 516 |  | 105 | 362 |  | 1384 | 727 |  | 384 | 766 |  |
| Arrive On Green 0.10 | 0.14 | 0.00 | 0.06 | 0.10 | 0.00 | 0.39 | 0.39 | 0.00 | 0.21 | 0.21 | 0.00 |
| Sat Flow，veh／h 1795 | 3582 | 1598 | 1795 | 3582 | 1598 | 3591 | 1885 | 1598 | 1795 | 3582 | 1598 |
| Grp Volume（v），veh／h 151 | 139 | 0 | 82 | 279 | 0 | 1302 | 379 | 0 | 89 | 680 | 0 |
| Grp Sat Flow（s），veh／h／ln1795 | 1791 | 1598 | 1795 | 1791 | 1598 | 1795 | 1885 | 1598 | 1795 | 1791 | 1598 |
| Q Serve（g＿s），s 8.0 | 3.4 | 0.0 | 4.4 | 7.4 | 0.0 | 34.1 | 15.1 | 0.0 | 4.0 | 18.0 | 0.0 |
| Cycle Q Clear（g＿c），s 8.0 | 3.4 | 0.0 | 4.4 | 7.4 | 0.0 | 34.1 | 15.1 | 0.0 | 4.0 | 18.0 | 0.0 |
| Prop In Lane 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Lane Grp Cap（c），veh／h 183 | 516 |  | 105 | 362 |  | 1384 | 727 |  | 384 | 766 |  |
| V／C Ratio（X） 0.83 | 0.27 |  | 0.78 | 0.77 |  | 0.94 | 0.52 |  | 0.23 | 0.89 |  |
| Avail Cap（c＿a），veh／h 460 | 918 |  | 276 | 735 |  | 1657 | 870 |  | 460 | 918 |  |
| HCM Platoon Ratio 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter（I） 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 |
| Uniform Delay（d），s／veh 43.0 | 37.2 | 0.0 | 45.3 | 42.7 | 0.0 | 28.9 | 23.0 | 0.0 | 31.7 | 37.2 | 0.0 |
| Incr Delay（d2），s／veh 3.6 | 0.1 | 0.0 | 4.6 | 1.3 | 0.0 | 9.3 | 0.2 | 0.0 | 0.1 | 8.3 | 0.0 |
| Initial Q Delay（d3），s／veh 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ（50\％），veh／IR3． 6 | 1.4 | 0.0 | 2.0 | 3.2 | 0.0 | 15.4 | 6.3 | 0.0 | 1.7 | 8.3 | 0.0 |
| Unsig．Movement Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay（d），s／veh 46.6 | 37.3 | 0.0 | 49.9 | 44.1 | 0.0 | 38.2 | 23.3 | 0.0 | 31.8 | 45.5 | 0.0 |
| LnGrp LOS D | D |  | D | D |  | D | C |  | C | D |  |
| Approach Vol，veh／h | 290 | A |  | 361 | A |  | 1681 | A |  | 769 | A |
| Approach Delay，s／veh | 42.1 |  |  | 45.4 |  |  | 34.8 |  |  | 43.9 |  |
| Approach LOS | D |  |  | D |  |  | C |  |  | D |  |
| Timer－Assigned Phs 1 | 2 |  | 4 | 5 | 6 |  | 8 |  |  |  |  |
| Phs Duration（G＋Y＋Rc），s8．7 | 19.8 |  | 26.2 | 12.9 | 15.6 |  | 42.9 |  |  |  |  |
| Change Period（Y＋Rc），s 3.0 | 5.7 |  | 5.3 | 3.0 | ＊ 5.7 |  | 5.3 |  |  |  |  |
| Max Green Setting（Gmak5，© | 25.0 |  | 25.0 | 25.0 | ＊ 20 |  | 45.0 |  |  |  |  |
| Max Q Clear Time（g＿c＋119，¢¢ | 5.4 |  | 20.0 | 10.0 | 9.4 |  | 36.1 |  |  |  |  |
| Green Ext Time（p＿c），s 0.0 | 0.2 |  | 0.9 | 0.0 | 0.5 |  | 1.5 |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |
| HCM 6th Ctrl Delay 39.0 |  |  |  |  |  |  |  |  |  |  |  |
| HCM 6th LOS D |  |  |  |  |  |  |  |  |  |  |  |
| Notes |  |  |  |  |  |  |  |  |  |  |  |
| User approved pedestrian interval to be less than phase max green． |  |  |  |  |  |  |  |  |  |  |  |
| User approved volume balancing among the lanes for turning movement． |  |  |  |  |  |  |  |  |  |  |  |
| ＊HCM 6th computational engine requires equal clearance times for the phases crossing the barrier． |  |  |  |  |  |  |  |  |  |  |  |

Unsignalized Delay for [NBR, EBR, WBR, SBR] is excluded from calculations of the approach delay and intersection delay.


Intersection Delay, s/veh52.4
Intersection LOS F

| Movement EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | 4 |  |  | $\uparrow$ | F |  | 4 |  |  | $\uparrow$ | 「 |
| Traffic Vol, veh/h 53 | 128 | 16 | 107 | 183 | 77 | 21 | 246 | 75 | 42 | 206 | 143 |
| Future Vol, veh/h 53 | 128 | 16 | 107 | 183 | 77 | 21 | 246 | 75 | 42 | 206 | 143 |
| Peak Hour Factor 0.80 | 0.80 | 0.80 | 0.80 | 0.80 | 0.80 | 0.80 | 0.80 | 0.80 | 0.80 | 0.80 | 0.80 |
| Heavy Vehicles, \% 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow 66 | 160 | 20 | 134 | 229 | 96 | 26 | 308 | 94 | 53 | 258 | 179 |
| Number of Lanes 0 | 1 | 0 | 0 | 1 | 1 | 0 | 1 | 0 | 0 | 1 | 1 |
| Approach EB |  |  | WB |  |  | NB |  |  | SB |  |  |
| Opposing Approach WB |  |  | EB |  |  | SB |  |  | NB |  |  |
| Opposing Lanes 2 |  |  | 1 |  |  | 2 |  |  | 1 |  |  |
| Conflicting Approach Left SB |  |  | NB |  |  | EB |  |  | WB |  |  |
| Conflicting Lanes Left 2 |  |  | 1 |  |  | 1 |  |  | 2 |  |  |
| Conflicting Approach RighNB |  |  | SB |  |  | WB |  |  | EB |  |  |
| Conflicting Lanes Right 1 |  |  | 2 |  |  | 2 |  |  | 1 |  |  |
| HCM Control Delay 31.3 |  |  | 47.9 |  |  | 95.1 |  |  | 30 |  |  |
| HCM LOS D |  |  | E |  |  | F |  |  | D |  |  |


| Lane | NBLn1 EBLn1WBLn1WBLn2 SBLn1 SBLn2 |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Vol Left, \% | $6 \%$ | $27 \%$ | $37 \%$ | $0 \%$ | $17 \%$ | $0 \%$ |
| Vol Thru, $\%$ | $72 \%$ | $65 \%$ | $63 \%$ | $0 \%$ | $83 \%$ | $0 \%$ |
| Vol Right, \% | $22 \%$ | $8 \%$ | $0 \%$ | $100 \%$ | $0 \%$ | $100 \%$ |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 342 | 197 | 290 | 77 | 248 | 143 |
| LT Vol | 21 | 53 | 107 | 0 | 42 | 0 |
| Through Vol | 246 | 128 | 183 | 0 | 206 | 0 |
| RT Vol | 75 | 16 | 0 | 77 | 0 | 143 |
| Lane Flow Rate | 428 | 246 | 362 | 96 | 310 | 179 |
| Geometry Grp | 6 | 6 | 7 | 7 | 7 | 7 |
| Degree of Util (X) | 1.069 | 0.668 | 0.911 | 0.217 | 0.774 | 0.406 |
| Departure Headway (Hd) | 9.00210 .145 | 9.331 | 8.408 | 9.303 | 8.483 |  |
| Convergence, Y/N | Yes | Yes | Yes | Yes | Yes | Yes |
| Cap | 406 | 360 | 392 | 429 | 391 | 427 |
| Service Time | 7.002 | 8.145 | 7.031 | 6.108 | 7.003 | 6.183 |
| HCM Lane V/C Ratio | 1.054 | 0.683 | 0.923 | 0.224 | 0.793 | 0.419 |
| HCM Control Delay | 95.1 | 31.3 | 57 | 13.4 | 37.5 | 16.9 |
| HCM Lane LOS | F | D | F | B | E | C |
| HCM 95th-tile Q | 14.5 | 4.6 | 9.5 | 0.8 | 6.5 | 1.9 |




| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | ＊＊ | 444 | 「 | ＊＊ | 444 | F＇ | ＊＊ | 444 | 「 | ＊＊ | 衡 |  |
| Traffic Volume（veh／h） | 394 | 1589 | 281 | 310 | 1354 | 238 | 446 | 876 | 206 | 248 | 765 | 148 |
| Future Volume（veh／h） | 394 | 1589 | 281 | 310 | 1354 | 238 | 446 | 876 | 206 | 248 | 765 | 148 |
| Initial Q（Qb），veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow，veh／h／ln | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 |
| Adj Flow Rate，veh／h | 419 | 1690 | 155 | 330 | 1440 | 0 | 474 | 932 | 0 | 264 | 814 | 137 |
| Peak Hour Factor | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 |
| Percent Heavy Veh，\％ | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| Cap，veh／h | 466 | 1784 | 553 | 551 | 1979 |  | 522 | 1330 |  | 313 | 881 | 147 |
| Arrive On Green | 0.13 | 0.35 | 0.35 | 0.16 | 0.38 | 0.00 | 0.15 | 0.26 | 0.00 | 0.09 | 0.20 | 0.20 |
| Sat Flow，veh／h | 3483 | 5147 | 1596 | 3483 | 5147 | 1598 | 3483 | 5147 | 1598 | 3483 | 4439 | 742 |
| Grp Volume（v），veh／h | 419 | 1690 | 155 | 330 | 1440 | 0 | 474 | 932 | 0 | 264 | 628 | 323 |
| Grp Sat Flow（s），veh／h／ln | 1742 | 1716 | 1596 | 1742 | 1716 | 1598 | 1742 | 1716 | 1598 | 1742 | 1716 | 1750 |
| Q Serve（g＿s），s | 17.8 | 47.9 | 7.0 | 13.2 | 35.9 | 0.0 | 20.1 | 24.6 | 0.0 | 11.2 | 26.9 | 27.2 |
| Cycle Q Clear（g＿c），s | 17.8 | 47.9 | 7.0 | 13.2 | 35.9 | 0.0 | 20.1 | 24.6 | 0.0 | 11.2 | 26.9 | 27.2 |
| Prop In Lane | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 0.42 |
| Lane Grp Cap（c），veh／h | 466 | 1784 | 553 | 551 | 1979 |  | 522 | 1330 |  | 313 | 681 | 347 |
| V／C Ratio（X） | 0.90 | 0.95 | 0.28 | 0.60 | 0.73 |  | 0.91 | 0.70 |  | 0.84 | 0.92 | 0.93 |
| Avail Cap（c＿a），veh／h | 534 | 1784 | 553 | 551 | 1979 |  | 604 | 1330 |  | 488 | 686 | 350 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter（l） | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay（d），s／veh | 64.0 | 47.7 | 15.8 | 58.7 | 39.4 | 0.0 | 62.7 | 50.4 | 0.0 | 67.2 | 59.0 | 59.1 |
| Incr Delay（d2），s／veh | 15.5 | 12.0 | 1.3 | 1.3 | 2.4 | 0.0 | 15.0 | 1.8 | 0.0 | 4.5 | 18.2 | 31.1 |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ（50\％），veh／In | 8.7 | 21.8 | 4.1 | 5.8 | 15.2 | 0.0 | 9.8 | 10.6 | 0.0 | 5.1 | 13.2 | 14.8 |
| Unsig．Movement Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay（d），s／veh | 79.5 | 59.7 | 17.1 | 60.0 | 41.8 | 0.0 | 77.8 | 52.2 | 0.0 | 71.7 | 77.2 | 90.2 |
| LnGrp LOS | E | E | B | E | D |  | E | D |  | E | E | F |
| Approach Vol，veh／h |  | 2264 |  |  | 1770 | A |  | 1406 | A |  | 1215 |  |
| Approach Delay，s／veh |  | 60.4 |  |  | 45.2 |  |  | 60.8 |  |  | 79.5 |  |
| Approach LOS |  | E |  |  | D |  |  | E |  |  | E |  |


| Timer－Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Phs Duration（G＋Y＋Rc），s | 29.7 | 58.0 | 26.5 | 35.8 | 24.1 | 63.7 | 17.5 | 44.8 |
| Change Period（Y＋Rc），s | 6.0 | 6.0 | 4.0 | 6.0 | 4.0 | 6.0 | 4.0 | 6.0 |
| Max Green Setting（Gmax），s | 20.0 | 52.0 | 26.0 | 30.0 | 23.0 | 51.0 | 21.0 | 35.0 |
| Max Q Clear Time（g＿c＋I1），s | 15.2 | 49.9 | 22.1 | 29.2 | 19.8 | 37.9 | 13.2 | 26.6 |
| Green Ext Time（p＿c），s | 0.3 | 1.9 | 0.4 | 0.5 | 0.3 | 8.1 | 0.3 | 4.4 |

## Intersection Summary

| HCM 6th Ctrl Delay | 59.9 |
| :--- | ---: |
| HCM 6th LOS | E |

## Notes

User approved pedestrian interval to be less than phase max green．
Unsignalized Delay for［NBR，WBR］is excluded from calculations of the approach delay and intersection delay．

| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay，s／veh 1.9 |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ＊ | 个4 | 「 | \％ | 㻢 |  |  | $\uparrow$ | F |  | $\uparrow$ | 「 |
| Traffic Vol，veh／h | 45 | 1907 | 56 | 31 | 1729 | 4 | 2 | 0 | 32 | 0 | 1 | 37 |
| Future Vol，veh／h | 45 | 1907 | 56 | 31 | 1729 | 4 | 2 | 0 | 32 | 0 | 1 | 37 |
| Conflicting Peds，\＃hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | － | － | None | － |  | None | ． |  | None | ． | － | None |
| Storage Length | 150 | － | 100 | 175 |  | － | － |  | 125 | － | － | 25 |
| Veh in Median Storage，\＃ | － | 0 | － | － | 0 | － | － | 0 | － |  | 0 | － |
| Grade，\％ | － | 0 | － | － | 0 | － | － | 0 | － | － | 0 | － |
| Peak Hour Factor | 94 | 94 | 94 | 94 | 94 | 94 | 94 | 94 | 94 | 94 | 94 | 94 |
| Heavy Vehicles，\％ | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| Mumt Flow | 48 | 2029 | 60 | 33 | 1839 | 4 | 2 | 0 | 34 | 0 | 1 | 39 |


| Major／Minor | Major1 |  |  | Major2 |  |  | Minor1 |  |  | Minor2 |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 1843 | 0 | 0 |  | 2089 | 0 | 0 | 3111 | 4034 | 1015 | 3018 | 4092 | 922 |
| Stage 1 |  | － | － |  | － | － |  | 2125 | 2125 | － | 1907 | 1907 | － |
| Stage 2 |  | － | － |  | － | － | － | 986 | 1909 | － | 1111 | 2185 |  |
| Critical Hdwy | 4.12 | － | － |  | 4.12 | － | － | 7.52 | 6.52 | 6.92 | 7.52 | 6.52 | 6.92 |
| Critical Hdwy Stg 1 |  | － | － |  | － | － |  | 6.52 | 5.52 | － | 6.52 | 5.52 | － |
| Critical Hdwy Stg 2 | － | － | － |  | － | － |  | 6.52 | 5.52 | － | 6.52 | 5.52 | － |
| Follow－up Hdwy | 2.21 | － | － |  | 2.21 | － | － | 3.51 | 4.01 | 3.31 | 3.51 | 4.01 | 3.31 |
| Pot Cap－1 Maneuver | 330 | － | － |  | 265 | － | － | － 5 | 3 | 238 | 6 | 2 | 274 |
| Stage 1 |  | － | － |  |  | － |  | 52 | 90 | － | 71 | 116 |  |
| Stage 2 | － | － | － |  | － | － |  | 268 | 116 | － | 225 | 84 | － |
| Platoon blocked，\％ |  | － | － |  |  | － | － |  |  |  |  |  |  |
| Mov Cap－1 Maneuver | 330 | － | － |  | 265 | － | － | － | 2 | 238 | 4 | $\sim 1$ | 274 |
| Mov Cap－2 Maneuver | － | － | － |  | － | － | － | － | 2 | － | 4 | $\sim 1$ | － |
| Stage 1 | － | － |  |  | － |  |  | 44 | 77 | － | 61 | 102 | － |
| Stage 2 | － | － |  |  | － |  |  | 199 | 102 | － | 165 | 72 | － |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Approach | EB |  |  |  | WB |  |  | NB |  |  | SB |  |  |
| HCM Control Delay，s | 0.4 |  |  |  | 0.4 |  |  |  |  |  | 149.6 |  |  |
| HCM LOS |  |  |  |  |  |  |  | － |  |  | F |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Minor Lane／Major Mvmt | NBLn1 | BLn2 | EBL | EBT | EBR | WBL | WBT | WBR | SBLn1 | SBLn2 |  |  |  |
| Capacity（veh／h） | － | 238 | 330 | － | － | 265 | － | － | 1 | 274 |  |  |  |
| HCM Lane V／C Ratio | － | 0.143 | 0.145 | － | － | 0.124 | － | － | 1.064 | 0.144 |  |  |  |
| HCM Control Delay（s） | － | 22.6 | 17.8 | － | － | 20.5 | － | \＄ | 4932.2 | 20.3 |  |  |  |
| HCM Lane LOS |  | C | C |  |  | C | － | － | F | C |  |  |  |
| HCM 95th \％tile Q（veh） |  | 0.5 | 0.5 |  | － | 0.4 | － | － | 0.6 | 0.5 |  |  |  |
| Notes |  |  |  |  |  |  |  |  |  |  |  |  |  |
| $\sim$ ：Volume exceeds capacity | \＄：D | ay exc | eeds 3 | 300s | ＋：Com | putation | Not D | Defined | ＊：All | major v | volume | in plato |  |


|  | $\Rightarrow$ |  |  | $\checkmark$ | $\leftarrow$ |  |  | $\dagger$ |  |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \% | 性 |  | \% | 个t |  |  |  |  |  | $\uparrow$ | F |
| Traffic Volume (veh/h) | 34 | 1905 | 0 | 0 | 1729 | 18 | 0 | 0 | 0 | 26 | 0 | 31 |
| Future Volume (veh/h) | 34 | 1905 | 0 | 0 | 1729 | 18 | 0 | 0 | 0 | 26 | 0 | 31 |
| Initial $\mathrm{Q}(\mathrm{Qb})$, veh | 0 | 0 | 0 | 0 | 0 | 0 |  |  |  | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 |  | 1.00 | 1.00 |  | 0.98 |  |  |  | 1.00 |  | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |  | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  |  |  |  | No |  |
| Adj Sat Flow, veh/h/ln | 1885 | 1885 | 1885 | 1870 | 1885 | 1885 |  |  |  | 1885 | 1870 | 1885 |
| Adj Flow Rate, veh/h | 36 | 2027 | 0 | 0 | 1839 | 19 |  |  |  | 28 | 0 | 12 |
| Peak Hour Factor | 0.94 | 0.94 | 0.92 | 0.92 | 0.94 | 0.94 |  |  |  | 0.94 | 0.92 | 0.94 |
| Percent Heavy Veh, \% | 1 | 1 | 1 | 2 | 1 | 1 |  |  |  | 1 | 2 | 1 |
| Cap, veh/h | 43 | 2679 | 0 | 3 | 2451 | 25 |  |  |  | 100 | 0 | 90 |
| Arrive On Green | 0.02 | 0.75 | 0.00 | 0.00 | 0.67 | 0.67 |  |  |  | 0.06 | 0.00 | 0.06 |
| Sat Flow, veh/h | 1795 | 3676 | 0 | 1781 | 3631 | 37 |  |  |  | 1781 | 0 | 1598 |
| Grp Volume(v), veh/h | 36 | 2027 | 0 | 0 | 906 | 952 |  |  |  | 28 | 0 | 12 |
| Grp Sat Flow(s),veh/h/n | 1795 | 1791 | 0 | 1781 | 1791 | 1877 |  |  |  | 1781 | 0 | 1598 |
| Q Serve(g_s), s | 1.2 | 20.2 | 0.0 | 0.0 | 20.4 | 20.5 |  |  |  | 0.9 | 0.0 | 0.4 |
| Cycle Q Clear(g_c), s | 1.2 | 20.2 | 0.0 | 0.0 | 20.4 | 20.5 |  |  |  | 0.9 | 0.0 | 0.4 |
| Prop In Lane | 1.00 |  | 0.00 | 1.00 |  | 0.02 |  |  |  | 1.00 |  | 1.00 |
| Lane Grp Cap(c), veh/h | 43 | 2679 | 0 | 3 | 1209 | 1267 |  |  |  | 100 | 0 | 90 |
| V/C Ratio(X) | 0.83 | 0.76 | 0.00 | 0.00 | 0.75 | 0.75 |  |  |  | 0.28 | 0.00 | 0.13 |
| Avail Cap(c_a), veh/h | 673 | 3912 | 0 | 378 | 1956 | 2051 |  |  |  | 1946 | 0 | 1745 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |  | 1.00 | 1.00 | 1.00 |
| Upstream Filter(1) | 1.00 | 1.00 | 0.00 | 0.00 | 1.00 | 1.00 |  |  |  | 1.00 | 0.00 | 1.00 |
| Uniform Delay (d), s/veh | 29.8 | 4.5 | 0.0 | 0.0 | 6.6 | 6.6 |  |  |  | 27.7 | 0.0 | 27.5 |
| Incr Delay (d2), s/veh | 13.8 | 0.5 | 0.0 | 0.0 | 1.0 | 0.9 |  |  |  | 1.5 | 0.0 | 0.7 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |  |  | 0.0 | 0.0 | 0.0 |
| \%ile BackOfQ(50\%),veh/ln | 0.6 | 0.9 | 0.0 | 0.0 | 3.1 | 3.3 |  |  |  | 0.4 | 0.0 | 0.0 |
| Unsig. Movement Delay, s/veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay(d),s/veh | 43.6 | 5.0 | 0.0 | 0.0 | 7.5 | 7.5 |  |  |  | 29.2 | 0.0 | 28.2 |
| LnGrp LOS | D | A | A | A | A | A |  |  |  | C | A | C |
| Approach Vol, veh/h |  | 2063 |  |  | 1858 |  |  |  |  |  | 40 |  |
| Approach Delay, s/veh |  | 5.7 |  |  | 7.5 |  |  |  |  |  | 28.9 |  |
| Approach LOS |  | A |  |  | A |  |  |  |  |  | C |  |


| Timer - Assigned Phs | 1 | 2 | 4 | 5 | 6 |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Phs Duration $(G+Y+R c)$, s | 4.5 | 47.4 | 9.5 | 0.0 | 51.9 |
| Change Period (Y+Rc), s | 3.0 | 6.0 | 6.0 | 3.0 | 6.0 |
| Max Green Setting (Gmax), s | 23.0 | 67.0 | 67.0 | 13.0 | 67.0 |
| Max Q Clear Time (g_c+1), s | 3.2 | 22.5 | 2.9 | 0.0 | 22.2 |
| Green Ext Time (p_C), s | 0.0 | 18.9 | 0.2 | 0.0 | 23.6 |

## Intersection Summary

| HCM 6th Ctrl Delay | 6.8 |
| :--- | ---: |
| HCM 6th LOS | A |

## Notes

User approved ignoring U-Turning movement.

| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |


| Major/Minor | Major1 | Major2 |  | Minor1 |  |
| :--- | ---: | ---: | :--- | :--- | :--- |
| Conflicting Flow All | 0 | 0 | 2087 | 0 | -1044 |
| $\quad$ Stage 1 | - | - | - | - | - |
| $\quad$ Stage 2 | - | - | - | - | - |
| Critical Hdwy | - | - | 4.14 | - | - |
| Critical Hdwy Stg 1 | - | - | - | - | - |
| Critical Hdwy Stg 2 | - | - | - | - | - |
| Follow-up Hdwy | - | - | 2.22 | - | - |
| Pot Cap-1 Maneuver | - | - | 262 | - | 0 |
| $\quad$ Stage 1 | - | - | - | - | 0 |
| $\quad$ Stage 2 | - | - | - | - | 0 |


|  | EB | WB | NB |
| :--- | ---: | ---: | ---: |
| Approach |  |  |  |
| HCM Control Delay, $s$ | 0 | 0.1 | 24.6 |
| HCM LOS |  |  | C |


| Minor Lane/Major Mvmt | NBLn1 | EBT | EBR | WBL | WBT |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Capacity (veh/h) | 226 | - |  | 262 | - |  |
| HCM Lane V/C Ratio | 0.188 | - |  | 0.054 |  |  |
| HCM Control Delay (s) | 24.6 | - |  | 19.5 |  |  |
| HCM Lane LOS | C | - |  | C |  |  |
| HCM 95th \%tile Q(veh) | 0.7 | - |  | 0.2 |  |  |


| Intersection |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0.8 |  |  |  |  |

 Stage 2

| Approach | EB | WB | NB | SB |
| :--- | :---: | :---: | :---: | :---: |
| HCM Control Delay, s | 0.6 | 0.4 | 19.8 | 20 |
| HCM LOS |  | $C$ | C |  |


| Minor Lane/Major Mvmt | NBLn1 | EBL | EBT | EBR | WBL | WBT | WBR SBLn1 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 255 | 352 | - | -303 | - | -290 |  |
| HCM Lane V/C Ratio | 0.045 | 0.203 | - | -0.139 | - | -0.174 |  |
| HCM Control Delay (s) | 19.8 | 17.8 | - | - | 18.8 | - | - |
| HCM Lane LOS | C | C | - | - | C | - | - |
| HCM 95th \%tile Q(veh) | 0.1 | 0.8 | - | - | 0.5 | - | - |
| C | 0.6 |  |  |  |  |  |  |


| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | ＊ | 中\％ |  | \＃ | 44 | 「 | ${ }^{7}$ | $\uparrow$ | 「 |  | $\uparrow$ | 「 |
| Traffic Volume（veh／h） | 45 | 1567 | 199 | 92 | 1503 | 165 | 132 | 75 | 102 | 147 | 90 | 56 |
| Future Volume（veh／h） | 45 | 1567 | 199 | 92 | 1503 | 165 | 132 | 75 | 102 | 147 | 90 | 56 |
| Initial Q（Qb），veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 0.98 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow，veh／h／ln | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Adj Flow Rate，veh／h | 46 | 1615 | 198 | 95 | 1549 | 128 | 106 | 118 | 0 | 152 | 93 | 13 |
| Peak Hour Factor | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 |
| Percent Heavy Veh，\％ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Cap，veh／h | 58 | 1549 | 187 | 122 | 1856 | 827 | 154 | 162 |  | 178 | 109 | 250 |
| Arrive On Green | 0.03 | 0.48 | 0.48 | 0.07 | 0.51 | 0.51 | 0.09 | 0.09 | 0.00 | 0.16 | 0.16 | 0.16 |
| Sat Flow，veh／h | 1810 | 3235 | 390 | 1810 | 3610 | 1609 | 1810 | 1900 | 1610 | 1143 | 700 | 1610 |
| Grp Volume（v），veh／h | 46 | 888 | 925 | 95 | 1549 | 128 | 106 | 118 | 0 | 245 | 0 | 13 |
| Grp Sat Flow（s），veh／h／ln | 1810 | 1805 | 1820 | 1810 | 1805 | 1609 | 1810 | 1900 | 1610 | 1843 | 0 | 1610 |
| Q Serve（g＿s），s | 2.1 | 40.0 | 40.0 | 4.3 | 30.5 | 3.5 | 4.8 | 5.1 | 0.0 | 10.8 | 0.0 | 0.6 |
| Cycle Q Clear（g＿c），s | 2.1 | 40.0 | 40.0 | 4.3 | 30.5 | 3.5 | 4.8 | 5.1 | 0.0 | 10.8 | 0.0 | 0.6 |
| Prop In Lane | 1.00 |  | 0.21 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 0.62 |  | 1.00 |
| Lane Grp Cap（c），veh／h | 58 | 864 | 872 | 122 | 1856 | 827 | 154 | 162 |  | 286 | 0 | 250 |
| V／C Ratio（X） | 0.79 | 1.03 | 1.06 | 0.78 | 0.83 | 0.15 | 0.69 | 0.73 |  | 0.86 | 0.00 | 0.05 |
| Avail Cap（c＿a），veh／h | 325 | 864 | 872 | 433 | 1945 | 867 | 433 | 455 |  | 441 | 0 | 386 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter（I） | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 0.00 | 1.00 |
| Uniform Delay（d），s／veh | 40.1 | 21.8 | 21.8 | 38.3 | 17.3 | 10.7 | 37.1 | 37.3 | 0.0 | 34.4 | 0.0 | 30.0 |
| Incr Delay（d2），s／veh | 8.3 | 37.9 | 48.0 | 4.0 | 2.9 | 0.0 | 2.0 | 2.4 | 0.0 | 6.2 | 0.0 | 0.0 |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ（50\％），veh／ln | 1.0 | 22.5 | 25.2 | 1.9 | 10.9 | 1.0 | 2.1 | 2.4 | 0.0 | 5.2 | 0.0 | 0.2 |
| Unsig．Movement Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay（d），s／veh | 48.5 | 59.7 | 69.8 | 42.3 | 20.2 | 10.7 | 39.2 | 39.6 | 0.0 | 40.5 | 0.0 | 30.1 |
| LnGrp LOS | D | F | F | D | C | B | D | D |  | D | A | C |
| Approach Vol，veh／h |  | 1859 |  |  | 1772 |  |  | 224 | A |  | 258 |  |
| Approach Delay，s／veh |  | 64.4 |  |  | 20.7 |  |  | 39.4 |  |  | 40.0 |  |
| Approach LOS |  | E |  |  | C |  |  | D |  |  | D |  |


| Timer－Assigned Phs | 1 | 2 | 4 | 5 | 6 | 8 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Phs Duration（G＋Y＋Rc），s | 8.6 | 46.0 | 17.4 | 5.7 | 48.9 | 11.5 |
| Change Period（Y＋Rc），s | 3.0 | 6.0 | 4.4 | 3.0 | 6.0 | 4.4 |
| Max Green Setting（Gmax），s | 20.0 | 40.0 | 20.0 | 15.0 | 45.0 | 20.0 |
| Max Q Clear Time（g＿c＋11），s | 6.3 | 42.0 | 12.8 | 4.1 | 32.5 | 7.1 |
| Green Ext Time（p＿c），s | 0.0 | 0.0 | 0.2 | 0.0 | 3.5 | 0.1 |

## Intersection Summary

| HCM 6th Ctrl Delay | 42.7 |
| :--- | ---: |
| HCM 6th LOS | D |

## Notes

User approved pedestrian interval to be less than phase max green．
User approved volume balancing among the lanes for turning movement．
Unsignalized Delay for［NBR］is excluded from calculations of the approach delay and intersection delay．

| 4 | $\rightarrow$ | $\checkmark$ | 1 |  | 4 | 4 | $\dagger$ | \％ | $\pm$ | $\frac{1}{1}$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations＊／ | 44 | 「 | ＊ | 44 | T | ${ }^{*}$ | －${ }^{4}$ | 「 | ＊ | 44 | F |
| Traffic Volume（veh／h） 211 | 269 | 1108 | 57 | 235 | 98 | 1176 | 689 | 80 | 111 | 440 | 201 |
| Future Volume（veh／h） 211 | 269 | 1108 | 57 | 235 | 98 | 1176 | 689 | 80 | 111 | 440 | 201 |
| Initial Q（Qb），veh 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus，Adj 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow，veh／h／ln 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 |
| Adj Flow Rate，veh／h 220 | 280 | 0 | 59 | 245 | 0 | 1225 | 718 | 0 | 116 | 458 | 0 |
| Peak Hour Factor 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 |
| Percent Heavy Veh，\％ 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| Cap，veh／h 253 | 693 |  | 76 | 339 |  | 1461 | 767 |  | 277 | 553 |  |
| Arrive On Green 0.14 | 0.19 | 0.00 | 0.04 | 0.09 | 0.00 | 0.41 | 0.41 | 0.00 | 0.15 | 0.15 | 0.00 |
| Sat Flow，veh／h 1795 | 3582 | 1598 | 1795 | 3582 | 1598 | 3591 | 1885 | 1598 | 1795 | 3582 | 1598 |
| Grp Volume（v），veh／h 220 | 280 | 0 | 59 | 245 | 0 | 1225 | 718 | 0 | 116 | 458 | 0 |
| Grp Sat Flow（s），veh／h／ln1795 | 1791 | 1598 | 1795 | 1791 | 1598 | 1795 | 1885 | 1598 | 1795 | 1791 | 1598 |
| Q Serve（g＿s），s 11.4 | 6.5 | 0.0 | 3.1 | 6.3 | 0.0 | 29.2 | 34.7 | 0.0 | 5.6 | 11.8 | 0.0 |
| Cycle Q Clear（g＿c），s 11.4 | 6.5 | 0.0 | 3.1 | 6.3 | 0.0 | 29.2 | 34.7 | 0.0 | 5.6 | 11.8 | 0.0 |
| Prop In Lane 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Lane Grp Cap（c），veh／h 253 | 693 |  | 76 | 339 |  | 1461 | 767 |  | 277 | 553 |  |
| V／C Ratio（X） 0.87 | 0.40 |  | 0.78 | 0.72 |  | 0.84 | 0.94 |  | 0.42 | 0.83 |  |
| Avail Cap（c＿a），veh／h 471940 |  |  | 283 | 752 |  | 1696 | 891 |  | 471 | 940 |  |
| HCM Platoon Ratio 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter（I） 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 |
| Uniform Delay（d），s／veh 40.0 | 33.6 | 0.0 | 45.2 | 41.9 | 0.0 | 25.4 | 27.0 | 0.0 | 36.4 | 39.0 | 0.0 |
| Incr Delay（d2），s／veh 3.5 | 0.1 | 0.0 | 6.2 | 1.1 | 0.0 | 3.0 | 14.6 | 0.0 | 0.4 | 1.2 | 0.0 |
| Initial Q Delay（d3），s／veh 0.0 \％ile BackOfQ（50\％），veh／／r5．0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
|  | 2.7 | 0.0 | 1.5 | 2.8 | 0.0 | 12.1 | 17.4 | 0.0 | 2.4 | 5.0 | 0.0 |
| Unsig．Movement Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay（d），s／veh 43.6 | 33.7 | 0.0 | 51.3 | 43.0 | 0.0 | 28.4 | 41.7 | 0.0 | 36.8 | 40.3 | 0.0 |
| LnGrp LOS D | C |  | D | D |  | C | D |  | D | D |  |
| Approach Vol，veh／h | 500 | A |  | 304 | A |  | 1943 | A |  | 574 | A |
| Approach Delay，s／veh | 38.1 |  |  | 44.6 |  |  | 33.3 |  |  | 39.6 |  |
| Approach LOS | D |  |  | D |  |  | C |  |  | D |  |
| Timer－Assigned Phs 1 | 2 |  | 4 | 5 | 6 |  | 8 |  |  |  |  |
| Phs Duration（G＋Y＋Rc），s7．0 | 24.1 |  | 20.0 | 16.4 | 14.7 |  | 44.1 |  |  |  |  |
| Change Period（Y＋Rc），s 3.0 | 5.7 |  | 5.3 | 3.0 | ＊ 5.7 |  | 5.3 |  |  |  |  |
| Max Green Setting（Gmak5，© | 25.0 |  | 25.0 | 25.0 | ＊ 20 |  | 45.0 |  |  |  |  |
| Max Q Clear Time（g＿c＋1年，1s | 8.5 |  | 13.8 | 13.4 | 8.3 |  | 36.7 |  |  |  |  |
| Green Ext Time（p＿c），s 0.0 | 0.5 |  | 0.8 | 0.1 | 0.4 |  | 2.0 |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |
| HCM 6th Ctrl Delay 36.1 |  |  |  |  |  |  |  |  |  |  |  |
| HCM 6th LOS D |  |  |  |  |  |  |  |  |  |  |  |
| Notes |  |  |  |  |  |  |  |  |  |  |  |
| User approved pedestrian interval to be less than phase max green． |  |  |  |  |  |  |  |  |  |  |  |
| User approved volume balancing among the lanes for turning movement． |  |  |  |  |  |  |  |  |  |  |  |
| ＊HCM 6th computational engine requires equal clearance times for the phases crossing the barrier． |  |  |  |  |  |  |  |  |  |  |  |

Unsignalized Delay for [NBR, EBR, WBR, SBR] is excluded from calculations of the approach delay and intersection delay.
Intersection
Intersection Delay, s/veh24.1
Intersection LOS $\quad$ C


| Lane | NBLn1 EBLn1WBLn1WBLn2 SBLn1 SBLn2 |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Vol Left, \% | $8 \%$ | $14 \%$ | $24 \%$ | $0 \%$ | $28 \%$ | $0 \%$ |
| Vol Thru, \% | $80 \%$ | $70 \%$ | $76 \%$ | $0 \%$ | $72 \%$ | $0 \%$ |
| Vol Right, \% | $12 \%$ | $16 \%$ | $0 \%$ | $100 \%$ | $0 \%$ | $100 \%$ |
| Sign Control | Sttop | Stop | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 226 | 309 | 156 | 51 | 339 | 40 |
| LT Vol | 18 | 44 | 38 | 0 | 96 | 0 |
| Through Vol | 180 | 217 | 118 | 0 | 243 | 0 |
| RT Vol | 28 | 48 | 0 | 51 | 0 | 40 |
| Lane Flow Rate | 248 | 340 | 171 | 56 | 373 | 44 |
| Geometry Grp | 6 | 6 | 7 | 7 | 7 | 7 |
| Degree of Util (X) | 0.537 | 0.714 | 0.383 | 0.112 | 0.774 | 0.081 |
| Departure Headway (Hd) | 7.781 | 7.57 | 8.04 | 7.192 | 7.479 | 6.615 |
| Convergence, Y/N | Yes | Yes | Yes | Yes | Yes | Yes |
| Cap | 462 | 479 | 447 | 498 | 484 | 543 |
| Service Time | 5.838 | 5.591 | 5.796 | 4.947 | 5.202 | 4.338 |
| HCM Lane V/C Ratio | 0.537 | 0.71 | 0.383 | 0.112 | 0.771 | 0.081 |
| HCM Control Delay | 19.6 | 27.4 | 15.7 | 10.9 | 31.5 | 9.9 |
| HCM Lane LOS | C | D | C | B | D | A |
| HCM 95th-tile Q | 3.1 | 5.6 | 1.8 | 0.4 | 6.8 | 0.3 |




| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | ＊＊ | 444 | 「 | ${ }_{4}^{4} 1$ | 4种 | 「 | ${ }_{4}^{4}$ | 444 | 「 | ＊＊ | 性 $\%$ |  |
| Traffic Volume（veh／h） | 184 | 1156 | 172 | 227 | 1687 | 113 | 438 | 811 | 130 | 209 | 581 | 171 |
| Future Volume（veh／h） | 184 | 1156 | 172 | 227 | 1687 | 113 | 438 | 811 | 130 | 209 | 581 | 171 |
| Initial Q（Qb），veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 0.99 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 0.99 |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow，veh／h／ln | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 |
| Adj Flow Rate，veh／h | 200 | 1257 | 60 | 247 | 1834 | 0 | 476 | 882 | 0 | 227 | 632 | 138 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh，\％ | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap，veh／h | 259 | 1659 | 508 | 533 | 2149 |  | 531 | 1297 |  | 289 | 773 | 166 |
| Arrive On Green | 0.07 | 0.32 | 0.32 | 0.15 | 0.42 | 0.00 | 0.20 | 0.34 | 0.00 | 0.08 | 0.18 | 0.18 |
| Sat Flow，veh／h | 3456 | 5106 | 1564 | 3456 | 5106 | 1585 | 3456 | 5106 | 1585 | 3456 | 4202 | 903 |
| Grp Volume（v），veh／h | 200 | 1257 | 60 | 247 | 1834 | 0 | 476 | 882 | 0 | 227 | 510 | 260 |
| Grp Sat Flow（s），veh／h／ln | 1728 | 1702 | 1564 | 1728 | 1702 | 1585 | 1728 | 1702 | 1585 | 1728 | 1702 | 1701 |
| Q Serve（g＿s），s | 6.8 | 26.5 | 2.1 | 7.8 | 39.0 | 0.0 | 16.1 | 17.8 | 0.0 | 7.7 | 17.3 | 17.7 |
| Cycle Q Clear（g＿c），s | 6.8 | 26.5 | 2.1 | 7.8 | 39.0 | 0.0 | 16.1 | 17.8 | 0.0 | 7.7 | 17.3 | 17.7 |
| Prop In Lane | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 0.53 |
| Lane Grp Cap（c），veh／h | 259 | 1659 | 508 | 533 | 2149 |  | 531 | 1297 |  | 289 | 626 | 313 |
| V／C Ratio（X） | 0.77 | 0.76 | 0.12 | 0.46 | 0.85 |  | 0.90 | 0.68 |  | 0.79 | 0.81 | 0.83 |
| Avail Cap（c＿a），veh／h | 461 | 1659 | 508 | 533 | 2149 |  | 605 | 1297 |  | 605 | 681 | 340 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.33 | 1.33 | 1.33 | 1.00 | 1.00 | 1.00 |
| Upstream Filter（l） | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay（d），s／veh | 54.5 | 36.3 | 12.0 | 46.2 | 31.4 | 0.0 | 46.8 | 35.5 | 0.0 | 53.9 | 47.0 | 47.2 |
| Incr Delay（d2），s／veh | 1.9 | 3.3 | 0.5 | 0.2 | 3.6 | 0.0 | 13.8 | 1.6 | 0.0 | 1.8 | 7.6 | 15.9 |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ（50\％），veh／In | 3.0 | 11.0 | 1.2 | 3.3 | 15.7 | 0.0 | 7.4 | 6.8 | 0.0 | 3.4 | 7.8 | 8.6 |
| Unsig．Movement Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay（d），s／veh | 56.3 | 39.6 | 12.4 | 46.5 | 35.0 | 0.0 | 60.6 | 37.1 | 0.0 | 55.8 | 54.6 | 63.1 |
| LnGrp LOS | E | D | B | D | D |  | E | D |  | E | D | E |
| Approach Vol，veh／h |  | 1517 |  |  | 2081 | A |  | 1358 | A |  | 997 |  |
| Approach Delay，s／veh |  | 40.7 |  |  | 36.4 |  |  | 45.4 |  |  | 57.1 |  |
| Approach LOS |  | D |  |  | D |  |  | D |  |  | E |  |


| Timer－Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Phs Duration（G＋Y＋Rc），s | 24.5 | 45.0 | 22.4 | 28.1 | 13.0 | 56.5 | 14.0 | 36.5 |
| Change Period（Y＋Rc），s | 6.0 | 6.0 | 4.0 | 6.0 | 4.0 | 6.0 | 4.0 | 6.0 |
| Max Green Setting（Gmax），s | 14.0 | 39.0 | 21.0 | 24.0 | 16.0 | 39.0 | 21.0 | 24.0 |
| Max Q Clear Time（g＿c＋I1），s | 9.8 | 28.5 | 18.1 | 19.7 | 8.8 | 41.0 | 9.7 | 19.8 |
| Green Ext Time（p＿c），s | 0.2 | 7.2 | 0.3 | 2.3 | 0.2 | 0.0 | 0.3 | 2.4 |

## Intersection Summary

| HCM 6th Ctrl Delay | 43.0 |
| :--- | ---: |
| HCM 6th LOS | D |

## Notes

User approved pedestrian interval to be less than phase max green．
Unsignalized Delay for［NBR，WBR］is excluded from calculations of the approach delay and intersection delay．



|  | $y$ | $\rightarrow$ |  | 5 | $\dagger$ |  |  | 4 | $\uparrow$ | P | $t$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBU | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT |
| Lane Configurations | \# | 个t |  |  | * | 中 ${ }^{\text {P }}$ |  |  |  |  |  | $\uparrow$ |
| Traffic Volume (veh/h) | 58 | 1384 | 0 | 2 | - | 1843 | 82 | 0 | 0 | 0 | 50 | 0 |
| Future Volume (veh/h) | 58 | 1384 | 0 | 2 | 0 | 1843 | 82 | 0 | 0 | 0 | 50 | 0 |
| Initial Q (Qb), veh | 0 | 0 | 0 |  | 0 | 0 | 0 |  |  |  | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 |  | 1.00 |  | 1.00 |  | 0.98 |  |  |  | 1.00 |  |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 |  |  |  | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  |  | No |  |  |  |  |  | No |
| Adj Sat Flow, veh/h/ln | 1870 | 1870 | 1870 |  | 1870 | 1870 | 1870 |  |  |  | 1870 | 1870 |
| Adj Flow Rate, veh/h | 63 | 1504 | 0 |  | 0 | 2003 | 87 |  |  |  | 54 | 0 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 |  | 0.92 | 0.92 | 0.92 |  |  |  | 0.92 | 0.92 |
| Percent Heavy Veh, \% | 2 | 2 | 2 |  | 2 | 2 | 2 |  |  |  | 2 | 2 |
| Cap, veh/h | 80 | 2907 | 0 |  | 3 | 2531 | 109 |  |  |  | 80 | 0 |
| Arrive On Green | 0.05 | 0.82 | 0.00 |  | 0.00 | 0.73 | 0.73 |  |  |  | 0.04 | 0.00 |
| Sat Flow, veh/h | 1781 | 3647 | 0 |  | 1781 | 3467 | 149 |  |  |  | 1781 | 0 |
| Grp Volume(v), veh/h | 63 | 1504 | 0 |  | 0 | 1018 | 1072 |  |  |  | 54 | 0 |
| Grp Sat Flow(s),veh/h/ln | 1781 | 1777 | 0 |  | 1781 | 1777 | 1840 |  |  |  | 1781 | 0 |
| Q Serve(g_s), s | 2.4 | 9.3 | 0.0 |  | 0.0 | 25.1 | 26.2 |  |  |  | 2.1 | 0.0 |
| Cycle Q Clear (g_c), s | 2.4 | 9.3 | 0.0 |  | 0.0 | 25.1 | 26.2 |  |  |  | 2.1 | 0.0 |
| Prop In Lane | 1.00 |  | 0.00 |  | 1.00 |  | 0.08 |  |  |  | 1.00 |  |
| Lane Grp Cap(c), veh/h | 80 | 2907 | 0 |  | 3 | 1297 | 1343 |  |  |  | 80 | 0 |
| V/C Ratio(X) | 0.79 | 0.52 | 0.00 |  | 0.00 | 0.79 | 0.80 |  |  |  | 0.68 | 0.00 |
| Avail Cap(c_a), veh/h | 591 | 3433 | 0 |  | 334 | 1716 | 1777 |  |  |  | 873 | 0 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 |  |  |  | 1.00 | 1.00 |
| Upstream Filter(l) | 1.00 | 1.00 | 0.00 |  | 0.00 | 1.00 | 1.00 |  |  |  | 1.00 | 0.00 |
| Uniform Delay (d), s/veh | 32.8 | 2.0 | 0.0 |  | 0.0 | 5.9 | 6.1 |  |  |  | 32.6 | 0.0 |
| Incr Delay (d2), s/veh | 6.2 | 0.1 | 0.0 |  | 0.0 | 1.8 | 2.0 |  |  |  | 3.7 | 0.0 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 |  |  |  | 0.0 | 0.0 |
| \%ile BackOfQ(50\%),veh/ln | 1.1 | 0.1 | 0.0 |  | 0.0 | 3.5 | 3.8 |  |  |  | 1.0 | 0.0 |
| Unsig. Movement Delay, s/veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay (d),s/veh | 39.0 | 2.1 | 0.0 |  | 0.0 | 7.7 | 8.0 |  |  |  | 36.3 | 0.0 |
| LnGrp LOS | D | A | A |  | A | A | A |  |  |  | D | A |
| Approach Vol, veh/h |  | 1567 |  |  |  | 2090 |  |  |  |  |  | 68 |
| Approach Delay, s/veh |  | 3.6 |  |  |  | 7.9 |  |  |  |  |  | 35.5 |
| Approach LOS |  | A |  |  |  | A |  |  |  |  |  | D |
| Timer - Assigned Phs | 1 | 2 |  | 4 | 5 | 6 |  |  |  |  |  |  |
| Phs Duration ( $\mathrm{G}+\mathrm{Y}+\mathrm{Rc}$ ), s | 6.1 | 56.6 |  | 6.6 | 0.0 | 62.7 |  |  |  |  |  |  |
| Change Period ( $\mathrm{Y}+\mathrm{Rc}$ ), s | 3.0 | 6.0 |  | 3.5 | 3.0 | 6.0 |  |  |  |  |  |  |
| Max Green Setting (Gmax), s | 23.0 | 67.0 |  | 34.0 | 13.0 | 67.0 |  |  |  |  |  |  |
| Max Q Clear Time (g_c+1), s | 4.4 | 28.2 |  | 4.1 | 0.0 | 11.3 |  |  |  |  |  |  |
| Green Ext Time (p_c), s | 0.0 | 22.5 |  | 0.2 | 0.0 | 14.6 |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 6th Ctrl Delay |  |  | 6.6 |  |  |  |  |  |  |  |  |  |
| HCM 6th LOS |  |  | A |  |  |  |  |  |  |  |  |  |
| Notes |  |  |  |  |  |  |  |  |  |  |  |  |

User approved ignoring U-Turning movement.

|  | $\downarrow$ |
| :---: | :---: |
| Movement | SBR |
| Lanefonfigurations | 「 |
| Traffic Volume (veh/h) | 46 |
| Future Volume (veh/h) | 46 |
| Initial Q (Qb), veh | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 |
| Parking Bus, Adj | 1.00 |
| Work Zone On Approach |  |
| Adj Sat Flow, veh/h/ln | 1870 |
| Adj Flow Rate, veh/h | 14 |
| Peak Hour Factor | 0.92 |
| Percent Heavy Veh, \% | 2 |
| Cap, veh/h | 71 |
| Arrive On Green | 0.04 |
| Sat Flow, veh/h | 1585 |
| Grp Volume(v), veh/h | 14 |
| Grp Sat Flow(s), veh/h/ln | 1585 |
| Q Serve(g_s), s | 0.6 |
| Cycle Q Clear(g_c), s | 0.6 |
| Prop In Lane | 1.00 |
| Lane Grp Cap(c), veh/h | 71 |
| V/C Ratio(X) | 0.20 |
| Avail Cap(c_a), veh/h | 777 |
| HCM Platoon Ratio | 1.00 |
| Upstream Filter(l) | 1.00 |
| Uniform Delay (d), s/veh | 31.9 |
| Incr Delay (d2), s/veh | 0.5 |
| Initial Q Delay(d3),s/veh | 0.0 |
| \%ile BackOfQ(50\%),veh/ln | 0.5 |
| Unsig. Movement Delay, s/veh |  |
| LnGrp Delay(d),s/veh | 32.4 |
| LnGrp LOS | C |
| Approach Vol, veh/h |  |
| Approach Delay, s/veh |  |
| Approach LOS |  |
| Timer - Assigned Phs |  |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0.2 |  |  |  |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | 怍 |  | 1 | 体 |  | $\mathbf{7}$ |
| Traffic Vol, veh/h | 1464 | 23 | 18 | 1885 | 0 | 24 |
| Future Vol, veh/h | 1464 | 23 | 18 | 1885 | 0 | 24 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | 200 | - | - | 0 |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, $\%$ | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 1591 | 25 | 20 | 2049 | 0 | 26 |


| Major/Minor | Major1 | Major2 |  |  |  |  |  | Minor1 |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | :---: | :---: | :---: |
| Conflicting Flow All | 0 | 0 | 1616 | 0 | - | 808 |  |  |  |
| $\quad$ Stage 1 | - | - | - | - | - | - |  |  |  |
| $\quad$ Stage 2 | - | - | - | - | - | - |  |  |  |
| Critical Hdwy | - | - | 4.14 | - | - | 6.94 |  |  |  |
| Critical Hdwy Stg 1 | - | - | - | - | - | - |  |  |  |
| Critical Hdwy Stg 2 | - | - | - | - | - | - |  |  |  |
| Follow-up Hdwy | - | - | 2.22 | - | - | 3.32 |  |  |  |
| Pot Cap-1 Maneuver | - | - | 399 | - | 0 | 324 |  |  |  |
| $\quad$ Stage 1 | - | - | - | - | 0 | - |  |  |  |
| $\quad$ Stage 2 | - | - | - | - | 0 | - |  |  |  |
| Platoon blocked, \% | - | - |  | - |  |  |  |  |  |
| Mov Cap-1 Maneuver | - | - | 399 | - | - | 324 |  |  |  |
| Mov Cap-2 Maneuver | - | - | - | - | - | - |  |  |  |
| Stage 1 | - | - | - | - | - | - |  |  |  |
| Stage 2 | - | - | - | - | - | - |  |  |  |


| Approach | EB | WB | NB |
| :--- | ---: | :---: | :---: |
| HCM Control Delay, s | 0 | 0.1 | 17.1 |
| HCM LOS |  | C |  |


| Minor Lane/Major Mvmt | NBLn1 | EBT | EBR | WBL | WBT |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 324 | - | - | 399 | - |
| HCM Lane V/C Ratio | 0.081 | - | -0.049 | - |  |
| HCM Control Delay (s) | 17.1 | - | - | 14.5 | - |
| HCM Lane LOS | C | - | - | B | - |
| HCM 95th \%tile Q(veh) | 0.3 | - | - | 0.2 | - |




Stage 2

| Approach | EB | WB | NB | SB |
| :--- | ---: | ---: | ---: | ---: |
| HCM Control Delay, s | 0.9 | 0.2 | 14.6 | 24.5 |
| HCM LOS |  |  | B |  |


| Minor Lane/Major Mvmt | NBLn1 | EBL | EBT | EBR | WBL | WBT | WBR SBLn1 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 379 | 305 | - | - | 482 | - | - |
| HCM Lane V/C Ratio | 0.005 | 0.208 | - | -0.073 | - | -0.281 |  |
| HCM Control Delay (s) | 14.6 | 19.9 | - | - | 13.1 | - | - |
| HCM Lane LOS | B | C | - | - | B | - | - |
| HCM 95th \%tile Q(veh) | 0 | 0.8 | - | - | 0.2 | - | - |


| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | \＃ | 中\％ |  | \＃ | 44 | 「 | ${ }^{7}$ | $\uparrow$ | 「 |  | $\uparrow$ | 「 |
| Traffic Volume（veh／h） | 41 | 1188 | 131 | 134 | 1571 | 114 | 220 | 98 | 76 | 137 | 116 | 34 |
| Future Volume（veh／h） | 41 | 1188 | 131 | 134 | 1571 | 114 | 220 | 98 | 76 | 137 | 116 | 34 |
| Initial Q（Qb），veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 1.00 | 1.00 |  | 0.98 | 1.00 |  | 1.00 | 1.00 |  | 0.99 |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow，veh／h／ln | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 |
| Adj Flow Rate，veh／h | 44 | 1264 | 132 | 143 | 1671 | 76 | 169 | 195 | 0 | 146 | 123 | 7 |
| Peak Hour Factor | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 |
| Percent Heavy Veh，\％ | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| Cap，veh／h | 56 | 1365 | 142 | 175 | 1732 | 755 | 223 | 235 |  | 166 | 140 | 263 |
| Arrive On Green | 0.03 | 0.42 | 0.42 | 0.10 | 0.48 | 0.48 | 0.12 | 0.12 | 0.00 | 0.17 | 0.17 | 0.17 |
| Sat Flow，veh／h | 1795 | 3274 | 341 | 1795 | 3582 | 1562 | 1795 | 1885 | 1598 | 996 | 839 | 1576 |
| Grp Volume（v），veh／h | 44 | 689 | 707 | 143 | 1671 | 76 | 169 | 195 | 0 | 269 | 0 | 7 |
| Grp Sat Flow（s），veh／h／ln | 1795 | 1791 | 1824 | 1795 | 1791 | 1562 | 1795 | 1885 | 1598 | 1835 | 0 | 1576 |
| Q Serve（g＿s），s | 2.2 | 33.5 | 33.8 | 7.2 | 41.4 | 2.4 | 8.3 | 9.3 | 0.0 | 13.1 | 0.0 | 0.3 |
| Cycle Q Clear（g＿c），s | 2.2 | 33.5 | 33.8 | 7.2 | 41.4 | 2.4 | 8.3 | 9.3 | 0.0 | 13.1 | 0.0 | 0.3 |
| Prop In Lane | 1.00 |  | 0.19 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 0.54 |  | 1.00 |
| Lane Grp Cap（c），veh／h | 56 | 747 | 761 | 175 | 1732 | 755 | 223 | 235 |  | 306 | 0 | 263 |
| V／C Ratio（X） | 0.79 | 0.92 | 0.93 | 0.82 | 0.96 | 0.10 | 0.76 | 0.83 |  | 0.88 | 0.00 | 0.03 |
| Avail Cap（c＿a），veh／h | 294 | 781 | 796 | 392 | 1758 | 767 | 392 | 411 |  | 400 | 0 | 344 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter（I） | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 0.00 | 1.00 |
| Uniform Delay（d），s／veh | 44.1 | 25.3 | 25.4 | 40.6 | 22.9 | 12.8 | 38.8 | 39.2 | 0.0 | 37.3 | 0.0 | 32.0 |
| Incr Delay（d2），s／veh | 8.7 | 15.6 | 16.3 | 3.5 | 13.8 | 0.0 | 2.0 | 2.9 | 0.0 | 13.6 | 0.0 | 0.0 |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ（50\％），veh／ln | 1.1 | 15.4 | 15.9 | 3.1 | 18.0 | 0.8 | 3.7 | 4.3 | 0.0 | 6.9 | 0.0 | 0.1 |
| Unsig．Movement Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay（d），s／veh | 52.8 | 40.9 | 41.7 | 44.0 | 36.7 | 12.9 | 40.8 | 42.1 | 0.0 | 50.9 | 0.0 | 32.0 |
| LnGrp LOS | D | D | D | D | D | B | D | D |  | D | A | C |
| Approach Vol，veh／h |  | 1440 |  |  | 1890 |  |  | 364 | A |  | 276 |  |
| Approach Delay，s／veh |  | 41.7 |  |  | 36.3 |  |  | 41.5 |  |  | 50.4 |  |
| Approach LOS |  | D |  |  | D |  |  | D |  |  | D |  |


| Timer－Assigned Phs | 1 | 2 | 4 | 5 | 6 | 8 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Phs Duration（G＋Y＋Rc），s | 12.0 | 44.2 | 19.7 | 5.9 | 50.3 | 15.8 |
| Change Period（Y＋Rc），s | 3.0 | 6.0 | 4.4 | 3.0 | 6.0 | 4.4 |
| Max Green Setting（Gmax），s | 20.0 | 40.0 | 20.0 | 15.0 | 45.0 | 20.0 |
| Max Q Clear Time（g＿c＋11），s | 9.2 | 35.8 | 15.1 | 4.2 | 43.4 | 11.3 |
| Green Ext Time（p＿c），s | 0.0 | 1.3 | 0.2 | 0.0 | 0.9 | 0.1 |

## Intersection Summary

| HCM 6th Ctrl Delay | 39.7 |
| :--- | ---: |
| HCM 6th LOS | D |

## Notes

User approved pedestrian interval to be less than phase max green．
User approved volume balancing among the lanes for turning movement．
Unsignalized Delay for［NBR］is excluded from calculations of the approach delay and intersection delay．

## $\forall \rightarrow\rangle \vdash \leftarrow \uparrow \uparrow \uparrow>\downarrow \downarrow \downarrow$

| Movement EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | 44 | 「 | ${ }^{*}$ | 44 | 「 | ${ }^{*}$ | +4 | F | ${ }^{1}$ | 44 | F |
| Traffic Volume (veh/h) 136 | 125 | 1022 | 74 | 252 | 96 | 1175 | 341 | 42 | 80 | 612 | 259 |
| Future Volume (veh/h) 136 | 125 | 1022 | 74 | 252 | 96 | 1175 | 341 | 42 | 80 | 612 | 259 |
| Initial Q (Qb), veh 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus, Adj 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow, veh/h/ln 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 |
| Adj Flow Rate, veh/h 151 | 139 | 0 | 82 | 280 | 0 | 1306 | 379 | 0 | 89 | 680 | 0 |
| Peak Hour Factor 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Percent Heavy Veh, \% 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| Cap, veh/h 182 | 517 |  | 105 | 363 |  | 1387 | 728 |  | 384 | 766 |  |
| Arrive On Green 0.10 | 0.14 | 0.00 | 0.06 | 0.10 | 0.00 | 0.39 | 0.39 | 0.00 | 0.21 | 0.21 | 0.00 |
| Sat Flow, veh/h 1795 | 3582 | 1598 | 1795 | 3582 | 1598 | 3591 | 1885 | 1598 | 1795 | 3582 | 1598 |
| Grp Volume(v), veh/h 151 | 139 | 0 | 82 | 280 | 0 | 1306 | 379 | 0 | 89 | 680 | 0 |
| Grp Sat Flow(s),veh/h/ln1795 | 1791 | 1598 | 1795 | 1791 | 1598 | 1795 | 1885 | 1598 | 1795 | 1791 | 1598 |
| Q Serve(g_s), s 8.1 | 3.4 | 0.0 | 4.4 | 7.5 | 0.0 | 34.4 | 15.1 | 0.0 | 4.0 | 18.0 | 0.0 |
| Cycle Q Clear(g_c), s 8.1 | 3.4 | 0.0 | 4.4 | 7.5 | 0.0 | 34.4 | 15.1 | 0.0 | 4.0 | 18.0 | 0.0 |
| Prop In Lane 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Lane Grp Cap(c), veh/h 182 | 517 |  | 105 | 363 |  | 1387 | 728 |  | 384 | 766 |  |
| V/C Ratio(X) 0.83 | 0.27 |  | 0.78 | 0.77 |  | 0.94 | 0.52 |  | 0.23 | 0.89 |  |
| Avail Cap(c_a), veh/h 458 | 914 |  | 275 | 731 |  | 1650 | 866 |  | 458 | 914 |  |
| HCM Platoon Ratio 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 |
| Uniform Delay (d), s/veh 43.1 | 37.3 | 0.0 | 45.5 | 42.9 | 0.0 | 29.0 | 23.1 | 0.0 | 31.8 | 37.4 | 0.0 |
| Incr Delay (d2), s/veh 3.6 | 0.1 | 0.0 | 4.6 | 1.3 | 0.0 | 9.5 | 0.2 | 0.0 | 0.1 | 8.4 | 0.0 |
| Initial Q Delay(d3),s/veh 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile BackOfQ(50\%),veh/IB. 6 | 1.4 | 0.0 | 2.0 | 3.3 | 0.0 | 15.5 | 6.4 | 0.0 | 1.7 | 8.4 | 0.0 |
| Unsig. Movement Delay, s/veh |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay(d),s/veh 46.8 | 37.4 | 0.0 | 50.1 | 44.2 | 0.0 | 38.4 | 23.3 | 0.0 | 32.0 | 45.8 | 0.0 |
| LnGrp LOS D | D |  | D | D |  | D | C |  | C | D |  |
| Approach Vol, veh/h | 290 | A |  | 362 | A |  | 1685 | A |  | 769 | A |
| Approach Delay, s/veh | 42.3 |  |  | 45.6 |  |  | 35.0 |  |  | 44.2 |  |
| Approach LOS | D |  |  | D |  |  | D |  |  | D |  |



## Notes

User approved pedestrian interval to be less than phase max green.
User approved volume balancing among the lanes for turning movement.

* HCM 6th computational engine requires equal clearance times for the phases crossing the barrier.

Unsignalized Delay for [NBR, EBR, WBR, SBR] is excluded from calculations of the approach delay and intersection delay.
Intersection
Intersection Delay, s/veh51.4
Intersection LOS F

| Movement EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | 4 |  |  | $\uparrow$ | F |  | 4 |  |  | $\uparrow$ | 「 |
| Traffic Vol, veh/h 53 | 128 | 16 | 107 | 183 | 77 | 21 | 250 | 75 | 42 | 206 | 143 |
| Future Vol, veh/h 53 | 128 | 16 | 107 | 183 | 77 | 21 | 250 | 75 | 42 | 206 | 143 |
| Peak Hour Factor 0.80 | 0.80 | 0.80 | 0.80 | 0.80 | 0.80 | 0.80 | 0.80 | 0.80 | 0.80 | 0.80 | 0.80 |
| Heavy Vehicles, \% 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow 66 | 160 | 20 | 134 | 229 | 96 | 26 | 313 | 94 | 53 | 258 | 179 |
| Number of Lanes 0 | 1 | 0 | 0 | 1 | 1 | 0 | 1 | 0 | 0 | 1 | 1 |
| Approach EB |  |  | WB |  |  | NB |  |  | SB |  |  |
| Opposing Approach WB |  |  | EB |  |  | SB |  |  | NB |  |  |
| Opposing Lanes 2 |  |  | 1 |  |  | 2 |  |  | 1 |  |  |
| Conflicting Approach Left SB |  |  | NB |  |  | EB |  |  | WB |  |  |
| Conflicting Lanes Left 2 |  |  | 1 |  |  | 1 |  |  | 2 |  |  |
| Conflicting Approach RighNB |  |  | SB |  |  | WB |  |  | EB |  |  |
| Conflicting Lanes Right 1 |  |  | 2 |  |  | 2 |  |  | 1 |  |  |
| HCM Control Delay 30.3 |  |  | 45.3 |  |  | 95.4 |  |  | 28.9 |  |  |
| HCM LOS D |  |  | E |  |  | F |  |  | D |  |  |


| Lane | NBLn1 EBLn1WBLn1WBLn2 SBLn1 SBLn2 |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Vol Left, \% | $6 \%$ | $27 \%$ | $37 \%$ | $0 \%$ | $17 \%$ | $0 \%$ |
| Vol Thru, $\%$ | $72 \%$ | $65 \%$ | $63 \%$ | $0 \%$ | $83 \%$ | $0 \%$ |
| Vol Right, \% | $22 \%$ | $8 \%$ | $0 \%$ | $100 \%$ | $0 \%$ | $100 \%$ |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 346 | 197 | 290 | 77 | 248 | 143 |
| LT Vol | 21 | 53 | 107 | 0 | 42 | 0 |
| Through Vol | 250 | 128 | 183 | 0 | 206 | 0 |
| RT Vol | 75 | 16 | 0 | 77 | 0 | 143 |
| Lane Flow Rate | 432 | 246 | 362 | 96 | 310 | 179 |
| Geometry Grp | 6 | 6 | 7 | 7 | 7 | 7 |
| Degree of Util (X) | 1.071 | 0.654 | 0.894 | 0.214 | 0.761 | 0.4 |
| Departure Headway (Hd) | 8.916 | 10.091 | 9.288 | 8.366 | 9.241 | 8.422 |
| Convergence, Y/N | Yes | Yes | Yes | Yes | Yes | Yes |
| Cap | 411 | 360 | 392 | 432 | 394 | 431 |
| Service Time | 6.916 | 8.091 | 6.988 | 6.066 | 6.941 | 6.122 |
| HCM Lane V/C Ratio | 1.051 | 0.683 | 0.923 | 0.222 | 0.787 | 0.415 |
| HCM Control Delay | 95.4 | 30.3 | 53.8 | 13.3 | 36 | 16.6 |
| HCM Lane LOS | F | D | F | B | E | C |
| HCM 95th-tile Q | 14.7 | 4.4 | 9.1 | 0.8 | 6.2 | 1.9 |




| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | ＊＊ | 444 | 「 | ＊＊ | 444 | F | ＊＊ | 444 | 「 | ＊＊ | 衡 |  |
| Traffic Volume（veh／h） | 394 | 1589 | 281 | 319 | 1378 | 240 | 446 | 876 | 208 | 248 | 765 | 148 |
| Future Volume（veh／h） | 394 | 1589 | 281 | 319 | 1378 | 240 | 446 | 876 | 208 | 248 | 765 | 148 |
| Initial Q（Qb），veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow，veh／h／ln | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 |
| Adj Flow Rate，veh／h | 419 | 1690 | 155 | 339 | 1466 | 0 | 474 | 932 | 0 | 264 | 814 | 137 |
| Peak Hour Factor | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 |
| Percent Heavy Veh，\％ | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| Cap，veh／h | 466 | 1784 | 553 | 551 | 1979 |  | 522 | 1330 |  | 313 | 881 | 147 |
| Arrive On Green | 0.13 | 0.35 | 0.35 | 0.16 | 0.38 | 0.00 | 0.15 | 0.26 | 0.00 | 0.09 | 0.20 | 0.20 |
| Sat Flow，veh／h | 3483 | 5147 | 1596 | 3483 | 5147 | 1598 | 3483 | 5147 | 1598 | 3483 | 4439 | 742 |
| Grp Volume（v），veh／h | 419 | 1690 | 155 | 339 | 1466 | 0 | 474 | 932 | 0 | 264 | 628 | 323 |
| Grp Sat Flow（s），veh／h／ln | 1742 | 1716 | 1596 | 1742 | 1716 | 1598 | 1742 | 1716 | 1598 | 1742 | 1716 | 1750 |
| Q Serve（g＿s），s | 17.8 | 47.9 | 7.0 | 13.6 | 36.8 | 0.0 | 20.1 | 24.6 | 0.0 | 11.2 | 26.9 | 27.2 |
| Cycle Q Clear（g＿c），s | 17.8 | 47.9 | 7.0 | 13.6 | 36.8 | 0.0 | 20.1 | 24.6 | 0.0 | 11.2 | 26.9 | 27.2 |
| Prop In Lane | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 0.42 |
| Lane Grp Cap（c），veh／h | 466 | 1784 | 553 | 551 | 1979 |  | 522 | 1330 |  | 313 | 681 | 347 |
| V／C Ratio（X） | 0.90 | 0.95 | 0.28 | 0.61 | 0.74 |  | 0.91 | 0.70 |  | 0.84 | 0.92 | 0.93 |
| Avail Cap（c＿a），veh／h | 534 | 1784 | 553 | 551 | 1979 |  | 604 | 1330 |  | 488 | 686 | 350 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter（l） | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay（d），s／veh | 64.0 | 47.7 | 15.8 | 58.9 | 39.7 | 0.0 | 62.7 | 50.4 | 0.0 | 67.2 | 59.0 | 59.1 |
| Incr Delay（d2），s／veh | 15.5 | 12.0 | 1.3 | 1.5 | 2.5 | 0.0 | 15.0 | 1.8 | 0.0 | 4.5 | 18.2 | 31.1 |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ（50\％），veh／In | 8.7 | 21.8 | 4.1 | 6.0 | 15.6 | 0.0 | 9.8 | 10.6 | 0.0 | 5.1 | 13.2 | 14.8 |
| Unsig．Movement Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay（d），s／veh | 79.5 | 59.7 | 17.1 | 60.4 | 42.3 | 0.0 | 77.8 | 52.2 | 0.0 | 71.7 | 77.2 | 90.2 |
| LnGrp LOS | E | E | B | E | D |  | E | D |  | E | E | F |
| Approach Vol，veh／h |  | 2264 |  |  | 1805 | A |  | 1406 | A |  | 1215 |  |
| Approach Delay，s／veh |  | 60.4 |  |  | 45.7 |  |  | 60.8 |  |  | 79.5 |  |
| Approach LOS |  | E |  |  | D |  |  | E |  |  | E |  |


| Timer－Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Phs Duration（G＋Y＋Rc），s | 29.7 | 58.0 | 26.5 | 35.8 | 24.1 | 63.7 | 17.5 | 44.8 |
| Change Period（Y＋Rc），s | 6.0 | 6.0 | 4.0 | 6.0 | 4.0 | 6.0 | 4.0 | 6.0 |
| Max Green Setting（Gmax），s | 20.0 | 52.0 | 26.0 | 30.0 | 23.0 | 51.0 | 21.0 | 35.0 |
| Max Q Clear Time（g＿c＋I1），s | 15.6 | 49.9 | 22.1 | 29.2 | 19.8 | 38.8 | 13.2 | 26.6 |
| Green Ext Time（p＿c），s | 0.3 | 1.9 | 0.4 | 0.5 | 0.3 | 7.8 | 0.3 | 4.4 |

## Intersection Summary

| HCM 6th Ctrl Delay | 60.0 |
| :--- | ---: |
| HCM 6th LOS | E |

## Notes

User approved pedestrian interval to be less than phase max green．
Unsignalized Delay for［NBR，WBR］is excluded from calculations of the approach delay and intersection delay．

| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |



|  | $\rangle$ |  |  | 7 |  |  |  | $\uparrow$ |  |  | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \% | 中t |  | N | 蚛 |  |  |  |  |  | $\uparrow$ | F |
| Traffic Volume (veh/h) | 34 | 1912 | 0 | 0 | 1766 | 18 | 0 | 0 | 0 | 26 | 0 | 31 |
| Future Volume (veh/h) | 34 | 1912 | 0 | 0 | 1766 | 18 | 0 | 0 | 0 | 26 | 0 | 31 |
| Initial $\mathrm{Q}(\mathrm{Qb})$, veh | 0 | 0 | 0 | 0 | 0 | 0 |  |  |  | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 |  | 1.00 | 1.00 |  | 0.98 |  |  |  | 1.00 |  | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |  | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  |  |  |  | No |  |
| Adj Sat Flow, veh/h/ln | 1885 | 1885 | 1885 | 1870 | 1885 | 1885 |  |  |  | 1885 | 1870 | 1885 |
| Adj Flow Rate, veh/h | 36 | 2034 | 0 | 0 | 1879 | 19 |  |  |  | 28 | 0 | 12 |
| Peak Hour Factor | 0.94 | 0.94 | 0.92 | 0.92 | 0.94 | 0.94 |  |  |  | 0.94 | 0.92 | 0.94 |
| Percent Heavy Veh, \% | 1 | 1 | 1 | 2 | 1 | 1 |  |  |  | 1 | 2 | 1 |
| Cap, veh/h | 43 | 2701 | 0 | 3 | 2478 | 25 |  |  |  | 100 | 0 | 89 |
| Arrive On Green | 0.02 | 0.75 | 0.00 | 0.00 | 0.68 | 0.68 |  |  |  | 0.06 | 0.00 | 0.06 |
| Sat Flow, veh/h | 1795 | 3676 | 0 | 1781 | 3632 | 37 |  |  |  | 1781 | 0 | 1598 |
| Grp Volume(v), veh/h | 36 | 2034 | 0 | 0 | 925 | 973 |  |  |  | 28 | 0 | 12 |
| Grp Sat Flow(s),veh/h/ln | 1795 | 1791 | 0 | 1781 | 1791 | 1878 |  |  |  | 1781 | 0 | 1598 |
| Q Serve(g_s), s | 1.3 | 20.4 | 0.0 | 0.0 | 21.4 | 21.6 |  |  |  | 1.0 | 0.0 | 0.5 |
| Cycle Q Clear(g_c), s | 1.3 | 20.4 | 0.0 | 0.0 | 21.4 | 21.6 |  |  |  | 1.0 | 0.0 | 0.5 |
| Prop In Lane | 1.00 |  | 0.00 | 1.00 |  | 0.02 |  |  |  | 1.00 |  | 1.00 |
| Lane Grp Cap(c), veh/h | 43 | 2701 | 0 | 3 | 1222 | 1281 |  |  |  | 100 | 0 | 89 |
| V/C Ratio(X) | 0.83 | 0.75 | 0.00 | 0.00 | 0.76 | 0.76 |  |  |  | 0.28 | 0.00 | 0.13 |
| Avail Cap(c_a), veh/h | 654 | 3799 | 0 | 367 | 1900 | 1992 |  |  |  | 1889 | 0 | 1695 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |  | 1.00 | 1.00 | 1.00 |
| Upstream Filter(1) | 1.00 | 1.00 | 0.00 | 0.00 | 1.00 | 1.00 |  |  |  | 1.00 | 0.00 | 1.00 |
| Uniform Delay (d), s/veh | 30.7 | 4.4 | 0.0 | 0.0 | 6.6 | 6.6 |  |  |  | 28.6 | 0.0 | 28.4 |
| Incr Delay (d2), s/veh | 13.5 | 0.5 | 0.0 | 0.0 | 1.0 | 1.0 |  |  |  | 1.5 | 0.0 | 0.7 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |  |  | 0.0 | 0.0 | 0.0 |
| \%ile BackOfQ(50\%),veh/ln | 0.6 | 0.9 | 0.0 | 0.0 | 3.3 | 3.5 |  |  |  | 0.4 | 0.0 | 0.4 |
| Unsig. Movement Delay, s/veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay (d),s/veh | 44.2 | 5.0 | 0.0 | 0.0 | 7.6 | 7.6 |  |  |  | 30.1 | 0.0 | 29.0 |
| LnGrp LOS | D | A | A | A | A | A |  |  |  | C | A | C |
| Approach Vol, veh/h |  | 2070 |  |  | 1898 |  |  |  |  |  | 40 |  |
| Approach Delay, s/veh |  | 5.6 |  |  | 7.6 |  |  |  |  |  | 29.8 |  |
| Approach LOS |  | A |  |  | A |  |  |  |  |  | C |  |


| Timer - Assigned Phs | 1 | 2 | 4 | 5 | 6 |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Phs Duration $(G+Y+R c)$, s | 4.5 | 49.1 | 9.5 | 0.0 | 53.6 |
| Change Period $(\mathrm{Y}+\mathrm{Rc})$, s | 3.0 | 6.0 | 6.0 | 3.0 | 6.0 |
| Max Green Setting (Gmax), s | 23.0 | 67.0 | 67.0 | 13.0 | 67.0 |
| Max Q Clear Time (g_c+11), s | 3.3 | 23.6 | 3.0 | 0.0 | 22.4 |
| Green Ext Time (p_C), s | 0.0 | 19.5 | 0.2 | 0.0 | 23.7 |

## Intersection Summary

| HCM 6th Ctrl Delay | 6.8 |
| :--- | ---: |
| HCM 6th LOS | A |

Notes
User approved ignoring U-Turning movement.

| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |


| Major/Minor | Major1 | Major2 |  | Minor1 |  |
| :--- | ---: | ---: | :--- | :--- | :--- |
| Conflicting Flow All | 0 | 0 | 2095 | 0 | -1048 |
| $\quad$ Stage 1 | - | - | - | - | - |
| $\quad$ Stage 2 | - | - | - | - | - |
| Critical Hdwy | - | - | 4.14 | - | - |
| Critical Hdwy Stg 1 | - | - | - | - | - |
| Critical Hdwy Stg 2 | - | - | - | - | - |
| Follow-up Hdwy | - | - | 2.22 | - | - |
| Pot Cap-1 Maneuver | - | - | 260 | - | 0 |
| $\quad$ Stage 1 | - | - | - | - | 0 |
| $\quad$ Stage 2 | - | - | - | - | 0 |


|  | EB | WB | NB |
| :--- | ---: | ---: | ---: |
| Approach | 0.4 | 24.8 |  |
| HCM Control Delay, $s$ | 0 | 0.4 | C LOS |


| Minor Lane/Major Mvmt | NBLn1 | EBT | EBR | WBL | WBT |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Capacity (veh/h) | 224 | - | - | 260 | - |  |
| HCM Lane V/C Ratio | 0.189 | - | - | 0.138 | - |  |
| HCM Control Delay (s) | 24.8 | - | - | 21.1 | - |  |
| HCM Lane LOS | C | - | - | C | - |  |
| HCM 95th \%tile $Q$ (veh) | 0.7 | - | - | 0.5 | - |  |



| Major/Minor | Major1 |  |  | Major2 |  | Minor1 |  |  | Minor2 |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 1775 | 0 | 0 | 1958 | 0 | 0 | - | - | 979 | - | - | 888 |
| Stage 1 | - | - | - | - | - | - | - | - | - | - | - | - |
| Stage 2 | - | - | - | - | - | - | - | - | - | - | - | - |
| Critical Hdwy | 4.12 | - | - | 4.12 | - | - | - | - | 6.92 | - | - | 6.92 |
| Critical Hdwy Stg 1 | - | - | - | - | - | - | - | - | - | - | - | - |
| Critical Hdwy Stg 2 | - | - | - | - | - | - | - | - | - | - | - | - |
| Follow-up Hdwy | 2.21 | - | - | 2.21 | - | - | - | - | 3.31 | - | - | 3.31 |
| Pot Cap-1 Maneuver | 351 | - | - | 298 | - | - | 0 | 0 | 251 | 0 | 0 | 289 |
| Stage 1 | - | - | - | - | - | - | 0 | 0 | - | 0 | 0 | - |
| Stage 2 | - | - | - | - | - | - | 0 | 0 | - | 0 | 0 | - |
| Platoon blocked, \% |  | - | - |  | - | - |  |  |  |  |  |  |
| Mov Cap-1 Maneuver | 351 | - | - | 298 | - | - | - | - | 251 | - | - | 289 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | - | - | - | - | - | - |
| Stage 1 | - | - | - | - | - | - | - | - | - | - | - | - | Stage 2


| Approach | EB | WB | NB | SB |
| :--- | :---: | :---: | :---: | :---: |
| HCM Control Delay, s | 0.7 | 0.4 | 20 | 25 |
| HCM LOS |  | C | D |  |


| Minor Lane/Major Mvmt | NBLn1 | EBL | EBT | EBR | WBL | WBT | WBR SBLn1 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 251 | 351 | - | - | 298 | - | - |
| HCM Lane V/C Ratio | 0.046 | 0.225 | - | -0.141 | - | -0.382 |  |
| HCM Control Delay (s) | 20 | 18.2 | - | -19.1 | - | - | 25 |
| HCM Lane LOS | C | C | - | - | C | - | - |
| HCM 95th \%tile Q(veh) | 0.1 | 0.8 | - | - | 0.5 | - | - |


| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | $\stackrel{y}{4}$ | 个 ${ }^{\text {a }}$ |  | ＊ | 个4 | F | ${ }^{*}$ | $\uparrow$ | 「 |  | $\uparrow$ | F |
| Traffic Volume（veh／h） | 45 | 1579 | 207 | 92 | 1505 | 165 | 134 | 75 | 102 | 147 | 90 | 56 |
| Future Volume（veh／h） | 45 | 1579 | 207 | 92 | 1505 | 165 | 134 | 75 | 102 | 147 | 90 | 56 |
| Initial $Q(Q b)$ ，veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 0.98 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow，veh／h／ln | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Adj Flow Rate，veh／h | 46 | 1628 | 206 | 95 | 1552 | 128 | 108 | 120 | 0 | 152 | 93 | 13 |
| Peak Hour Factor | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 |
| Percent Heavy Veh，\％ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Cap，veh／h | 58 | 1541 | 191 | 122 | 1853 | 826 | 156 | 164 |  | 178 | 109 | 250 |
| Arrive On Green | 0.03 | 0.48 | 0.48 | 0.07 | 0.51 | 0.51 | 0.09 | 0.09 | 0.00 | 0.16 | 0.16 | 0.16 |
| Sat Flow，veh／h | 1810 | 3223 | 400 | 1810 | 3610 | 1609 | 1810 | 1900 | 1610 | 1143 | 700 | 1610 |
| Grp Volume（v），veh／h | 46 | 898 | 936 | 95 | 1552 | 128 | 108 | 120 | 0 | 245 | 0 | 13 |
| Grp Sat Flow（s），veh／h／ln | 1810 | 1805 | 1818 | 1810 | 1805 | 1609 | 1810 | 1900 | 1610 | 1843 | 0 | 1610 |
| Q Serve（g＿s），s | 2.1 | 40.0 | 40.0 | 4.3 | 30.7 | 3.5 | 4.9 | 5.2 | 0.0 | 10.8 | 0.0 | 0.6 |
| Cycle Q Clear（g＿c），s | 2.1 | 40.0 | 40.0 | 4.3 | 30.7 | 3.5 | 4.9 | 5.2 | 0.0 | 10.8 | 0.0 | 0.6 |
| Prop In Lane | 1.00 |  | 0.22 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 0.62 |  | 1.00 |
| Lane Grp Cap（c），veh／h | 58 | 863 | 869 | 122 | 1853 | 826 | 156 | 164 |  | 286 | 0 | 250 |
| V／C Ratio（X） | 0.79 | 1.04 | 1.08 | 0.78 | 0.84 | 0.16 | 0.69 | 0.73 |  | 0.86 | 0.00 | 0.05 |
| Avail Cap（c＿a），veh／h | 324 | 863 | 869 | 433 | 1942 | 865 | 433 | 454 |  | 441 | 0 | 385 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter（1） | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 0.00 | 1.00 |
| Uniform Delay（d），s／veh | 40.2 | 21.8 | 21.8 | 38.4 | 17.4 | 10.8 | 37.1 | 37.3 | 0.0 | 34.4 | 0.0 | 30.1 |
| Incr Delay（d2），s／veh | 8.3 | 41.6 | 53.4 | 4.0 | 3.0 | 0.0 | 2.0 | 2.4 | 0.0 | 6.2 | 0.0 | 0.0 |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \％oile BackOfQ（50\％），veh／ln | 1.0 | 23.4 | 26.4 | 1.9 | 11.0 | 1.1 | 2.1 | 2.4 | 0.0 | 5.2 | 0.0 | 0.2 |
| Unsig．Movement Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay（d），s／veh | 48.5 | 63.5 | 75.2 | 42.4 | 20.4 | 10.8 | 39.2 | 39.6 | 0.0 | 40.6 | 0.0 | 30.1 |
| LnGrp LOS | D | F | F | D | C | B | D | D |  | D | A | C |
| Approach Vol，veh／h |  | 1880 |  |  | 1775 |  |  | 228 | A |  | 258 |  |
| Approach Delay，s／veh |  | 68.9 |  |  | 20.9 |  |  | 39.4 |  |  | 40.1 |  |
| Approach LOS |  | E |  |  | C |  |  | D |  |  | D |  |


| Timer－Assigned Phs | 1 | 2 | 4 | 5 | 6 | 8 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Phs Duration $(G+Y+R c)$ ，s | 8.6 | 46.0 | 17.4 | 5.7 | 48.9 | 11.6 |
| Change Period（Y＋Rc），s | 3.0 | 6.0 | 4.4 | 3.0 | 6.0 | 4.4 |
| Max Green Setting（Gmax），s | 20.0 | 40.0 | 20.0 | 15.0 | 45.0 | 20.0 |
| Max Q Clear Time（g＿c＋1），s | 6.3 | 42.0 | 12.8 | 4.1 | 32.7 | 7.2 |
| Green Ext Time（p＿C），s | 0.0 | 0.0 | 0.2 | 0.0 | 3.5 | 0.1 |

## Intersection Summary

| HCM 6th Ctrl Delay | 44.9 |
| :--- | ---: |
| HCM 6th LOS | $D$ |

## Notes

User approved pedestrian interval to be less than phase max green．
User approved volume balancing among the lanes for turning movement．
Unsignalized Delay for［NBR］is excluded from calculations of the approach delay and intersection delay．

## $\Rightarrow \rightarrow\rangle \vdash \leftarrow \uparrow \uparrow \uparrow \downarrow \downarrow \downarrow \downarrow$

| Movement EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | 44 | 「 | ${ }^{1}$ | 种 | 「 | ${ }^{7}$ | ＊ 4 | 「 | ${ }^{1 /}$ | 中4 | 「 |
| Traffic Volume（veh／h） 211 | 271 | 1113 | 57 | 235 | 98 | 1177 | 689 | 80 | 111 | 440 | 201 |
| Future Volume（veh／h） 211 | 271 | 1113 | 57 | 235 | 98 | 1177 | 689 | 80 | 111 | 440 | 201 |
| Initial Q（Qb），veh 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus，Adj $\quad 1.00$ | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow，veh／h／ln 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 |
| Adj Flow Rate，veh／h 220 | 282 | 0 | 59 | 245 | 0 | 1226 | 718 | 0 | 116 | 458 | 0 |
| Peak Hour Factor 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 |
| Percent Heavy Veh，\％ 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| Cap，veh／h 253 | 693 |  | 76 | 339 |  | 1461 | 767 |  | 277 | 553 |  |
| Arrive On Green 0.14 | 0.19 | 0.00 | 0.04 | 0.09 | 0.00 | 0.41 | 0.41 | 0.00 | 0.15 | 0.15 | 0.00 |
| Sat Flow，veh／h 1795 | 3582 | 1598 | 1795 | 3582 | 1598 | 3591 | 1885 | 1598 | 1795 | 3582 | 1598 |
| Grp Volume（v），veh／h 220 | 282 | 0 | 59 | 245 | 0 | 1226 | 718 | 0 | 116 | 458 | 0 |
| Grp Sat Flow（s），veh／h／ln1795 | 1791 | 1598 | 1795 | 1791 | 1598 | 1795 | 1885 | 1598 | 1795 | 1791 | 1598 |
| Q Serve（g＿s），s 11.4 | 6.6 | 0.0 | 3.1 | 6.3 | 0.0 | 29.3 | 34.7 | 0.0 | 5.6 | 11.8 | 0.0 |
| Cycle Q Clear（g＿c），s 11.4 | 6.6 | 0.0 | 3.1 | 6.3 | 0.0 | 29.3 | 34.7 | 0.0 | 5.6 | 11.8 | 0.0 |
| Prop In Lane 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Lane Grp Cap（c），veh／h 253 | 693 |  | 76 | 339 |  | 1461 | 767 |  | 277 | 553 |  |
| V／C Ratio（X） 0.87 | 0.41 |  | 0.78 | 0.72 |  | 0.84 | 0.94 |  | 0.42 | 0.83 |  |
| Avail Cap（c＿a），veh／h 471 | 940 |  | 283 | 752 |  | 1696 | 891 |  | 471 | 940 |  |
| HCM Platoon Ratio 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter（I）$\quad 1.00$ | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 |
| Uniform Delay（d），s／veh 40.0 | 33.6 | 0.0 | 45.2 | 41.9 | 0.0 | 25.4 | 27.0 | 0.0 | 36.4 | 39.0 | 0.0 |
| Incr Delay（d2），s／veh 3.5 | 0.1 | 0.0 | 6.2 | 1.1 | 0.0 | 3.0 | 14.6 | 0.0 | 0.4 | 1.2 | 0.0 |
| Initial Q Delay（d3），s／veh 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ（50\％），veh／lı5．0 | 2.7 | 0.0 | 1.5 | 2.8 | 0.0 | 12.1 | 17.4 | 0.0 | 2.4 | 5.0 | 0.0 |
| Unsig．Movement Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay（d），s／veh 43.6 | 33.8 | 0.0 | 51.3 | 43.0 | 0.0 | 28.4 | 41.7 | 0.0 | 36.8 | 40.3 | 0.0 |
| LnGrp LOS D | C |  | D | D |  | C | D |  | D | D |  |
| Approach Vol，veh／h | 502 | A |  | 304 | A |  | 1944 | A |  | 574 | A |
| Approach Delay，s／veh | 38.1 |  |  | 44.6 |  |  | 33.3 |  |  | 39.6 |  |
| Approach LOS | D |  |  | D |  |  | C |  |  | D |  |



## Notes

User approved pedestrian interval to be less than phase max green．
User approved volume balancing among the lanes for turning movement．
＊HCM 6th computational engine requires equal clearance times for the phases crossing the barrier．

Unsignalized Delay for [NBR, EBR, WBR, SBR] is excluded from calculations of the approach delay and intersection delay.


| Movement EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | \$ |  |  | $\uparrow$ | F |  | \& |  |  | $\uparrow$ | 「 |
| Traffic Vol, veh/h 44 | 217 | 48 | 38 | 118 | 51 | 18 | 181 | 28 | 97 | 249 | 42 |
| Future Vol, veh/h 44 | 217 | 48 | 38 | 118 | 51 | 18 | 181 | 28 | 97 | 249 | 42 |
| Peak Hour Factor 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 |
| Heavy Vehicles, \% 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Mvmt Flow 48 | 238 | 53 | 42 | 130 | 56 | 20 | 199 | 31 | 107 | 274 | 46 |
| Number of Lanes 0 | 1 | 0 | 0 | 1 | 1 | 0 | 1 | 0 | 0 | 1 | 1 |
| Approach EB |  |  | WB |  |  | NB |  |  | SB |  |  |
| Opposing Approach WB |  |  | EB |  |  | SB |  |  | NB |  |  |
| Opposing Lanes 2 |  |  | 1 |  |  | 2 |  |  | 1 |  |  |
| Conflicting Approach Left SB |  |  | NB |  |  | EB |  |  | WB |  |  |
| Conflicting Lanes Left 2 |  |  | 1 |  |  | 1 |  |  | 2 |  |  |
| Conflicting Approach RighNB |  |  | SB |  |  | WB |  |  | EB |  |  |
| Conflicting Lanes Right 1 |  |  | 2 |  |  | 2 |  |  | 1 |  |  |
| HCM Control Delay 27.9 |  |  | 14.7 |  |  | 19.8 |  |  | 30.7 |  |  |
| HCM LOS D |  |  | B |  |  | C |  |  | D |  |  |


| Lane | NBLn1 EBLn1WBLn1WBLn2 SBLn1 SBLn2 |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Vol Left, \% | $8 \%$ | $14 \%$ | $24 \%$ | $0 \%$ | $28 \%$ | $0 \%$ |
| Vol Thru, $\%$ | $80 \%$ | $70 \%$ | $76 \%$ | $0 \%$ | $72 \%$ | $0 \%$ |
| Vol Right, \% | $12 \%$ | $16 \%$ | $0 \%$ | $100 \%$ | $0 \%$ | $100 \%$ |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 227 | 309 | 156 | 51 | 346 | 42 |
| LT Vol | 18 | 44 | 38 | 0 | 97 | 0 |
| Through Vol | 181 | 217 | 118 | 0 | 249 | 0 |
| RT Vol | 28 | 48 | 0 | 51 | 0 | 42 |
| Lane Flow Rate | 249 | 340 | 171 | 56 | 380 | 46 |
| Geometry Grp | 6 | 6 | 7 | 7 | 7 | 7 |
| Degree of Util (X) | 0.542 | 0.719 | 0.385 | 0.113 | 0.792 | 0.085 |
| Departure Headway (Hd) | 7.824 | 7.618 | 8.095 | 7.246 | 7.498 | 6.635 |
| Convergence, Y/N | Yes | Yes | Yes | Yes | Yes | Yes |
| Cap | 461 | 475 | 444 | 494 | 483 | 541 |
| Service Time | 5.885 | 5.641 | 5.853 | 5.004 | 5.223 | 4.36 |
| HCM Lane V/C Ratio | 0.54 | 0.716 | 0.385 | 0.113 | 0.787 | 0.085 |
| HCM Control Delay | 19.8 | 27.9 | 15.9 | 10.9 | 33.2 | 10 |
| HCM Lane LOS | C | D | C | B | D | A |
| HCM 95th-tile Q | 3.2 | 5.7 | 1.8 | 0.4 | 7.2 | 0.3 |




HCM 6th Signalized Intersection Summary
1：Sierra College Blvd \＆Douglas Blvd

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | ${ }^{*}$ | 444 | 「 | ${ }^{*}$ | 444 | 「 | ${ }^{*}$ | 4革4 | 「 | ＊＊ | 虫的 |  |
| Traffic Volume（veh／h） | 184 | 1156 | 172 | 245 | 1850 | 119 | 438 | 824 | 152 | 215 | 588 | 180 |
| Future Volume（veh／h） | 184 | 1156 | 172 | 245 | 1850 | 119 | 438 | 824 | 152 | 215 | 588 | 180 |
| Initial Q（Qb），veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 0.99 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 0.99 |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow，veh／h／ln | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 |
| Adj Flow Rate，veh／h | 200 | 1257 | 60 | 266 | 2011 | 0 | 476 | 896 | 0 | 234 | 639 | 148 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh，\％ | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap，veh／h | 259 | 1659 | 508 | 522 | 2134 |  | 534 | 1302 |  | 296 | 773 | 176 |
| Arrive On Green | 0.07 | 0.32 | 0.32 | 0.15 | 0.42 | 0.00 | 0.15 | 0.25 | 0.00 | 0.09 | 0.19 | 0.19 |
| Sat Flow，veh／h | 3456 | 5106 | 1564 | 3456 | 5106 | 1585 | 3456 | 5106 | 1585 | 3456 | 4151 | 946 |
| Grp Volume（v），veh／h | 200 | 1257 | 60 | 266 | 2011 | 0 | 476 | 896 | 0 | 234 | 522 | 265 |
| Grp Sat Flow（s），veh／h／ln | 1728 | 1702 | 1564 | 1728 | 1702 | 1585 | 1728 | 1702 | 1585 | 1728 | 1702 | 1693 |
| Q Serve（g＿s），s | 6.8 | 26.5 | 2.1 | 8.5 | 45.4 | 0.0 | 16.2 | 19.0 | 0.0 | 8.0 | 17.7 | 18.1 |
| Cycle Q Clear（g＿c），s | 6.8 | 26.5 | 2.1 | 8.5 | 45.4 | 0.0 | 16.2 | 19.0 | 0.0 | 8.0 | 17.7 | 18.1 |
| Prop In Lane | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 0.56 |
| Lane Grp Cap（c），veh／h | 259 | 1659 | 508 | 522 | 2134 |  | 534 | 1302 |  | 296 | 634 | 315 |
| V／C Ratio（X） | 0.77 | 0.76 | 0.12 | 0.51 | 0.94 |  | 0.89 | 0.69 |  | 0.79 | 0.82 | 0.84 |
| Avail Cap（c＿a），veh／h | 461 | 1659 | 508 | 522 | 2134 |  | 605 | 1302 |  | 605 | 681 | 339 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter（I） | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay（d），s／veh | 54.5 | 36.3 | 11.9 | 46.8 | 33.5 | 0.0 | 49.8 | 40.4 | 0.0 | 53.8 | 46.9 | 47.1 |
| Incr Delay（d2），s／veh | 1.9 | 3.3 | 0.5 | 0.3 | 9.3 | 0.0 | 13.3 | 1.7 | 0.0 | 1.8 | 8.2 | 17.1 |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ（50\％），veh／ln | 3.0 | 11.0 | 1.2 | 3.6 | 19.4 | 0.0 | 7.8 | 7.9 | 0.0 | 3.5 | 8.0 | 8.9 |
| Unsig．Movement Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay（d），s／veh | 56.3 | 39.6 | 12.4 | 47.2 | 42.8 | 0.0 | 63.1 | 42.1 | 0.0 | 55.6 | 55.2 | 64.3 |
| LnGrp LOS | E | D | B | D | D |  | E | D |  | E | E | E |
| Approach Vol，veh／h |  | 1517 |  |  | 2277 | A |  | 1372 | A |  | 1021 |  |
| Approach Delay，s／veh |  | 40.7 |  |  | 43.4 |  |  | 49.4 |  |  | 57.6 |  |
| Approach LOS |  | D |  |  | D |  |  | D |  |  | E |  |


| Timer－Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Phs Duration（G＋Y＋Rc），s | 24.1 | 45.0 | 22.5 | 28.3 | 13.0 | 56.1 | 14.3 | 36.6 |
| Change Period（Y＋Rc），s | 6.0 | 6.0 | 4.0 | 6.0 | 4.0 | 6.0 | 4.0 | 6.0 |
| Max Green Setting（Gmax），s | 14.0 | 39.0 | 21.0 | 24.0 | 16.0 | 39.0 | 21.0 | 24.0 |
| Max Q Clear Time（g＿c＋I1），s | 10.5 | 28.5 | 18.2 | 20.1 | 8.8 | 47.4 | 10.0 | 21.0 |
| Green Ext Time（p＿c），s | 0.2 | 7.2 | 0.3 | 2.1 | 0.2 | 0.0 | 0.3 | 1.8 |

Intersection Summary

| HCM 6th Ctrl Delay | 46.4 |
| :--- | ---: |
| HCM 6th LOS | D |

## Notes

User approved pedestrian interval to be less than phase max green．
Unsignalized Delay for［NBR，WBR］is excluded from calculations of the approach delay and intersection delay．

| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \＃ | 44 | T | \＃ | 性 |  |  | $\uparrow$ | 「 |  | $\uparrow$ | 「 |
| Traffic Vol，veh／h | 39 | 1494 | 40 | 51 | 1982 | 7 | 7 | 0 | 68 | 0 | 1 | 99 |
| Future Vol，veh／h | 39 | 1494 | 40 | 51 | 1982 | 7 | 7 | 0 | 68 | 0 | 1 | 99 |
| Conflicting Peds，\＃／hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | － | － | None | － | － | None | － | － | None | － | － | None |
| Storage Length | 150 | － | 100 | 175 | － | － | － | － | 125 | － | － | 25 |
| Veh in Median Storage，\＃ | － | 0 | － | － | 0 | － | － | 0 | － | － | 0 | － |
| Grade，\％ | － | 0 | － | － | 0 | － | － | 0 | － | － | 0 | － |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles，\％ | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 42 | 1624 | 43 | 55 | 2154 | 8 | 8 | 0 | 74 | 0 | 1 | 108 |



HCM 6th Signalized Intersection Summary
3: Douglas Blvd \& Seeno Ave
0. 05/25/2018


## Notes

User approved ignoring U-Turning movement.

| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |


| Major/Minor | Major1 |  | Major2 | Minor1 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 0 | 0 | 1741 | 0 |  | 871 |
| Stage 1 |  |  |  | - |  |  |
| Stage 2 |  | - |  | - |  |  |
| Critical Hdwy |  |  | 4.14 | - |  | 6.94 |
| Critical Hdwy Stg 1 | - | - | - | - |  |  |
| Critical Hdwy Stg 2 | - | - | - | - |  |  |
| Follow-up Hdwy | - | - | 2.22 | - | - | 3.32 |
| Pot Cap-1 Maneuver | - | - | 357 | - | 0 | 294 |
| Stage 1 |  | - |  | - | 0 |  |
| Stage 2 |  | - |  | - | 0 |  |
| Platoon blocked, \% |  | - |  | - |  |  |
| Mov Cap-1 Maneuver |  |  | 357 | - |  | 294 |
| Mov Cap-2 Maneuver | - | - | - | - | - |  |
| Stage 1 |  | - |  | - | - |  |
| Stage 2 | - | - | - | - | - |  |


|  | EB | WB | NB |
| :--- | :---: | :---: | :---: |
| Approach | 0.6 | 22.8 |  |
| HCM Control Delay, s | 0 | 0.6 | C |


| Minor Lane/Major Mvmt | NBLn1 | EBT | EBR | WBL | WBT |
| :--- | ---: | ---: | ---: | ---: | :--- |
| Capacity (veh/h) | 294 | - | -357 | - |  |
| HCM Lane V/C Ratio | 0.314 | - | -0.222 | - |  |
| HCM Control Delay (s) | 22.8 | - | -17.9 | - |  |
| HCM Lane LOS | C | - | - | C | - |
| HCM 95th \%tile Q(veh) | 1.3 | - | - | 0.8 | - |


| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 1.6 |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \% | 个t |  | \% | 性 |  |  |  | F |  |  | F |
| Traffic Vol, veh/h | 105 | 1448 | 14 | 70 | 1954 | 15 | 0 | 0 | 2 | 0 | 0 | 76 |
| Future Vol, veh/h | 105 | 1448 | 14 | 70 | 1954 | 15 | 0 | 0 | 2 | 0 | 0 | 76 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | None | - |  | None |
| Storage Length | 250 | - | - | 325 | - | - | - | - | 0 | - | - | 0 |
| Veh in Median Storage, \# | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 96 | 96 | 96 | 96 | 96 | 96 | 96 | 96 | 96 | 96 | 96 | 96 |
| Heavy Vehicles, \% | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| Mumt Flow | 109 | 1508 | 15 | 73 | 2035 | 16 | 0 | 0 | 2 | 0 | 0 | 79 |



Stage 2

| Approach | EB | WB | NB | SB |
| :--- | :--- | :---: | :---: | :---: |
| HCM Control Delay, s | 1.8 | 0.5 | 15.3 | 28.1 |
| HCM LOS |  |  | $C$ | D |


| Minor Lane/Major Mvmt | NBLn1 | EBL | EBT | EBR | WBL | WBT | WBR SBLn1 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 350 | 274 | - | -439 | - | -234 |  |
| HCM Lane V/C Ratio | 0.006 | 0.399 | - | -0.166 | - | -0.338 |  |
| HCM Control Delay (s) | 15.3 | 26.6 | - | - | 14.8 | - | -28.1 |
| HCM Lane LOS | C | D | - | - | $B$ | - | - |
| HCM 95th \%tile Q(veh) | 0 | 1.8 | - | - | 0.6 | - | -1.4 |

HCM 6th Signalized Intersection Summary
6：Barton Rd \＆Douglas Blvd
6．Bart 05／25／2018

|  | 4 | $\rightarrow$ | 7 | $\dagger$ | 4 |  | 4 | $\uparrow$ | $p$ |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 幺 | 个t |  | \％ | 4 4 | F | 7 | $\uparrow$ | 「 |  | $\uparrow$ | F |
| Traffic Volume（veh／h） | 47 | 1227 | 140 | 143 | 1673 | 122 | 247 | 102 | 80 | 149 | 122 | 46 |
| Future Volume（veh／h） | 47 | 1227 | 140 | 143 | 1673 | 122 | 247 | 102 | 80 | 149 | 122 | 46 |
| Initial Q（Qb），veh | － | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 1.00 | 1.00 |  | 0.98 | 1.00 |  | 1.00 | 1.00 |  | 0.99 |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow，veh／h／ln | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 |
| Adj Flow Rate，veh／h | 50 | 1305 | 142 | 152 | 1780 | 85 | 186 | 217 | 0 | 159 | 130 | 20 |
| Peak Hour Factor | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 |
| Percent Heavy Veh，\％ | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| Cap，veh／h | 64 | 1326 | 144 | 183 | 1694 | 739 | 241 | 254 |  | 177 | 145 | 277 |
| Arrive On Green | 0.04 | 0.41 | 0.41 | 0.10 | 0.47 | 0.47 | 0.13 | 0.13 | 0.00 | 0.18 | 0.18 | 0.18 |
| Sat Flow，veh／h | 1795 | 3259 | 353 | 1795 | 3582 | 1562 | 1795 | 1885 | 1598 | 1009 | 825 | 1576 |
| Grp Volume（v），veh／h | 50 | 714 | 733 | 152 | 1780 | 85 | 186 | 217 | 0 | 289 | 0 | 20 |
| Grp Sat Flow（s），veh／h／ln | 1795 | 1791 | 1822 | 1795 | 1791 | 1562 | 1795 | 1885 | 1598 | 1835 | 0 | 1576 |
| Q Serve（g＿s），s | 2.7 | 38.7 | 39.3 | 8.2 | 46.5 | 3.0 | 9.8 | 11.1 | 0.0 | 15.2 | 0.0 | 1.0 |
| Cycle Q Clear（g＿c），s | 2.7 | 38.7 | 39.3 | 8.2 | 46.5 | 3.0 | 9.8 | 11.1 | 0.0 | 15.2 | 0.0 | 1.0 |
| Prop In Lane | 1.00 |  | 0.19 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 0.55 |  | 1.00 |
| Lane Grp Cap（c），veh／h | 64 | 728 | 741 | 183 | 1694 | 739 | 241 | 254 |  | 322 | 0 | 277 |
| V／C Ratio（X） | 0.78 | 0.98 | 0.99 | 0.83 | 1.05 | 0.12 | 0.77 | 0.86 |  | 0.90 | 0.00 | 0.07 |
| Avail Cap（c＿a），veh／h | 274 | 728 | 741 | 365 | 1694 | 739 | 365 | 383 |  | 373 | 0 | 321 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter（l） | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 0.00 | 1.00 |
| Uniform Delay（d），s／veh | 47.0 | 28.8 | 29.0 | 43.3 | 25.9 | 14.4 | 41.1 | 41.6 | 0.0 | 39.7 | 0.0 | 33.8 |
| Incr Delay（d2），s／veh | 7.3 | 28.4 | 30.1 | 3.6 | 36.5 | 0.0 | 2.4 | 7.6 | 0.0 | 19.8 | 0.0 | 0.0 |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ（50\％），veh／In | 1.3 | 20.3 | 21.1 | 3.6 | 25.7 | 1.0 | 4.4 | 5.5 | 0.0 | 8.4 | 0.0 | 0.4 |
| Unsig．Movement Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay（d），s／veh | 54.4 | 57.2 | 59.1 | 47.0 | 62.4 | 14.5 | 43.5 | 49.2 | 0.0 | 59.5 | 0.0 | 33.9 |
| LnGrp LOS | D | E | E | D | F | B | D | D |  | E | A | C |
| Approach Vol，veh／h |  | 1497 |  |  | 2017 |  |  | 403 | A |  | 309 |  |
| Approach Delay，s／veh |  | 58.0 |  |  | 59.2 |  |  | 46.6 |  |  | 57.8 |  |
| Approach LOS |  | E |  |  | E |  |  | D |  |  | E |  |


| Timer－Assigned Phs | 1 | 2 | 4 | 5 | 6 | 8 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Phs Duration（G＋Y＋Rc），s | 13.0 | 46.0 | 21.7 | 6.5 | 52.5 | 17.6 |
| Change Period $(\mathrm{Y}+\mathrm{Rc})$ ，s | 3.0 | 6.0 | 4.4 | 3.0 | 6.0 | 4.4 |
| Max Green Setting（Gmax），s | 20.0 | 40.0 | 20.0 | 15.0 | 45.0 | 20.0 |
| Max Q Clear Time（g＿c＋11），s | 10.2 | 41.3 | 17.2 | 4.7 | 48.5 | 13.1 |
| Green Ext Time（p＿c），s | 0.0 | 0.0 | 0.1 | 0.0 | 0.0 | 0.2 |

## Intersection Summary

| HCM 6th Ctrl Delay | 57.5 |
| :--- | ---: |
| HCM 6th LOS | $E$ |

## Notes

User approved pedestrian interval to be less than phase max green．
User approved volume balancing among the lanes for turning movement．
Unsignalized Delay for［NBR］is excluded from calculations of the approach delay and intersection delay．

## $\Rightarrow \rightarrow\rangle \vdash \leftarrow \uparrow \uparrow \uparrow \downarrow \downarrow \downarrow \downarrow$

| Movement EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations \％ | 个个 | 「 | ＊ | 个4 | 「 | \％ | ¢个 | F＇ | ${ }_{1}$ | 个4 | 「 |
| Traffic Volume（veh／h） 148 | 147 | 1037 | 80 | 314 | 99 | 1203 | 347 | 45 | 81 | 620 | 285 |
| Future Volume（veh／h） 148 | 147 | 1037 | 80 | 314 | 99 | 1203 | 347 | 45 | 81 | 620 | 285 |
| Initial Q（Qb），veh 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus，Adj 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow，veh／h／ln 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 |
| Adj Flow Rate，veh／h 164 | 163 | 0 | 89 | 349 | 0 | 1337 | 386 | 0 | 90 | 689 | 0 |
| Peak Hour Factor 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Percent Heavy Veh，\％ | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| Cap，veh／h 193 | 583 |  | 113 | 422 |  | 1397 | 733 |  | 378 | 755 |  |
| Arrive On Green 0.11 | 0.16 | 0.00 | 0.06 | 0.12 | 0.00 | 0.39 | 0.39 | 0.00 | 0.21 | 0.21 | 0.00 |
| Sat Flow，veh／h 1795 | 3582 | 1598 | 1795 | 3582 | 1598 | 3591 | 1885 | 1598 | 1795 | 3582 | 1598 |
| Grp Volume（v），veh／h 164 | 163 | 0 | 89 | 349 | 0 | 1337 | 386 | 0 | 90 | 689 | 0 |
| Grp Sat Flow（s），veh／h／ln1795 | 1791 | 1598 | 1795 | 1791 | 1598 | 1795 | 1885 | 1598 | 1795 | 1791 | 1598 |
| Q Serve（g＿s），s 9.9 | 4.4 | 0.0 | 5.4 | 10.5 | 0.0 | 40.0 | 17.4 | 0.0 | 4.6 | 20.7 | 0.0 |
| Cycle Q Clear（g＿c），s 9.9 | 4.4 | 0.0 | 5.4 | 10.5 | 0.0 | 40.0 | 17.4 | 0.0 | 4.6 | 20.7 | 0.0 |
| Prop In Lane 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Lane Grp Cap（c），veh／h 193 | 583 |  | 113 | 422 |  | 1397 | 733 |  | 378 | 755 |  |
| V／C Ratio（X） 0.85 | 0.28 |  | 0.79 | 0.83 |  | 0.96 | 0.53 |  | 0.24 | 0.91 |  |
| Avail Cap（c＿a），veh／h 407 | 812 |  | 244 | 649 |  | 1465 | 769 |  | 407 | 812 |  |
| HCM Platoon Ratio 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter（I） 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 |
| Uniform Delay（d），s／veh 48.4 | 40.5 | 0.0 | 51.0 | 47.6 | 0.0 | 32.8 | 25.9 | 0.0 | 36.2 | 42.6 | 0.0 |
| Incr Delay（d2），s／veh 4.0 | 0.1 | 0.0 | 4.6 | 2.9 | 0.0 | 14.0 | 0.2 | 0.0 | 0.1 | 13.4 | 0.0 |
| Initial Q Delay（d3），s／veh 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ（50\％），veh／／19．5 | 1.9 | 0.0 | 2.5 | 4.8 | 0.0 | 19.1 | 7.5 | 0.0 | 2.0 | 10.2 | 0.0 |
| Unsig．Movement Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay（d），s／veh 52.3 | 40.6 | 0.0 | 55.6 | 50.5 | 0.0 | 46.8 | 26.1 | 0.0 | 36.3 | 56.0 | 0.0 |
| LnGrp LOS D | D |  | E | D |  | D | C |  | D | E |  |
| Approach Vol，veh／h | 327 | A |  | 438 | A |  | 1723 | A |  | 779 | A |
| Approach Delay，s／veh | 46.5 |  |  | 51.5 |  |  | 42.2 |  |  | 53.7 |  |
| Approach LOS | D |  |  | D |  |  | D |  |  | D |  |


| Phs 1 | 2 | 4 | 5 | 6 | 8 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Phs Duration（ $\mathrm{G}+\mathrm{Y}+\mathrm{RC}$ ）， 59.9 | 23.6 | 28.5 | 14.9 | 18.7 | 48.2 |
| Change Period（ $Y+R \mathrm{Cc}$ ，s 3.0 | 5.7 | 5.3 | 3.0 | ＊5．7 | 5.3 |
| Max Green Setting（Gmak5，${ }^{\text {c }}$ | 25.0 | 25.0 | 25.0 | ＊ 20 | 45.0 |
| Max Q Clear Time（g＿c $+117, \mathbf{L s}^{\text {c }}$ | 6.4 | 22.7 | 11.9 | 12.5 | 42.0 |
| Green Ext Time（p＿c），s 0.0 | 0.3 | 0.5 | 0.0 | 0.5 | 0.9 |
| Intersection Summary |  |  |  |  |  |
| HCM 6th Ctrr Delay | 46.6 |  |  |  |  |
| HCM 6th LOS D |  |  |  |  |  |

## Notes

User approved pedestrian interval to be less than phase max green．
User approved volume balancing among the lanes for turning movement．
＊HCM 6th computational engine requires equal clearance times for the phases crossing the barrier．

Unsignalized Delay for [NBR, EBR, WBR, SBR] is excluded from calculations of the approach delay and intersection delay.


Intersection Delay, s/veh73.4
Intersection LOS
F

| Movement EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | \$ |  |  | $\uparrow$ | 「 |  | ¢ |  |  | $\uparrow$ | 「 |
| Traffic Vol, veh/h 60 | 137 | 19 | 113 | 192 | 83 | 23 | 273 | 77 | 45 | 221 | 148 |
| Future Vol, veh/h 60 | 137 | 19 | 113 | 192 | 83 | 23 | 273 | 77 | 45 | 221 | 148 |
| Peak Hour Factor 0.80 | 0.80 | 0.80 | 0.80 | 0.80 | 0.80 | 0.80 | 0.80 | 0.80 | 0.80 | 0.80 | 0.80 |
| Heavy Vehicles, \% 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow 75 | 171 | 24 | 141 | 240 | 104 | 29 | 341 | 96 | 56 | 276 | 185 |
| Number of Lanes 0 | 1 | 0 | 0 | 1 | 1 | 0 | 1 | 0 | 0 | 1 | 1 |
| Approach EB |  |  | WB |  |  | NB |  |  | SB |  |  |
| Opposing Approach WB |  |  | EB |  |  | SB |  |  | NB |  |  |
| Opposing Lanes 2 |  |  | 1 |  |  | 2 |  |  | 1 |  |  |
| Conflicting Approach Left SB |  |  | NB |  |  | EB |  |  | WB |  |  |
| Conflicting Lanes Left 2 |  |  | 1 |  |  | 1 |  |  | 2 |  |  |
| Conflicting Approach RighNB |  |  | SB |  |  | WB |  |  | EB |  |  |
| Conflicting Lanes Right 1 |  |  | 2 |  |  | 2 |  |  | 1 |  |  |
| HCM Control Delay 38.8 |  |  | 59 |  |  | 148.4 |  |  | 37.4 |  |  |
| HCM LOS E |  |  | F |  |  | F |  |  | E |  |  |


| Lane | NBLn1 EBLn1WBLn1WBLn2 SBLn1 SBLn2 |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Vol Left, \% | $6 \%$ | $28 \%$ | $37 \%$ | $0 \%$ | $17 \%$ | $0 \%$ |
| Vol Thru, \% | $73 \%$ | $63 \%$ | $63 \%$ | $0 \%$ | $83 \%$ | $0 \%$ |
| Vol Right, $\%$ | $21 \%$ | $9 \%$ | $0 \%$ | $100 \%$ | $0 \%$ | $100 \%$ |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 373 | 216 | 305 | 83 | 266 | 148 |
| LT Vol | 23 | 60 | 113 | 0 | 45 | 0 |
| Through Vol | 273 | 137 | 192 | 0 | 221 | 0 |
| RT Vol | 77 | 19 | 0 | 83 | 0 | 148 |
| Lane Flow Rate | 466 | 270 | 381 | 104 | 332 | 185 |
| Geometry Grp | 6 | 6 | 7 | 7 | 7 | 7 |
| Degree of Util (X) | 1.218 | 0.738 | 0.968 | 0.238 | 0.845 | 0.429 |
| Departure Headway (Hd) | 9.404 | 10.78 | 9.85 | 8.922 | 9.848 | 9.025 |
| Convergence, Y/N | Yes | Yes | Yes | Yes | Yes | Yes |
| Cap | 392 | 337 | 370 | 405 | 369 | 401 |
| Service Time | 7.404 | 8.78 | 7.55 | 6.622 | 7.548 | 6.725 |
| HCM Lane V/C Ratio | 1.189 | 0.801 | 1.03 | 0.257 | 0.9 | 0.461 |
| HCM Control Delay | 148.4 | 38.8 | 71.2 | 14.4 | 48.1 | 18.3 |
| HCM Lane LOS | F | E | F | B | E | C |
| HCM 95th-tile Q | 19.4 | 5.6 | 10.8 | 0.9 | 7.8 | 2.1 |




| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | ＊ | 444 | 「 | ＊＊ | 444 | 「 | ＊＊ | 444 | F | ＊＊ | 惺 |  |
| Traffic Volume（veh／h） | 394 | 1589 | 281 | 361 | 1542 | 249 | 446 | 898 | 238 | 261 | 775 | 160 |
| Future Volume（veh／h） | 394 | 1589 | 281 | 361 | 1542 | 249 | 446 | 898 | 238 | 261 | 775 | 160 |
| Initial $Q(Q b)$ ，veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow，veh／h／ln | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 |
| Adj Flow Rate，veh／h | 419 | 1690 | 155 | 384 | 1640 | 0 | 474 | 955 | 0 | 278 | 824 | 150 |
| Peak Hour Factor | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 |
| Percent Heavy Veh，\％ | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| Cap，veh／h | 466 | 1784 | 553 | 546 | 1971 |  | 522 | 1318 |  | 327 | 876 | 158 |
| Arrive On Green | 0.13 | 0.35 | 0.35 | 0.16 | 0.38 | 0.00 | 0.15 | 0.26 | 0.00 | 0.09 | 0.20 | 0.20 |
| Sat Flow，veh／h | 3483 | 5147 | 1596 | 3483 | 5147 | 1598 | 3483 | 5147 | 1598 | 3483 | 4380 | 792 |
| Grp Volume（v），veh／h | 419 | 1690 | 155 | 384 | 1640 | 0 | 474 | 955 | 0 | 278 | 644 | 330 |
| Grp Sat Flow（s），veh／h／ln | 1742 | 1716 | 1596 | 1742 | 1716 | 1598 | 1742 | 1716 | 1598 | 1742 | 1716 | 1741 |
| Q Serve（g＿s），s | 17.8 | 47.9 | 7.0 | 15.7 | 43.3 | 0.0 | 20.1 | 25.4 | 0.0 | 11.8 | 27.7 | 28.0 |
| Cycle Q Clear（g＿c），s | 17.8 | 47.9 | 7.0 | 15.7 | 43.3 | 0.0 | 20.1 | 25.4 | 0.0 | 11.8 | 27.7 | 28.0 |
| Prop In Lane | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 0.45 |
| Lane Grp Cap（c），veh／h | 466 | 1784 | 553 | 546 | 1971 |  | 522 | 1318 |  | 327 | 686 | 348 |
| V／C Ratio（X） | 0.90 | 0.95 | 0.28 | 0.70 | 0.83 |  | 0.91 | 0.72 |  | 0.85 | 0.94 | 0.95 |
| Avail Cap（c＿a），veh／h | 534 | 1784 | 553 | 546 | 1971 |  | 604 | 1318 |  | 488 | 686 | 348 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter（l） | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay（d），s／veh | 64.0 | 47.7 | 15.8 | 59.9 | 41.9 | 0.0 | 62.7 | 51.0 | 0.0 | 66.9 | 59.1 | 59.2 |
| Incr Delay（d2），s／veh | 15.5 | 12.0 | 1.3 | 3.5 | 4.3 | 0.0 | 15.0 | 2.2 | 0.0 | 6.0 | 21.0 | 34.8 |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ（50\％），veh／In | 8.7 | 21.8 | 4.1 | 7.1 | 18.5 | 0.0 | 9.8 | 11.0 | 0.0 | 5.4 | 13.8 | 15.5 |
| Unsig．Movement Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay（d），s／veh | 79.5 | 59.7 | 17.1 | 63.4 | 46.2 | 0.0 | 77.8 | 53.1 | 0.0 | 72.9 | 80.1 | 94.0 |
| LnGrp LOS | E | E | B | E | D |  | E | D |  | E | F | F |
| Approach Vol，veh／h |  | 2264 |  |  | 2024 | A |  | 1429 | A |  | 1252 |  |
| Approach Delay，s／veh |  | 60.4 |  |  | 49.5 |  |  | 61.3 |  |  | 82.1 |  |
| Approach LOS |  | E |  |  | D |  |  | E |  |  | F |  |


| Timer－Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Phs Duration（G＋Y＋Rc），s | 29.5 | 58.0 | 26.5 | 36.0 | 24.1 | 63.4 | 18.1 | 44.4 |
| Change Period（Y＋Rc），s | 6.0 | 6.0 | 4.0 | 6.0 | 4.0 | 6.0 | 4.0 | 6.0 |
| Max Green Setting（Gmax），s | 20.0 | 52.0 | 26.0 | 30.0 | 23.0 | 51.0 | 21.0 | 35.0 |
| Max Q Clear Time（g＿c＋I1），s | 17.7 | 49.9 | 22.1 | 30.0 | 19.8 | 45.3 | 13.8 | 27.4 |
| Green Ext Time（p＿c），s | 0.2 | 1.9 | 0.4 | 0.0 | 0.3 | 4.5 | 0.3 | 4.2 |

## Intersection Summary

| HCM 6th Ctrl Delay | 61.3 |
| :--- | ---: |
| HCM 6th LOS | E |

## Notes

User approved pedestrian interval to be less than phase max green．
Unsignalized Delay for［NBR，WBR］is excluded from calculations of the approach delay and intersection delay．

| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ＊ | 44 | 「 | \＃ | 虾 |  |  | $\uparrow$ | 「 |  | $\uparrow$ | 「 |
| Traffic Vol，veh／h | 45 | 2127 | 60 | 48 | 1942 | 4 | 7 | 0 | 44 | 0 | 1 | 37 |
| Future Vol，veh／h | 45 | 2127 | 60 | 48 | 1942 | 4 | 7 | 0 | 44 | 0 | 1 | 37 |
| Conflicting Peds，\＃／hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | － | － | None | － | － | None | － | － | None | － | － | None |
| Storage Length | 150 | － | 100 | 175 | － | － | － | － | 125 | － | － | 25 |
| Veh in Median Storage，\＃ | － | 0 | － | － | 0 | － | － | 0 | － | － | 0 | － |
| Grade，\％ | － | 0 | － | － | 0 | － | － | 0 | － | － | 0 | － |
| Peak Hour Factor | 94 | 94 | 94 | 94 | 94 | 94 | 94 | 94 | 94 | 94 | 94 | 94 |
| Heavy Vehicles，\％ | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| Mvmt Flow | 48 | 2263 | 64 | 51 | 2066 | 4 | 7 | 0 | 47 | 0 | 1 | 39 |



HCM 6th Signalized Intersection Summary
3: Douglas Blvd \& Seeno Ave
3. Douglas 05/25/2018

|  | 4 |  |  | 7 |  |  | 4 | 4 | $p$ |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \% | 个t |  | * | 个t |  |  | $\uparrow$ |  |  | $\uparrow$ | 7 |
| Traffic Volume (veh/h) | 41 | 2096 | 31 | , | 1934 | 18 | 18 | 0 | 2 | 26 | 0 | 31 |
| Future Volume (veh/h) | 41 | 2096 | 31 | 4 | 1934 | 18 | 18 | 0 | 2 | 26 | 0 | 31 |
| Initial $\mathrm{Q}(\mathrm{Qb})$, veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 |  | 1.00 | 1.00 |  | 0.98 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow, veh/h/ln | 1885 | 1885 | 1885 | 1870 | 1885 | 1885 | 1870 | 1870 | 1870 | 1870 | 1870 | 1885 |
| Adj Flow Rate, veh/h | 44 | 2230 | 34 | 4 | 2057 | 19 | 20 | 0 | 2 | 28 | 0 | 12 |
| Peak Hour Factor | 0.94 | 0.94 | 0.92 | 0.92 | 0.94 | 0.94 | 0.92 | 0.92 | 0.92 | 0.94 | 0.92 | 0.94 |
| Percent Heavy Veh, \% | 1 | 1 | 1 | 2 | 1 | 1 | 2 | 2 | 2 | 2 | 2 | 1 |
| Cap, veh/h | 56 | 2536 | 39 | 0 | 2451 | 23 | 38 | 0 | 4 | 88 | 0 | 79 |
| Arrive On Green | 0.03 | 0.70 | 0.70 | 0.00 | 0.67 | 0.67 | 0.02 | 0.00 | 0.02 | 0.05 | 0.00 | 0.05 |
| Sat Flow, veh/h | 1795 | 3611 | 55 | 1781 | 3636 | 34 | 1601 | 0 | 160 | 1781 | 0 | 1598 |
| Grp Volume(v), veh/h | 44 | 1103 | 1161 |  | 1011 | 1065 | 22 | 0 | 0 | 28 | 0 | 12 |
| Grp Sat Flow(s),veh/h/ln | 1795 | 1791 | 1875 | 1781 | 1791 | 1878 | 1761 | 0 | 0 | 1781 | 0 | 1598 |
| Q Serve(g_s), s | 2.1 | 42.1 | 42.6 | 0.2 | 37.2 | 37.5 | 1.1 | 0.0 | 0.0 | 1.3 | 0.0 | 0.6 |
| Cycle Q Clear(g_c), s | 2.1 | 42.1 | 42.6 | 0.2 | 37.2 | 37.5 | 1.1 | 0.0 | 0.0 | 1.3 | 0.0 | 0.6 |
| Prop In Lane | 1.00 |  | 0.03 | 1.00 |  | 0.02 | 0.91 |  | 0.09 | 1.00 |  | 1.00 |
| Lane Grp Cap(c), veh/h | 56 | 1258 | 1317 | 6 | 1208 | 1266 | 42 | 0 | 0 | 88 | 0 | 79 |
| V/C Ratio(X) | 0.79 | 0.88 | 0.88 | 0.71 | 0.84 | 0.84 | 0.53 | 0.00 | 0.00 | 0.32 | 0.00 | 0.15 |
| Avail Cap(c_a), veh/h | 469 | 1363 | 1427 | 263 | 1363 | 1429 | 360 | 0 | 0 | 1355 | 0 | 1215 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(1) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 0.00 | 1.00 | 0.00 | 1.00 |
| Uniform Delay (d), s/veh | 42.4 | 10.2 | 10.3 | 43.9 | 10.7 | 10.8 | 42.5 | 0.0 | 0.0 | 40.4 | 0.0 | 40.1 |
| Incr Delay (d2), s/veh | 8.8 | 6.4 | 6.4 | 45.7 | 4.3 | 4.2 | 10.0 | 0.0 | 0.0 | 2.0 | 0.0 | 0.9 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile BackOfQ(50\%),veh/ln | 1.0 | 11.7 | 12.4 | 0.2 | 10.6 | 11.2 | 0.6 | 0.0 | 0.0 | 0.6 | 0.0 | 0.3 |
| Unsig. Movement Delay, s/veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay(d),s/veh | 51.2 | 16.6 | 16.7 | 89.5 | 15.1 | 15.0 | 52.5 | 0.0 | 0.0 | 42.4 | 0.0 | 40.9 |
| LnGrp LOS | D | B | B | F | B | B | D | A | A | D | A | D |
| Approach Vol, veh/h |  | 2308 |  |  | 2080 |  |  | 22 |  |  | 40 |  |
| Approach Delay, s/veh |  | 17.3 |  |  | 15.2 |  |  | 52.5 |  |  | 42.0 |  |
| Approach LOS |  | B |  |  | B |  |  | D |  |  | D |  |
| Timer - Assigned Phs | 1 | 2 |  | 4 | 5 | 6 |  | 8 |  |  |  |  |
| Phs Duration ( $\mathrm{G}+\mathrm{Y}+\mathrm{Rc}$ ), s | 5.7 | 65.4 |  | 10.4 | 3.3 | 67.8 |  | 6.6 |  |  |  |  |
| Change Period ( $Y+R \mathrm{c}$ ), s | 3.0 | 6.0 |  | 6.0 | 3.0 | 6.0 |  | 4.5 |  |  |  |  |
| Max Green Setting (Gmax), s | 23.0 | 67.0 |  | 67.0 | 13.0 | 67.0 |  | 18.0 |  |  |  |  |
| Max Q Clear Time (g_c+11), s | 4.1 | 39.5 |  | 3.3 | 2.2 | 44.6 |  | 3.1 |  |  |  |  |
| Green Ext Time (p_c), s | 0.0 | 17.8 |  | 0.2 | 0.0 | 17.2 |  | 0.0 |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 6th Ctrl DelayHCM 6th LOS |  |  | 16.7 |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |

## Notes

User approved ignoring U-Turning movement.

| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |


| Major/Minor | Major1 | Major2 | Minor1 |  |  |
| :--- | ---: | ---: | :--- | :--- | :--- |
| Conflicting Flow All | 0 | 0 | 2298 | 0 | -1149 |
| $\quad$ Stage 1 | - | - | - | - | - |
| $\quad$ Stage 2 | - | - | - | - | - |
| Critical Hdwy | - | - | 4.14 | - | - |
| Critical Hdwy Stg 1 | - | - | - | - | - |
| Critical Hdwy Stg 2 | - | - | - | - | - |
| Follow-up Hdwy | - | - | 2.22 | - | - |
| Pot Cap-1 Maneuver | - | - | 216 | - | 0 |
| $\quad$ Stage 1 | - | - | - | - | 0 |
| $\quad$ Stage 2 | - | - | - | - | 0 |


|  | EB | WB | NB |
| :--- | :---: | :---: | :---: |
| Approach | 0.7 | 68.6 |  |
| HCM Control Delay, s | 0 | 0.7 |  |
| HCM LOS |  |  | F |


| Minor Lane/Major Mvmt | NBLn1 | EBT | EBR | WBL | WBT |
| :--- | ---: | ---: | ---: | ---: | :--- |
| Capacity (veh/h) | 192 | - | -216 | - |  |
| HCM Lane V/C Ratio | 0.776 | - | -0.267 | - |  |
| HCM Control Delay (s) | 68.6 | - | -27.6 | - |  |
| HCM Lane LOS | F | - | - | D | - |
| HCM 95th \%tile Q(veh) | 5.2 | - | - | 1 | - |


| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \＃ | 虫 |  | \＃ | 中 ${ }^{\text {a }}$ |  |  |  | 「 |  |  | 「 |
| Traffic Vol，veh／h | 136 | 2009 | 27 | 52 | 1832 | 14 | 0 | 0 | 11 | 0 | 0 | 72 |
| Future Vol，veh／h | 136 | 2009 | 27 | 52 | 1832 | 14 | 0 | 0 | 11 | 0 | 0 | 72 |
| Conflicting Peds，\＃／hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | － | － | None | － | － | None | － | － | None | － | － | None |
| Storage Length | 250 | － | － | 325 | － | － | － | － | 0 | － | － | 0 |
| Veh in Median Storage，\＃ | － | 0 | － | － | 0 | － | － | 0 | － | － | 0 | － |
| Grade，\％ | － | 0 | － | － | 0 | － | － | 0 | － | － | 0 | － |
| Peak Hour Factor | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 |
| Heavy Vehicles，\％ | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| Mvmt Flow | 143 | 2115 | 28 | 55 | 1928 | 15 | 0 | 0 | 12 | 0 | 0 | 76 |



Stage 2

| Approach | EB | WB | NB | SB |
| :--- | :---: | :---: | :---: | :---: |
| HCM Control Delay，s | 1.7 | 0.6 | 22.4 | 25.1 |
| HCM LOS |  |  | $C$ | D |


| Minor Lane／Major Mvmt | NBLn1 | EBL | EBT | EBR | WBL | WBT | WBR SBLn1 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Capacity（veh／h） | 218 | 302 | - | -252 | - | -254 |  |
| HCM Lane V／C Ratio | 0.053 | 0.474 | - | -0.217 | - | -0.298 |  |
| HCM Control Delay（s） | 22.4 | 27.2 | - | - | 23.2 | - | -25.1 |
| HCM Lane LOS | C | D | - | - | C | - | - |
| HCM 95th \％tile Q（veh） | 0.2 | 2.4 | - | - | 0.8 | - | - |
| （ven |  |  |  |  |  |  |  |


| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | \＃ | 中 ${ }^{\text {F }}$ |  | \＃ | 44 | 「 | ${ }^{7}$ | $\uparrow$ | 「 |  | $\uparrow$ | 「 |
| Traffic Volume（veh／h） | 102 | 1738 | 247 | 98 | 1568 | 178 | 149 | 85 | 109 | 162 | 96 | 63 |
| Future Volume（veh／h） | 102 | 1738 | 247 | 98 | 1568 | 178 | 149 | 85 | 109 | 162 | 96 | 63 |
| Initial Q（Qb），veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 0.98 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow，veh／h／ln | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Adj Flow Rate，veh／h | 105 | 1792 | 248 | 101 | 1616 | 142 | 121 | 134 | 0 | 167 | 99 | 20 |
| Peak Hour Factor | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 |
| Percent Heavy Veh，\％ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Cap，veh／h | 133 | 1514 | 204 | 129 | 1705 | 760 | 167 | 175 |  | 191 | 113 | 266 |
| Arrive On Green | 0.07 | 0.47 | 0.47 | 0.07 | 0.47 | 0.47 | 0.09 | 0.09 | 0.00 | 0.16 | 0.16 | 0.16 |
| Sat Flow，veh／h | 1810 | 3187 | 430 | 1810 | 3610 | 1608 | 1810 | 1900 | 1610 | 1157 | 686 | 1610 |
| Grp Volume（v），veh／h | 105 | 994 | 1046 | 101 | 1616 | 142 | 121 | 134 | 0 | 266 | 0 | 20 |
| Grp Sat Flow（s），veh／h／ln | 1810 | 1805 | 1812 | 1810 | 1805 | 1608 | 1810 | 1900 | 1610 | 1842 | 0 | 1610 |
| Q Serve（g＿s），s | 5.2 | 42.9 | 42.9 | 5.0 | 38.7 | 4.6 | 5.9 | 6.2 | 0.0 | 12.7 | 0.0 | 0.9 |
| Cycle Q Clear（g＿c），s | 5.2 | 42.9 | 42.9 | 5.0 | 38.7 | 4.6 | 5.9 | 6.2 | 0.0 | 12.7 | 0.0 | 0.9 |
| Prop In Lane | 1.00 |  | 0.24 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 0.63 |  | 1.00 |
| Lane Grp Cap（c），veh／h | 133 | 857 | 861 | 129 | 1705 | 760 | 167 | 175 |  | 304 | 0 | 266 |
| V／C Ratio（X） | 0.79 | 1.16 | 1.22 | 0.78 | 0.95 | 0.19 | 0.73 | 0.77 |  | 0.88 | 0.00 | 0.08 |
| Avail Cap（c＿a），veh／h | 300 | 857 | 861 | 400 | 1797 | 801 | 400 | 420 |  | 408 | 0 | 356 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter（I） | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 0.00 | 1.00 |
| Uniform Delay（d），s／veh | 41.2 | 23.7 | 23.7 | 41.3 | 22.8 | 13.8 | 39.9 | 40.1 | 0.0 | 36.8 | 0.0 | 31.9 |
| Incr Delay（d2），s／veh | 3.8 | 84.6 | 107.7 | 3.9 | 10.7 | 0.0 | 2.3 | 2.6 | 0.0 | 12.3 | 0.0 | 0.0 |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ（50\％），veh／ln | 2.3 | 35.2 | 40.8 | 2.2 | 16.4 | 1.5 | 2.6 | 2.9 | 0.0 | 6.6 | 0.0 | 0.4 |
| Unsig．Movement Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay（d），s／veh | 45.0 | 108.4 | 131.4 | 45.2 | 33.5 | 13.8 | 42.2 | 42.7 | 0.0 | 49.2 | 0.0 | 32.0 |
| LnGrp LOS | D | F | F | D | C | B | D | D |  | D | A | C |
| Approach Vol，veh／h |  | 2145 |  |  | 1859 |  |  | 255 | A |  | 286 |  |
| Approach Delay，s／veh |  | 116.5 |  |  | 32.6 |  |  | 42.5 |  |  | 48.0 |  |
| Approach LOS |  | F |  |  | C |  |  | D |  |  | D |  |


| Timer－Assigned Phs | 1 | 2 | 4 | 5 | 6 | 8 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Phs Duration（G＋Y＋Rc），s | 9.4 | 48.9 | 19.3 | 9.7 | 48.7 | 12.7 |
| Change Period（Y＋Rc），s | 3.0 | 6.0 | 4.4 | 3.0 | 6.0 | 4.4 |
| Max Green Setting（Gmax），s | 20.0 | 40.0 | 20.0 | 15.0 | 45.0 | 20.0 |
| Max Q Clear Time（g＿c＋11），s | 7.0 | 44.9 | 14.7 | 7.2 | 40.7 | 8.2 |
| Green Ext Time（p＿c），s | 0.0 | 0.0 | 0.2 | 0.0 | 2.1 | 0.1 |

## Intersection Summary

| HCM 6th Ctrl Delay | 73.7 |
| :--- | ---: |
| HCM 6th LOS | E |

## Notes

User approved pedestrian interval to be less than phase max green．
User approved volume balancing among the lanes for turning movement．
Unsignalized Delay for［NBR］is excluded from calculations of the approach delay and intersection delay．


Unsignalized Delay for [NBR, EBR, WBR, SBR] is excluded from calculations of the approach delay and intersection delay.
Intersection
Intersection Delay, s/veh43.9
Intersection LOS E


| Lane | NBLn1 | EBLn1WBLn1WBLn2 SBLn1 SBLn2 |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Vol Left, \% | $8 \%$ | $15 \%$ | $24 \%$ | $0 \%$ | $28 \%$ | $0 \%$ |
| Vol Thru, \% | $77 \%$ | $70 \%$ | $76 \%$ | $0 \%$ | $72 \%$ | $0 \%$ |
| Vol Right, \% | $15 \%$ | $15 \%$ | $0 \%$ | $100 \%$ | $0 \%$ | $100 \%$ |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 264 | 338 | 171 | 55 | 390 | 49 |
| LT Vol | 21 | 50 | 41 | 0 | 110 | 0 |
| Through Vol | 204 | 238 | 130 | 0 | 280 | 0 |
| RT Vol | 39 | 50 | 0 | 55 | 0 | 49 |
| Lane Flow Rate | 290 | 371 | 188 | 60 | 429 | 54 |
| Geometry Grp | 6 | 6 | 7 | 7 | 7 | 7 |
| Degree of Util (X) | 0.705 | 0.878 | 0.474 | 0.138 | 0.985 | 0.111 |
| Departure Headway (Hd) | 8.746 | 8.509 | 9.088 | 8.234 | 8.273 | 7.403 |
| Convergence, Y/N | Yes | Yes | Yes | Yes | Yes | Yes |
| Cap | 412 | 427 | 396 | 435 | 441 | 485 |
| Service Time | 6.818 | 6.535 | 6.859 | 6.005 | 6.001 | 5.131 |
| HCM Lane V/C Ratio | 0.704 | 0.869 | 0.475 | 0.138 | 0.973 | 0.111 |
| HCM Control Delay | 30.3 | 48.3 | 19.8 | 12.3 | 68.4 | 11.1 |
| HCM Lane LOS | D | E | C | B | F | B |
| HCM 95th-tile Q | 5.3 | 9 | 2.5 | 0.5 | 12.3 | 0.4 |




| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | ${ }_{4}^{4}$ | 444 | 「 | ＊＊ | 444 | 「 | ＊＊ | 444 | 「 | ＊＊ | 衡 |  |
| Traffic Volume（veh／h） | 212 | 1276 | 176 | 246 | 1852 | 119 | 450 | 824 | 157 | 216 | 588 | 180 |
| Future Volume（veh／h） | 212 | 1276 | 176 | 246 | 1852 | 119 | 450 | 824 | 157 | 216 | 588 | 180 |
| Initial Q（Qb），veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 0.99 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 0.99 |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow，veh／h／ln | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 |
| Adj Flow Rate，veh／h | 230 | 1387 | 64 | 267 | 2013 | 0 | 489 | 896 | 0 | 235 | 639 | 148 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh，\％ | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap，veh／h | 289 | 1659 | 508 | 513 | 2075 |  | 543 | 1314 |  | 297 | 773 | 176 |
| Arrive On Green | 0.08 | 0.32 | 0.32 | 0.15 | 0.41 | 0.00 | 0.21 | 0.34 | 0.00 | 0.09 | 0.19 | 0.19 |
| Sat Flow，veh／h | 3456 | 5106 | 1564 | 3456 | 5106 | 1585 | 3456 | 5106 | 1585 | 3456 | 4151 | 946 |
| Grp Volume（v），veh／h | 230 | 1387 | 64 | 267 | 2013 | 0 | 489 | 896 | 0 | 235 | 522 | 265 |
| Grp Sat Flow（s），veh／h／ln | 1728 | 1702 | 1564 | 1728 | 1702 | 1585 | 1728 | 1702 | 1585 | 1728 | 1702 | 1693 |
| Q Serve（g＿s），s | 7.8 | 30.2 | 2.2 | 8.6 | 46.4 | 0.0 | 16.5 | 18.1 | 0.0 | 8.0 | 17.7 | 18.1 |
| Cycle Q Clear（g＿c），s | 7.8 | 30.2 | 2.2 | 8.6 | 46.4 | 0.0 | 16.5 | 18.1 | 0.0 | 8.0 | 17.7 | 18.1 |
| Prop In Lane | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 0.56 |
| Lane Grp Cap（c），veh／h | 289 | 1659 | 508 | 513 | 2075 |  | 543 | 1314 |  | 297 | 634 | 315 |
| V／C Ratio（X） | 0.80 | 0.84 | 0.13 | 0.52 | 0.97 |  | 0.90 | 0.68 |  | 0.79 | 0.82 | 0.84 |
| Avail Cap（c＿a），veh／h | 461 | 1659 | 508 | 513 | 2075 |  | 605 | 1314 |  | 605 | 681 | 339 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.33 | 1.33 | 1.33 | 1.00 | 1.00 | 1.00 |
| Upstream Filter（l） | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay（d），s／veh | 54.0 | 37.5 | 11.8 | 47.1 | 34.9 | 0.0 | 46.6 | 35.3 | 0.0 | 53.8 | 46.9 | 47.1 |
| Incr Delay（d2），s／veh | 1.9 | 5.2 | 0.5 | 0.4 | 13.4 | 0.0 | 14.7 | 1.6 | 0.0 | 1.8 | 8.2 | 17.1 |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ（50\％），veh／In | 3.4 | 12.8 | 1.3 | 3.6 | 20.5 | 0.0 | 7.6 | 6.9 | 0.0 | 3.5 | 8.0 | 8.9 |
| Unsig．Movement Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay（d），s／veh | 55.9 | 42.7 | 12.3 | 47.6 | 48.3 | 0.0 | 61.3 | 36.8 | 0.0 | 55.6 | 55.2 | 64.3 |
| LnGrp LOS | E | D | B | D | D |  | E | D |  | E | E | E |
| Approach Vol，veh／h |  | 1681 |  |  | 2280 | A |  | 1385 | A |  | 1022 |  |
| Approach Delay，s／veh |  | 43.3 |  |  | 48.2 |  |  | 45.5 |  |  | 57.6 |  |
| Approach LOS |  | D |  |  | D |  |  | D |  |  | E |  |


| Timer－Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Phs Duration（G＋Y＋Rc），s | 23.8 | 45.0 | 22.8 | 28.3 | 14.0 | 54.8 | 14.3 | 36.9 |
| Change Period（Y＋Rc），s | 6.0 | 6.0 | 4.0 | 6.0 | 4.0 | 6.0 | 4.0 | 6.0 |
| Max Green Setting（Gmax），s | 14.0 | 39.0 | 21.0 | 24.0 | 16.0 | 39.0 | 21.0 | 24.0 |
| Max Q Clear Time（g＿c＋I1），s | 10.6 | 32.2 | 18.5 | 20.1 | 9.8 | 48.4 | 10.0 | 20.1 |
| Green Ext Time（p＿c），s | 0.2 | 5.3 | 0.3 | 2.1 | 0.2 | 0.0 | 0.3 | 2.3 |

Intersection Summary

| HCM 6th Ctrl Delay | 47.8 |
| :--- | ---: |
| HCM 6th LOS | D |

## Notes

User approved pedestrian interval to be less than phase max green．
Unsignalized Delay for［NBR，WBR］is excluded from calculations of the approach delay and intersection delay．



|  | 3 |  | 7 | $\checkmark$ |  | 4 | 4 | $\dagger$ | $p$ |  | $\dagger$ | $\pm$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \# | 中 ${ }^{\text {a }}$ |  | \# | 中 ${ }^{\text {a }}$ |  |  | * |  |  | $\uparrow$ | F |
| Traffic Volume (veh/h) | 68 | 1516 | 9 | 3 | 1959 | 82 | 27 | 0 | 4 | 50 | 0 | 46 |
| Future Volume (veh/h) | 68 | 1516 | 9 | 3 | 1959 | 82 | 27 | 0 | 4 | 50 | 0 | 46 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 |  | 1.00 | 1.00 |  | 0.98 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow, veh/h/ln | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 |
| Adj Flow Rate, veh/h | 74 | 1648 | 10 | 3 | 2129 | 87 | 29 | 0 | 4 | 54 | 0 | 14 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap, veh/h | 95 | 2669 | 16 | 4 | 2385 | 97 | 48 | 0 | 7 | 79 | 0 | 70 |
| Arrive On Green | 0.05 | 0.74 | 0.74 | 0.00 | 0.69 | 0.69 | 0.03 | 0.00 | 0.03 | 0.04 | 0.00 | 0.04 |
| Sat Flow, veh/h | 1781 | 3621 | 22 | 1781 | 3477 | 141 | 1542 | 0 | 213 | 1781 | 0 | 1585 |
| Grp Volume(v), veh/h | 74 | 808 | 850 | 3 | 1080 | 1136 | 33 | 0 | 0 | 54 | 0 | 14 |
| Grp Sat Flow(s), veh/h/ln | 1781 | 1777 | 1866 | 1781 | 1777 | 1841 | 1755 | 0 | 0 | 1781 | 0 | 1585 |
| Q Serve(g_s), s | 3.8 | 20.1 | 20.2 | 0.2 | 44.6 | 46.4 | 1.7 | 0.0 | 0.0 | 2.7 | 0.0 | 0.8 |
| Cycle Q Clear(g_c), s | 3.8 | 20.1 | 20.2 | 0.2 | 44.6 | 46.4 | 1.7 | 0.0 | 0.0 | 2.7 | 0.0 | 0.8 |
| Prop In Lane | 1.00 |  | 0.01 | 1.00 |  | 0.08 | 0.88 |  | 0.12 | 1.00 |  | 1.00 |
| Lane Grp Cap(c), veh/h | 95 | 1310 | 1376 | 4 | 1219 | 1263 | 54 | 0 | 0 | 79 | 0 | 70 |
| V/C Ratio(X) | 0.78 | 0.62 | 0.62 | 0.70 | 0.89 | 0.90 | 0.61 | 0.00 | 0.00 | 0.68 | 0.00 | 0.20 |
| Avail Cap(c_a), veh/h | 446 | 1310 | 1376 | 252 | 1297 | 1345 | 344 | 0 | 0 | 660 | 0 | 587 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 0.00 | 1.00 | 0.00 | 1.00 |
| Uniform Delay (d), s/veh | 42.9 | 5.8 | 5.8 | 45.7 | 11.5 | 11.8 | 43.9 | 0.0 | 0.0 | 43.2 | 0.0 | 42.3 |
| Incr Delay (d2), s/veh | 5.0 | 0.9 | 0.8 | 55.5 | 7.4 | 8.2 | 10.4 | 0.0 | 0.0 | 3.9 | 0.0 | 0.5 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile BackOfQ(50\%),veh/ln | 1.7 | 4.3 | 4.5 | 0.1 | 13.5 | 14.8 | 0.9 | 0.0 | 0.0 | 1.3 | 0.0 | 0.3 |
| Unsig. Movement Delay, s/veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay(d),s/veh | 47.9 | 6.7 | 6.7 | 101.2 | 18.9 | 20.0 | 54.3 | 0.0 | 0.0 | 47.1 | 0.0 | 42.8 |
| LnGrp LOS | D | A | A | F | B | B | D | A | A | D | A | D |
| Approach Vol, veh/h |  | 1732 |  |  | 2219 |  |  | 33 |  |  | 68 |  |
| Approach Delay, s/veh |  | 8.4 |  |  | 19.6 |  |  | 54.3 |  |  | 46.2 |  |
| Approach LOS |  | A |  |  | B |  |  | D |  |  | D |  |
| Timer - Assigned Phs | 1 | 2 |  | 4 | 5 | 6 |  | 8 |  |  |  |  |
| Phs Duration ( $\mathrm{G}+\mathrm{Y}+\mathrm{Rc}$ ), s | 7.9 | 68.9 |  | 7.6 | 3.2 | 73.6 |  | 7.3 |  |  |  |  |
| Change Period ( $\mathrm{Y}+\mathrm{Rc}$ ), s | 3.0 | 6.0 |  | 3.5 | 3.0 | 6.0 |  | 4.5 |  |  |  |  |
| Max Green Setting (Gmax), s | 23.0 | 67.0 |  | 34.0 | 13.0 | 67.0 |  | 18.0 |  |  |  |  |
| Max Q Clear Time (g_c+11), s | 5.8 | 48.4 |  | 4.7 | 2.2 | 22.2 |  | 3.7 |  |  |  |  |
| Green Ext Time (p_c), s | 0.0 | 14.5 |  | 0.2 | 0.0 | 15.0 |  | 0.1 |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 6th Ctrl Delay |  |  | 15.5 |  |  |  |  |  |  |  |  |  |
| HCM 6th LOS |  |  | B |  |  |  |  |  |  |  |  |  |

## Notes

User approved ignoring U-Turning movement.

| Intersection |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 0.9 |  |  |  |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | 虫 |  | ${ }^{7}$ | 44 |  | 「 |
| Traffic Vol, veh/h | 1570 | 54 | 75 | 2002 | 0 | 85 |
| Future Vol, veh/h | 1570 | 54 | 75 | 2002 | 0 | 85 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | 200 | - | - | 0 |
| Veh in Median Storage, \# | \# 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 1707 | 59 | 82 | 2176 | 0 | 92 |


| Major/Minor | Major1 | Major2 |  | Minor1 |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Conflicting Flow All | 0 | 0 | 1766 | 0 | - | 883 |
| $\quad$ Stage 1 | - | - | - | - | - | - |
| $\quad$ Stage 2 | - | - | - | - | - | - |
| Critical Hdwy | - | - | 4.14 | - | - | 6.94 |
| Critical Hdwy Stg 1 | - | - | - | - | - | - |
| Critical Hdwy Stg 2 | - | - | - | - | - | - |
| Follow-up Hdwy | - | - | 2.22 | - | - | 3.32 |
| Pot Cap-1 Maneuver | - | - | 349 | - | 0 | 289 |
| $\quad$ Stage 1 | - | - | - | - | 0 | - |
| $\quad$ Stage 2 | - | - | - | - | 0 | - |
| Platoon blocked, \% | - | - |  | - |  |  |
| Mov Cap-1 Maneuver | - | - | 349 | - | - | 289 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - |
| Stage 1 | - | - | - | - | - | - |
| Stage 2 | - | - | - | - | - | - |
|  |  |  |  |  |  |  |


| Approach | EB | WB | NB |
| :--- | ---: | ---: | ---: |
| HCM Control Delay, s | 0 | 0.7 | 23.2 |
| HCM LOS |  |  | C |


| Minor Lane/Major Mvmt | NBLn1 | EBT | EBR | WBL | WBT |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 289 | - | - | 349 | - |
| HCM Lane V/C Ratio | 0.32 | - | -0.234 | - |  |
| HCM Control Delay (s) | 23.2 | - | - | 18.4 | - |
| HCM Lane LOS | C | - | - | C | - |
| HCM 95th \%tile Q(veh) | 1.3 | - | - | 0.9 | - |


| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \＃ | 虫 |  | \＃ | 虾 |  |  |  | 「 |  |  | 「 |
| Traffic Vol，veh／h | 118 | 1450 | 14 | 70 | 1954 | 28 | 0 | 0 | 2 | 0 | 0 | 81 |
| Future Vol，veh／h | 118 | 1450 | 14 | 70 | 1954 | 28 | 0 | 0 | 2 | 0 | 0 | 81 |
| Conflicting Peds，\＃／hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | － | － | None | － | － | None | － | － | None | － | － | None |
| Storage Length | 250 | － | － | 325 | － | － | － | － | 0 | － | － | 0 |
| Veh in Median Storage，\＃ | － | 0 | － | － | 0 | － | － | 0 | － | － | 0 | － |
| Grade，\％ | － | 0 | － | － | 0 | － | － | 0 | － | － | 0 | － |
| Peak Hour Factor | 96 | 96 | 96 | 96 | 96 | 96 | 96 | 96 | 96 | 96 | 96 | 96 |
| Heavy Vehicles，\％ | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| Mvmt Flow | 123 | 1510 | 15 | 73 | 2035 | 29 | 0 | 0 | 2 | 0 | 0 | 84 |



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | \＃ | 中\％ |  | \＃ | 44 | 「 | ${ }^{7}$ | $\uparrow$ | 「 |  | $\uparrow$ | 「 |
| Traffic Volume（veh／h） | 47 | 1228 | 141 | 143 | 1680 | 122 | 252 | 102 | 80 | 149 | 122 | 46 |
| Future Volume（veh／h） | 47 | 1228 | 141 | 143 | 1680 | 122 | 252 | 102 | 80 | 149 | 122 | 46 |
| Initial Q（Qb），veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 1.00 | 1.00 |  | 0.98 | 1.00 |  | 1.00 | 1.00 |  | 0.99 |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow，veh／h／ln | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 |
| Adj Flow Rate，veh／h | 50 | 1306 | 143 | 152 | 1787 | 85 | 188 | 220 | 0 | 159 | 130 | 20 |
| Peak Hour Factor | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 |
| Percent Heavy Veh，\％ | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| Cap，veh／h | 64 | 1321 | 144 | 183 | 1691 | 737 | 244 | 256 |  | 177 | 145 | 277 |
| Arrive On Green | 0.04 | 0.41 | 0.41 | 0.10 | 0.47 | 0.47 | 0.14 | 0.14 | 0.00 | 0.18 | 0.18 | 0.18 |
| Sat Flow，veh／h | 1795 | 3257 | 355 | 1795 | 3582 | 1561 | 1795 | 1885 | 1598 | 1009 | 825 | 1576 |
| Grp Volume（v），veh／h | 50 | 715 | 734 | 152 | 1787 | 85 | 188 | 220 | 0 | 289 | 0 | 20 |
| Grp Sat Flow（s），veh／h／ln | 1795 | 1791 | 1821 | 1795 | 1791 | 1561 | 1795 | 1885 | 1598 | 1835 | 0 | 1576 |
| Q Serve（g＿s），s | 2.7 | 39.0 | 39.5 | 8.2 | 46.5 | 3.0 | 10.0 | 11.3 | 0.0 | 15.2 | 0.0 | 1.0 |
| Cycle Q Clear（g＿c），s | 2.7 | 39.0 | 39.5 | 8.2 | 46.5 | 3.0 | 10.0 | 11.3 | 0.0 | 15.2 | 0.0 | 1.0 |
| Prop In Lane | 1.00 |  | 0.19 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 0.55 |  | 1.00 |
| Lane Grp Cap（c），veh／h | 64 | 727 | 739 | 183 | 1691 | 737 | 244 | 256 |  | 322 | 0 | 277 |
| V／C Ratio（X） | 0.78 | 0.98 | 0.99 | 0.83 | 1.06 | 0.12 | 0.77 | 0.86 |  | 0.90 | 0.00 | 0.07 |
| Avail Cap（c＿a），veh／h | 273 | 727 | 739 | 364 | 1691 | 737 | 364 | 382 |  | 372 | 0 | 320 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter（I） | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 0.00 | 1.00 |
| Uniform Delay（d），s／veh | 47.1 | 29.0 | 29.2 | 43.4 | 26.0 | 14.5 | 41.1 | 41.7 | 0.0 | 39.8 | 0.0 | 33.9 |
| Incr Delay（d2），s／veh | 7.3 | 29.4 | 31.2 | 3.6 | 38.7 | 0.0 | 2.6 | 8.2 | 0.0 | 20.0 | 0.0 | 0.0 |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ（50\％），veh／ln | 1.3 | 20.6 | 21.5 | 3.6 | 26.2 | 1.0 | 4.4 | 5.6 | 0.0 | 8.5 | 0.0 | 0.4 |
| Unsig．Movement Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay（d），s／veh | 54.5 | 58.4 | 60.3 | 47.1 | 64.8 | 14.6 | 43.7 | 49.9 | 0.0 | 59.7 | 0.0 | 34.0 |
| LnGrp LOS | D | E | E | D | F | B | D | D |  | E | A | C |
| Approach Vol，veh／h |  | 1499 |  |  | 2024 |  |  | 408 | A |  | 309 |  |
| Approach Delay，s／veh |  | 59.2 |  |  | 61.3 |  |  | 47.0 |  |  | 58.1 |  |
| Approach LOS |  | E |  |  | E |  |  | D |  |  | E |  |


| Timer－Assigned Phs | 1 | 2 | 4 | 5 | 6 | 8 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Phs Duration（G＋Y＋Rc），s | 13.1 | 46.0 | 21.7 | 6.5 | 52.5 | 17.8 |
| Change Period（Y＋Rc），s | 3.0 | 6.0 | 4.4 | 3.0 | 6.0 | 4.4 |
| Max Green Setting（Gmax），s | 20.0 | 40.0 | 20.0 | 15.0 | 45.0 | 20.0 |
| Max Q Clear Time（g＿c＋11），s | 10.2 | 41.5 | 17.2 | 4.7 | 48.5 | 13.3 |
| Green Ext Time（p＿c），s | 0.0 | 0.0 | 0.1 | 0.0 | 0.0 | 0.2 |

## Intersection Summary

| HCM 6th Ctrl Delay | 59.0 |
| :--- | ---: |
| HCM 6th LOS | E |

## Notes

User approved pedestrian interval to be less than phase max green．
User approved volume balancing among the lanes for turning movement．
Unsignalized Delay for［NBR］is excluded from calculations of the approach delay and intersection delay．

## $\forall \rightarrow\rangle \vdash \leftarrow \uparrow \uparrow \uparrow>\downarrow \downarrow \downarrow$

| Movement EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | 中4 | F | ${ }^{7}$ | 种 | 「 | ${ }^{7}$ | $\uparrow$ ¢ ${ }^{\text {¢ }}$ | 「 | ${ }^{7}$ | 中4 | F＇ |
| Traffic Volume（veh／h） 148 | 147 | 1037 | 80 | 315 | 99 | 1206 | 347 | 45 | 81 | 620 | 285 |
| Future Volume（veh／h） 148 | 147 | 1037 | 80 | 315 | 99 | 1206 | 347 | 45 | 81 | 620 | 285 |
| Initial Q（Qb），veh 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus，Adj 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow，veh／h／ln 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 |
| Adj Flow Rate，veh／h 164 | 163 | 0 | 89 | 350 | 0 | 1340 | 386 | 0 | 90 | 689 | 0 |
| Peak Hour Factor 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Percent Heavy Veh，\％ 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| Cap，veh／h 193 | 583 |  | 113 | 423 |  | 1398 | 734 |  | 378 | 754 |  |
| Arrive On Green 0.11 | 0.16 | 0.00 | 0.06 | 0.12 | 0.00 | 0.39 | 0.39 | 0.00 | 0.21 | 0.21 | 0.00 |
| Sat Flow，veh／h 1795 | 3582 | 1598 | 1795 | 3582 | 1598 | 3591 | 1885 | 1598 | 1795 | 3582 | 1598 |
| Grp Volume（v），veh／h 164 | 163 | 0 | 89 | 350 | 0 | 1340 | 386 | 0 | 90 | 689 | 0 |
| Grp Sat Flow（s），veh／h／ln1795 | 1791 | 1598 | 1795 | 1791 | 1598 | 1795 | 1885 | 1598 | 1795 | 1791 | 1598 |
| Q Serve（g＿s），s 9.9 | 4.4 | 0.0 | 5.4 | 10.6 | 0.0 | 40.2 | 17.4 | 0.0 | 4.6 | 20.8 | 0.0 |
| Cycle Q Clear（g＿c），s 9.9 | 4.4 | 0.0 | 5.4 | 10.6 | 0.0 | 40.2 | 17.4 | 0.0 | 4.6 | 20.8 | 0.0 |
| Prop In Lane 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Lane Grp Cap（c），veh／h 193 | 583 |  | 113 | 423 |  | 1398 | 734 |  | 378 | 754 |  |
| V／C Ratio（X） 0.85 | 0.28 |  | 0.79 | 0.83 |  | 0.96 | 0.53 |  | 0.24 | 0.91 |  |
| Avail Cap（c＿a），veh／h 406 | 809 |  | 243 | 647 |  | 1460 | 767 |  | 406 | 809 |  |
| HCM Platoon Ratio 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter（I）$\quad 1.00$ | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 |
| Uniform Delay（d），s／veh 48.5 | 40.6 | 0.0 | 51.1 | 47.7 | 0.0 | 32.9 | 25.9 | 0.0 | 36.3 | 42.7 | 0.0 |
| Incr Delay（d2），s／veh 4.0 | 0.1 | 0.0 | 4.6 | 3.0 | 0.0 | 14.2 | 0.2 | 0.0 | 0.1 | 13.6 | 0.0 |
| Initial Q Delay（d3），s／veh 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ（50\％），veh／lı4． 5 | 1.9 | 0.0 | 2.5 | 4.8 | 0.0 | 19.3 | 7.5 | 0.0 | 2.0 | 10.2 | 0.0 |
| Unsig．Movement Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay（d），s／veh 52.5 | 40.7 | 0.0 | 55.7 | 50.7 | 0.0 | 47.1 | 26.2 | 0.0 | 36.4 | 56.3 | 0.0 |
| LnGrp LOS D | D |  | E | D |  | D | C |  | D | E |  |
| Approach Vol，veh／h | 327 | A |  | 439 | A |  | 1726 | A |  | 779 | A |
| Approach Delay，s／veh | 46.6 |  |  | 51.7 |  |  | 42.5 |  |  | 54.0 |  |
| Approach LOS | D |  |  | D |  |  | D |  |  | D |  |



## Notes

User approved pedestrian interval to be less than phase max green．
User approved volume balancing among the lanes for turning movement．
＊HCM 6th computational engine requires equal clearance times for the phases crossing the barrier．

Unsignalized Delay for [NBR, EBR, WBR, SBR] is excluded from calculations of the approach delay and intersection delay.

## Intersection

Intersection Delay, s/veh75.3
Intersection LOS

| Movement EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | $\stackrel{+}{4}$ |  |  | $\uparrow$ | 「' |  | $\uparrow$ |  |  | $\uparrow$ | 「' |
| Traffic Vol, veh/h 60 | 137 | 19 | 113 | 192 | 83 | 23 | 277 | 77 | 45 | 222 | 148 |
| Future Vol, veh/h 60 | 137 | 19 | 113 | 192 | 83 | 23 | 277 | 77 | 45 | 222 | 148 |
| Peak Hour Factor 0.80 | 0.80 | 0.80 | 0.80 | 0.80 | 0.80 | 0.80 | 0.80 | 0.80 | 0.80 | 0.80 | 0.80 |
| Heavy Vehicles, \% 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow 75 | 171 | 24 | 141 | 240 | 104 | 29 | 346 | 96 | 56 | 278 | 185 |
| Number of Lanes 0 | 1 | 0 | 0 | 1 | 1 | 0 | 1 | 0 | 0 | 1 | 1 |
| Approach EB |  |  | WB |  |  | NB |  |  | SB |  |  |
| Opposing Approach WB |  |  | EB |  |  | SB |  |  | NB |  |  |
| Opposing Lanes 2 |  |  | 1 |  |  | 2 |  |  | 1 |  |  |
| Conflicting Approach Left SB |  |  | NB |  |  | EB |  |  | WB |  |  |
| Conflicting Lanes Left 2 |  |  | 1 |  |  | 1 |  |  | 2 |  |  |
| Conflicting Approach RighNB |  |  | SB |  |  | WB |  |  | EB |  |  |
| Conflicting Lanes Right 1 |  |  | 2 |  |  | 2 |  |  | 1 |  |  |
| HCM Control Delay 39 |  |  | 59.4 |  |  | 153.7 |  |  | 37.8 |  |  |
| HCM LOS E |  |  | F |  |  | F |  |  | E |  |  |


| Lane | NBLn1 EBLn1WBLn1WBLn2 SBLn1 SBLn2 |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Vol Left, \% | $6 \%$ | $28 \%$ | $37 \%$ | $0 \%$ | $17 \%$ | $0 \%$ |
| Vol Thru, \% | $73 \%$ | $63 \%$ | $63 \%$ | $0 \%$ | $83 \%$ | $0 \%$ |
| Vol Right, $\%$ | $20 \%$ | $9 \%$ | $0 \%$ | $100 \%$ | $0 \%$ | $100 \%$ |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 377 | 216 | 305 | 83 | 267 | 148 |
| LT Vol | 23 | 60 | 113 | 0 | 45 | 0 |
| Through Vol | 277 | 137 | 192 | 0 | 222 | 0 |
| RT Vol | 77 | 19 | 0 | 83 | 0 | 148 |
| Lane Flow Rate | 471 | 270 | 381 | 104 | 334 | 185 |
| Geometry Grp | 6 | 6 | 7 | 7 | 7 | 7 |
| Degree of Util (X) | 1.232 | 0.738 | 0.969 | 0.238 | 0.848 | 0.43 |
| Departure Headway (Hd) | 9.412 | 10.825 | 9.88 | 8.952 | 9.875 | 9.053 |
| Convergence, Y/N | Yes | Yes | Yes | Yes | Yes | Yes |
| Cap | 391 | 337 | 370 | 404 | 370 | 400 |
| Service Time | 7.412 | 8.825 | 7.58 | 6.652 | 7.575 | 6.753 |
| HCM Lane V/C Ratio | 1.205 | 0.801 | 1.03 | 0.257 | 0.903 | 0.463 |
| HCM Control Delay | 153.7 | 39 | 71.6 | 14.4 | 48.6 | 18.4 |
| HCM Lane LOS | F | E | F | B | E | C |
| HCM 95th-tile Q | 19.9 | 5.6 | 10.8 | 0.9 | 7.8 | 2.1 |




| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | ＊＊ | 个个4 | 「 | ${ }^{4}$ | 个价 | 「 | ${ }^{4}$ | 个个4 | 「 | ${ }^{4}$ | 惺官 |  |
| Traffic Volume（veh／h） | 460 | 1773 | 295 | 371 | 1566 | 251 | 454 | 898 | 240 | 261 | 775 | 160 |
| Future Volume（veh／h） | 460 | 1773 | 295 | 371 | 1566 | 251 | 454 | 898 | 240 | 261 | 775 | 160 |
| Initial $\mathrm{Q}(\mathrm{Qb})$ ，veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow，veh／h／ln | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 |
| Adj Flow Rate，veh／h | 489 | 1886 | 170 | 395 | 1666 | 0 | 483 | 955 | 0 | 278 | 824 | 150 |
| Peak Hour Factor | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 |
| Percent Heavy Veh，\％ | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| Cap，veh／h | 530 | 1784 | 553 | 537 | 1864 |  | 531 | 1330 |  | 327 | 876 | 158 |
| Arrive On Green | 0.15 | 0.35 | 0.35 | 0.15 | 0.36 | 0.00 | 0.15 | 0.26 | 0.00 | 0.09 | 0.20 | 0.20 |
| Sat Flow，veh／h | 3483 | 5147 | 1596 | 3483 | 5147 | 1598 | 3483 | 5147 | 1598 | 3483 | 4380 | 792 |
| Grp Volume（v），veh／h | 489 | 1886 | 170 | 395 | 1666 | 0 | 483 | 955 | 0 | 278 | 644 | 330 |
| Grp Sat Flow（s），veh／h／ln | 1742 | 1716 | 1596 | 1742 | 1716 | 1598 | 1742 | 1716 | 1598 | 1742 | 1716 | 1741 |
| Q Serve（g＿s），s | 20.8 | 52.0 | 7.8 | 16.2 | 45.8 | 0.0 | 20.5 | 25.3 | 0.0 | 11.8 | 27.7 | 28.0 |
| Cycle Q Clear（g＿c），s | 20.8 | 52.0 | 7.8 | 16.2 | 45.8 | 0.0 | 20.5 | 25.3 | 0.0 | 11.8 | 27.7 | 28.0 |
| Prop In Lane | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 0.45 |
| Lane Grp Cap（c），veh／h | 530 | 1784 | 553 | 537 | 1864 |  | 531 | 1330 |  | 327 | 686 | 348 |
| V／C Ratio（X） | 0.92 | 1.06 | 0.31 | 0.73 | 0.89 |  | 0.91 | 0.72 |  | 0.85 | 0.94 | 0.95 |
| Avail Cap（c＿a），veh／h | 534 | 1784 | 553 | 537 | 1864 |  | 604 | 1330 |  | 488 | 686 | 348 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter（I） | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay（d），s／veh | 62.7 | 49.0 | 15.8 | 60.5 | 45.1 | 0.0 | 62.6 | 50.6 | 0.0 | 66.9 | 59.1 | 59.2 |
| Incr Delay（d2），s／veh | 21.4 | 38.2 | 1.4 | 4.6 | 7.1 | 0.0 | 15.6 | 2.0 | 0.0 | 6.0 | 21.0 | 34.8 |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ（50\％），veh／ln | 10.6 | 27.8 | 4.5 | 7.4 | 20.1 | 0.0 | 10.1 | 10.9 | 0.0 | 5.4 | 13.8 | 15.5 |
| Unsig．Movement Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay（d），s／veh | 84.1 | 87.2 | 17.3 | 65.1 | 52.2 | 0.0 | 78.2 | 52.7 | 0.0 | 72.9 | 80.1 | 94.0 |
| LnGrp LOS | F | F | B | E | D |  | E | D |  | E | F | F |
| Approach Vol，veh／h |  | 2545 |  |  | 2061 | A |  | 1438 | A |  | 1252 |  |
| Approach Delay，s／veh |  | 82.0 |  |  | 54.6 |  |  | 61.2 |  |  | 82.1 |  |
| Approach LOS |  | F |  |  | D |  |  | E |  |  | F |  |


| Timer－Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Phs Duration（G＋Y＋Rc），s | 29.1 | 58.0 | 26.9 | 36.0 | 26.8 | 60.3 | 18.1 | 44.8 |
| Change Period（Y＋Rc），s | 6.0 | 6.0 | 4.0 | 6.0 | 4.0 | 6.0 | 4.0 | 6.0 |
| Max Green Setting（Gmax），s | 20.0 | 52.0 | 26.0 | 30.0 | 23.0 | 51.0 | 21.0 | 35.0 |
| Max Q Clear Time（g＿c＋I1），s | 18.2 | 54.0 | 22.5 | 30.0 | 22.8 | 47.8 | 13.8 | 27.3 |
| Green Ext Time（p＿c），s | 0.2 | 0.0 | 0.4 | 0.0 | 0.0 | 2.7 | 0.3 | 4.2 |

## Intersection Summary

| HCM 6th Ctrl Delay | 70.2 |
| :--- | ---: |
| HCM 6th LOS | E |

## Notes

User approved pedestrian interval to be less than phase max green．
Unsignalized Delay for［NBR，WBR］is excluded from calculations of the approach delay and intersection delay．

| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay，s／veh | 1.9 |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \％ | 中4 | F＇ | \％ | 中 $\%$ |  |  | $\uparrow$ | 7 |  | $\uparrow$ | 「 |
| Traffic Vol，veh／h | 45 | 2134 | 60 | 50 | 1977 | 4 | 7 | 0 | 44 | 0 | 1 | 37 |
| Future Vol，veh／h | 45 | 2134 | 60 | 50 | 1977 | 4 | 7 | 0 | 44 | 0 | 1 | 37 |
| Conflicting Peds，\＃／hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | － | － | None | － | － | None | － | － | None | － | － | None |
| Storage Length | 150 | － | 100 | 175 | － | － | － | － | 125 | － | － | 25 |
| Veh in Median Storage，\＃ | － | 0 | － | － | 0 | － | － | 0 | － | － | 0 | － |
| Grade，\％ | － | 0 | － | － | 0 | － | － | 0 | － | － | 0 | － |
| Peak Hour Factor | 94 | 94 | 94 | 94 | 94 | 94 | 94 | 94 | 94 | 94 | 94 | 94 |
| Heavy Vehicles，\％ | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| Mvmt Flow | 48 | 2270 | 64 | 53 | 2103 | 4 | 7 | 0 | 47 | 0 | 1 | 39 |



HCM LOS
F

| Minor Lane／Major Mvmt | NBLn1 NBLn2 | EBL | EBT | EBR | WBL | WBT | WBR SBLn1 SBLn2 |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Capacity（veh／h） | - | 198 | 260 | - | - | 212 | - | - | 1 |


|  | 4 |  |  | 7 | - |  | 4 | 4 | $p$ |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | $\stackrel{y}{4}$ | 个t |  | \# | 性 |  |  | $\dagger$ |  |  | $\uparrow$ | F |
| Traffic Volume (veh/h) | 41 | 2103 | 31 | 4 | 1971 | 18 | 18 | 0 | 2 | 26 | 0 | 31 |
| Future Volume (veh/h) | 41 | 2103 | 31 | 4 | 1971 | 18 | 18 | 0 | 2 | 26 | 0 | 31 |
| Initial $\mathrm{Q}(\mathrm{Qb})$, veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 |  | 1.00 | 1.00 |  | 0.98 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow, veh/h/ln | 1885 | 1885 | 1885 | 1870 | 1885 | 1885 | 1870 | 1870 | 1870 | 1870 | 1870 | 1885 |
| Adj Flow Rate, veh/h | 44 | 2237 | 34 | 4 | 2097 | 19 | 20 | 0 | 2 | 28 | 0 | 12 |
| Peak Hour Factor | 0.94 | 0.94 | 0.92 | 0.92 | 0.94 | 0.94 | 0.92 | 0.92 | 0.92 | 0.94 | 0.92 | 0.94 |
| Percent Heavy Veh, \% | 1 | 1 | 1 | 2 | 1 | 1 | 2 | 2 | 2 | 2 | 2 | 1 |
| Cap, veh/h | 56 | 2538 | 38 | 6 | 2454 | 22 | 38 | 0 | 4 | 88 | 0 | 79 |
| Arrive On Green | 0.03 | 0.70 | 0.70 | 0.00 | 0.67 | 0.67 | 0.02 | 0.00 | 0.02 | 0.05 | 0.00 | 0.05 |
| Sat Flow, veh/h | 1795 | 3611 | 55 | 1781 | 3636 | 33 | 1601 | 0 | 160 | 1781 | 0 | 1598 |
| Grp Volume(v), veh/h | 44 | 1106 | 1165 | 4 | 1031 | 1085 | 22 | 0 | 0 | 28 | 0 | 12 |
| Grp Sat Flow(s),veh/h/ln | 1795 | 1791 | 1875 | 1781 | 1791 | 1878 | 1761 | 0 | 0 | 1781 | 0 | 1598 |
| Q Serve(g_s), s | 2.1 | 42.4 | 43.0 | 0.2 | 38.9 | 39.3 | 1.1 | 0.0 | 0.0 | 1.3 | 0.0 | 0.6 |
| Cycle Q Clear(g_c), s | 2.1 | 42.4 | 43.0 | 0.2 | 38.9 | 39.3 | 1.1 | 0.0 | 0.0 | 1.3 | 0.0 | 0.6 |
| Prop In Lane | 1.00 |  | 0.03 | 1.00 |  | 0.02 | 0.91 |  | 0.09 | 1.00 |  | 1.00 |
| Lane Grp Cap(c), veh/h | 56 | 1259 | 1318 | 6 | 1209 | 1268 | 42 | 0 | 0 | 88 | 0 | 79 |
| V/C Ratio(X) | 0.79 | 0.88 | 0.88 | 0.71 | 0.85 | 0.86 | 0.53 | 0.00 | 0.00 | 0.32 | 0.00 | 0.15 |
| Avail Cap(c_a), veh/h | 468 | 1359 | 1423 | 262 | 1359 | 1426 | 359 | 0 | 0 | 1352 | 0 | 1213 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 0.00 | 1.00 | 0.00 | 1.00 |
| Uniform Delay (d), s/veh | 42.5 | 10.2 | 10.3 | 44.0 | 11.0 | 11.1 | 42.6 | 0.0 | 0.0 | 40.5 | 0.0 | 40.2 |
| Incr Delay (d2), s/veh | 8.8 | 6.6 | 6.6 | 45.7 | 5.0 | 4.9 | 10.0 | 0.0 | 0.0 | 2.0 | 0.0 | 0.9 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile BackOfQ(50\%),veh/ln | 1.0 | 11.8 | 12.5 | 0.2 | 11.4 | 11.9 | 0.6 | 0.0 | 0.0 | 0.6 | 0.0 | 0.3 |
| Unsig. Movement Delay, s/veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay(d),s/veh | 51.3 | 16.8 | 16.9 | 89.6 | 16.0 | 16.0 | 52.6 | 0.0 | 0.0 | 42.5 | 0.0 | 41.0 |
| LnGrp LOS | D | B | B | F | B | B | D | A | A | D | A | D |
| Approach Vol, veh/h |  | 2315 |  |  | 2120 |  |  | 22 |  |  | 40 |  |
| Approach Delay, s/veh |  | 17.5 |  |  | 16.1 |  |  | 52.6 |  |  | 42.1 |  |
| Approach LOS |  | B |  |  | B |  |  | D |  |  | D |  |
| Timer - Assigned Phs | 1 | 2 |  | 4 | 5 | 6 |  | 8 |  |  |  |  |
| Phs Duration ( $G+Y+R \mathrm{c}$ ), $s$ | 5.7 | 65.6 |  | 10.4 | 3.3 | 68.0 |  | 6.6 |  |  |  |  |
| Change Period ( $\mathrm{Y}+\mathrm{Rc}$ ), s | 3.0 | 6.0 |  | 6.0 | 3.0 | 6.0 |  | 4.5 |  |  |  |  |
| Max Green Setting (Gmax), s | 23.0 | 67.0 |  | 67.0 | 13.0 | 67.0 |  | 18.0 |  |  |  |  |
| Max Q Clear Time (g_c+11), s | 4.1 | 41.3 |  | 3.3 | 2.2 | 45.0 |  | 3.1 |  |  |  |  |
| Green Ext Time (p_c), s | 0.0 | 17.5 |  | 0.2 | 0.0 | 17.0 |  | 0.0 |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 6th Ctrr DelayHCM 6th LOS |  |  | 17.2 |  |  |  |  |  |  |  |  |  |
|  |  |  | B |  |  |  |  |  |  |  |  |  |

## Notes

User approved ignoring U-Turning movement.

| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |


| Major/Minor | Major1 | Major2 |  | Minor1 |  |
| :--- | ---: | ---: | :--- | :--- | :--- |
| Conflicting Flow All | 0 | 0 | 2305 | 0 | -1153 |
| $\quad$ Stage 1 | - | - | - | - | - |
| $\quad$ Stage 2 | - | - | - | - | - |
| Critical Hdwy | - | - | 4.14 | - | - |
| Critical Hdwy Stg 1 | - | - | - | - | - |
| Critical Hdwy Stg 2 | - | - | - | - | - |
| Follow-up Hdwy | - | - | 2.22 | - | - |
| Pot Cap-1 Maneuver | - | - | 215 | - | 0 |
| $\quad$ Stage 1 | - | - | - | - | 0 |
| $\quad$ Stage 2 | - | - | - | - | 0 |


|  | EB | WB | NB |
| :--- | ---: | ---: | ---: |
| Approach |  |  |  |
| HCM Control Delay, $s$ | 0 | 1.1 | 69.5 |
| HCM LOS |  |  | F |





Stage 2

| Approach | EB | WB | NB | SB |
| :--- | :---: | :---: | :---: | :---: |
| HCM Control Delay, s | 1.8 | 0.6 | 22.7 | 34.6 |
| HCM LOS |  |  | C | D |


| Minor Lane/Major Mvmt | NBLn1 | EBL | EBT | EBR | WBL | WBT | WBR SBLn1 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 215 | 301 | - | - | 247 | - | - |
| HCM Lane V/C Ratio | 0.054 | 0.5 | - | -0.222 | - | -0.537 |  |
| HCM Control Delay (s) | 22.7 | 28.3 | - | - | 23.7 | - | -34.6 |
| HCM Lane LOS | C | D | - | - | $C$ | - | - |
| HCM 95th \%tile Q(veh) | 0.2 | 2.6 | - | - | 0.8 | - | - |


| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | \＃ | 中 ${ }^{\text {a }}$ |  | \＃ | 44 | 「 | ${ }^{7}$ | $\uparrow$ | 「 |  | $\uparrow$ | 「 |
| Traffic Volume（veh／h） | 102 | 1750 | 255 | 98 | 1570 | 178 | 151 | 85 | 109 | 162 | 96 | 63 |
| Future Volume（veh／h） | 102 | 1750 | 255 | 98 | 1570 | 178 | 151 | 85 | 109 | 162 | 96 | 63 |
| Initial Q（Qb），veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 0.98 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow，veh／h／ln | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Adj Flow Rate，veh／h | 105 | 1804 | 256 | 101 | 1619 | 142 | 122 | 136 | 0 | 167 | 99 | 20 |
| Peak Hour Factor | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 |
| Percent Heavy Veh，\％ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Cap，veh／h | 133 | 1509 | 208 | 129 | 1706 | 760 | 168 | 177 |  | 191 | 113 | 265 |
| Arrive On Green | 0.07 | 0.48 | 0.48 | 0.07 | 0.47 | 0.47 | 0.09 | 0.09 | 0.00 | 0.16 | 0.16 | 0.16 |
| Sat Flow，veh／h | 1810 | 3176 | 439 | 1810 | 3610 | 1608 | 1810 | 1900 | 1610 | 1157 | 686 | 1610 |
| Grp Volume（v），veh／h | 105 | 1004 | 1056 | 101 | 1619 | 142 | 122 | 136 | 0 | 266 | 0 | 20 |
| Grp Sat Flow（s），veh／h／ln | 1810 | 1805 | 1810 | 1810 | 1805 | 1608 | 1810 | 1900 | 1610 | 1842 | 0 | 1610 |
| Q Serve（g＿s），s | 5.2 | 43.1 | 43.1 | 5.0 | 39.0 | 4.6 | 6.0 | 6.4 | 0.0 | 12.8 | 0.0 | 1.0 |
| Cycle Q Clear（g＿c），s | 5.2 | 43.1 | 43.1 | 5.0 | 39.0 | 4.6 | 6.0 | 6.4 | 0.0 | 12.8 | 0.0 | 1.0 |
| Prop In Lane | 1.00 |  | 0.24 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 0.63 |  | 1.00 |
| Lane Grp Cap（c），veh／h | 133 | 857 | 860 | 129 | 1706 | 760 | 168 | 177 |  | 304 | 0 | 265 |
| V／C Ratio（X） | 0.79 | 1.17 | 1.23 | 0.78 | 0.95 | 0.19 | 0.73 | 0.77 |  | 0.88 | 0.00 | 0.08 |
| Avail Cap（c＿a），veh／h | 299 | 857 | 860 | 399 | 1789 | 797 | 399 | 418 |  | 406 | 0 | 355 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter（I） | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 0.00 | 1.00 |
| Uniform Delay（d），s／veh | 41.4 | 23.8 | 23.8 | 41.5 | 22.9 | 13.9 | 40.1 | 40.2 | 0.0 | 37.0 | 0.0 | 32.1 |
| Incr Delay（d2），s／veh | 3.9 | 89.1 | 113.1 | 3.9 | 11.0 | 0.0 | 2.2 | 2.7 | 0.0 | 12.5 | 0.0 | 0.0 |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ（50\％），veh／ln | 2.3 | 36.3 | 42.1 | 2.2 | 16.6 | 1.5 | 2.7 | 3.0 | 0.0 | 6.6 | 0.0 | 0.4 |
| Unsig．Movement Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay（d），s／veh | 45.2 | 113.0 | 137.0 | 45.4 | 33.9 | 13.9 | 42.3 | 42.9 | 0.0 | 49.5 | 0.0 | 32.1 |
| LnGrp LOS | D | F | F | D | C | B | D | D |  | D | A | C |
| Approach Vol，veh／h |  | 2165 |  |  | 1862 |  |  | 258 | A |  | 286 |  |
| Approach Delay，s／veh |  | 121.4 |  |  | 33.0 |  |  | 42.6 |  |  | 48.3 |  |
| Approach LOS |  | F |  |  | C |  |  | D |  |  | D |  |


| Timer－Assigned Phs | 1 | 2 | 4 | 5 | 6 | 8 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Phs Duration（G＋Y＋Rc），s | 9.5 | 49.1 | 19.4 | 9.7 | 48.9 | 12.8 |
| Change Period（Y＋Rc），s | 3.0 | 6.0 | 4.4 | 3.0 | 6.0 | 4.4 |
| Max Green Setting（Gmax），s | 20.0 | 40.0 | 20.0 | 15.0 | 45.0 | 20.0 |
| Max Q Clear Time（g＿c＋11），s | 7.0 | 45.1 | 14.8 | 7.2 | 41.0 | 8.4 |
| Green Ext Time（p＿c），s | 0.0 | 0.0 | 0.2 | 0.0 | 2.0 | 0.1 |

## Intersection Summary

| HCM 6th Ctrl Delay | 76.4 |
| :--- | ---: |
| HCM 6th LOS | E |

## Notes

User approved pedestrian interval to be less than phase max green．
User approved volume balancing among the lanes for turning movement．
Unsignalized Delay for［NBR］is excluded from calculations of the approach delay and intersection delay．

## $\rightarrow \rightarrow\rangle \downarrow \leftarrow \uparrow \uparrow \uparrow>\downarrow \downarrow \downarrow$

| Movement EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | 44 | 「 | ${ }^{*}$ | 44 | 「 | ${ }^{*}$ | +4 | F | ${ }^{1}$ | 44 | F |
| Traffic Volume (veh/h) 254 | 333 | 1187 | 66 | 266 | 104 | 1200 | 721 | 87 | 114 | 452 | 220 |
| Future Volume (veh/h) 254 | 333 | 1187 | 66 | 266 | 104 | 1200 | 721 | 87 | 114 | 452 | 220 |
| Initial Q (Qb), veh 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus, Adj 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow, veh/h/ln 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 |
| Adj Flow Rate, veh/h 265 | 347 | 0 | 69 | 277 | 0 | 1250 | 751 | 0 | 119 | 471 | 0 |
| Peak Hour Factor 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 |
| Percent Heavy Veh, \% 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| Cap, veh/h 294 | 767 |  | 89 | 358 |  | 1464 | 769 |  | 276 | 551 |  |
| Arrive On Green 0.16 | 0.21 | 0.00 | 0.05 | 0.10 | 0.00 | 0.41 | 0.41 | 0.00 | 0.15 | 0.15 | 0.00 |
| Sat Flow, veh/h 1795 | 3582 | 1598 | 1795 | 3582 | 1598 | 3591 | 1885 | 1598 | 1795 | 3582 | 1598 |
| Grp Volume(v), veh/h 265 | 347 | 0 | 69 | 277 | 0 | 1250 | 751 | 0 | 119 | 471 | 0 |
| Grp Sat Flow(s),veh/h/ln1795 | 1791 | 1598 | 1795 | 1791 | 1598 | 1795 | 1885 | 1598 | 1795 | 1791 | 1598 |
| Q Serve(g_s), s 16.0 | 9.3 | 0.0 | 4.2 | 8.3 | 0.0 | 34.9 | 43.3 | 0.0 | 6.6 | 14.1 | 0.0 |
| Cycle Q Clear(g_c), s 16.0 | 9.3 | 0.0 | 4.2 | 8.3 | 0.0 | 34.9 | 43.3 | 0.0 | 6.6 | 14.1 | 0.0 |
| Prop In Lane 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Lane Grp Cap(c), veh/h 294 | 767 |  | 89 | 358 |  | 1464 | 769 |  | 276 | 551 |  |
| V/C Ratio(X) 0.90 | 0.45 |  | 0.78 | 0.77 |  | 0.85 | 0.98 |  | 0.43 | 0.85 |  |
| Avail Cap(c_a), veh/h 407 | 811 |  | 244 | 649 |  | 1464 | 769 |  | 407 | 811 |  |
| HCM Platoon Ratio 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 |
| Uniform Delay (d), s/veh 45.3 | 37.7 | 0.0 | 51.9 | 48.4 | 0.0 | 29.7 | 32.2 | 0.0 | 42.3 | 45.5 | 0.0 |
| Incr Delay (d2), s/veh 15.2 | 0.2 | 0.0 | 5.4 | 1.4 | 0.0 | 4.9 | 26.7 | 0.0 | 0.4 | 4.1 | 0.0 |
| Initial Q Delay(d3),s/veh 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile BackOfQ(50\%),veh/II8.0 | 3.9 | 0.0 | 2.0 | 3.7 | 0.0 | 15.2 | 24.2 | 0.0 | 2.9 | 6.4 | 0.0 |
| Unsig. Movement Delay, s/veh |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay(d),s/veh 60.5 | 37.9 | 0.0 | 57.2 | 49.8 | 0.0 | 34.6 | 58.8 | 0.0 | 42.7 | 49.6 | 0.0 |
| LnGrp LOS E | D |  | E | D |  | C | E |  | D | D |  |
| Approach Vol, veh/h | 612 | A |  | 346 | A |  | 2001 | A |  | 590 | A |
| Approach Delay, s/veh | 47.7 |  |  | 51.3 |  |  | 43.7 |  |  | 48.2 |  |
| Approach LOS | D |  |  | D |  |  | D |  |  | D |  |



## Notes

User approved pedestrian interval to be less than phase max green.
User approved volume balancing among the lanes for turning movement.

* HCM 6th computational engine requires equal clearance times for the phases crossing the barrier.

Unsignalized Delay for [NBR, EBR, WBR, SBR] is excluded from calculations of the approach delay and intersection delay.

## Intersection

Intersection Delay, s/veh46.2
Intersection LOS

| Movement EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | \& |  |  | $\uparrow$ | 「7 |  | \& |  |  | $\uparrow$ | 「 |
| Traffic Vol, veh/h 50 | 238 | 50 | 41 | 130 | 55 | 21 | 205 | 39 | 111 | 286 | 51 |
| Future Vol, veh/h 50 | 238 | 50 | 41 | 130 | 55 | 21 | 205 | 39 | 111 | 286 | 51 |
| Peak Hour Factor 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 |
| Heavy Vehicles, \% 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Mvmt Flow 55 | 262 | 55 | 45 | 143 | 60 | 23 | 225 | 43 | 122 | 314 | 56 |
| Number of Lanes 0 | 1 | 0 | 0 | 1 | 1 | 0 | 1 | 0 | 0 | 1 | 1 |
| Approach EB |  |  | WB |  |  | NB |  |  | SB |  |  |
| Opposing Approach WB |  |  | EB |  |  | SB |  |  | NB |  |  |
| Opposing Lanes 2 |  |  | 1 |  |  | 2 |  |  | 1 |  |  |
| Conflicting Approach Left SB |  |  | NB |  |  | EB |  |  | WB |  |  |
| Conflicting Lanes Left 2 |  |  | 1 |  |  | 1 |  |  | 2 |  |  |
| Conflicting Approach RighNB |  |  | SB |  |  | WB |  |  | EB |  |  |
| Conflicting Lanes Right 1 |  |  | 2 |  |  | 2 |  |  | 1 |  |  |
| HCM Control Delay 49.5 |  |  | 18.2 |  |  | 31 |  |  | 66.7 |  |  |
| HCM LOS E |  |  | C |  |  | D |  |  | F |  |  |


| Lane | NBLn1 EBLn1WBLn1WBLn2 SBLn1 SBLn2 |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Vol Left, \% | $8 \%$ | $15 \%$ | $24 \%$ | $0 \%$ | $28 \%$ | $0 \%$ |
| Vol Thru, \% | $77 \%$ | $70 \%$ | $76 \%$ | $0 \%$ | $72 \%$ | $0 \%$ |
| Vol Right, \% | $15 \%$ | $15 \%$ | $0 \%$ | $100 \%$ | $0 \%$ | $100 \%$ |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 265 | 338 | 171 | 55 | 397 | 51 |
| LT Vol | 21 | 50 | 41 | 0 | 111 | 0 |
| Through Vol | 205 | 238 | 130 | 0 | 286 | 0 |
| RT Vol | 39 | 50 | 0 | 55 | 0 | 51 |
| Lane Flow Rate | 291 | 371 | 188 | 60 | 436 | 56 |
| Geometry Grp | 6 | 6 | 7 | 7 | 7 | 7 |
| Degree of Util (X) | 0.712 | 0.884 | 0.478 | 0.139 | 1.006 | 0.116 |
| Departure Headway (Hd) | 8.807 | 8.572 | 9.156 | 8.302 | 8.305 | 7.436 |
| Convergence, Y/N | Yes | Yes | Yes | Yes | Yes | Yes |
| Cap | 411 | 423 | 393 | 431 | 441 | 483 |
| Service Time | 6.881 | 6.598 | 6.928 | 6.073 | 6.033 | 5.164 |
| HCM Lane V/C Ratio | 0.708 | 0.877 | 0.478 | 0.139 | 0.989 | 0.116 |
| HCM Control Delay | 31 | 49.5 | 20.1 | 12.4 | 73.8 | 11.1 |
| HCM Lane LOS | D | E | C | B | F | B |
| HCM 95th-tile Q | 5.4 | 9.1 | 2.5 | 0.5 | 12.9 | 0.4 |




| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | ${ }_{4}{ }^{2}$ | 444 | 「 | \＃＊ | 444 | 「 | ＊＊ | 444 | 「 | ＊＊ | 4中4 | 「 |
| Traffic Volume（veh／h） | 275 | 1275 | 220 | 332 | 1868 | 115 | 520 | 1030 | 155 | 175 | 820 | 295 |
| Future Volume（veh／h） | 275 | 1275 | 220 | 332 | 1868 | 115 | 520 | 1030 | 155 | 175 | 820 | 295 |
| Initial Q（Qb），veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 0.99 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 0.99 |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow，veh／h／ln | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 |
| Adj Flow Rate，veh／h | 299 | 1386 | 112 | 361 | 2030 | 0 | 565 | 1120 | 0 | 190 | 891 | 212 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh，\％ | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap，veh／h | 327 | 1621 | 496 | 482 | 1931 |  | 517 | 1486 |  | 272 | 1043 | 322 |
| Arrive On Green | 0.09 | 0.32 | 0.32 | 0.14 | 0.38 | 0.00 | 0.15 | 0.29 | 0.00 | 0.08 | 0.20 | 0.20 |
| Sat Flow，veh／h | 3456 | 5106 | 1563 | 3456 | 5106 | 1585 | 3456 | 5106 | 1585 | 3456 | 5106 | 1576 |
| Grp Volume（v），veh／h | 299 | 1386 | 112 | 361 | 2030 | 0 | 565 | 1120 | 0 | 190 | 891 | 212 |
| Grp Sat Flow（s），veh／h／ln | 1728 | 1702 | 1563 | 1728 | 1702 | 1585 | 1728 | 1702 | 1585 | 1728 | 1702 | 1576 |
| Q Serve（g＿s），s | 10.9 | 32.3 | 6.7 | 12.7 | 48.0 | 0.0 | 19.0 | 25.3 | 0.0 | 6.8 | 21.3 | 12.3 |
| Cycle Q Clear（g＿c），s | 10.9 | 32.3 | 6.7 | 12.7 | 48.0 | 0.0 | 19.0 | 25.3 | 0.0 | 6.8 | 21.3 | 12.3 |
| Prop In Lane | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Lane Grp Cap（c），veh／h | 327 | 1621 | 496 | 482 | 1931 |  | 517 | 1486 |  | 272 | 1043 | 322 |
| V／C Ratio（X） | 0.92 | 0.86 | 0.23 | 0.75 | 1.05 |  | 1.09 | 0.75 |  | 0.70 | 0.85 | 0.66 |
| Avail Cap（c＿a），veh／h | 327 | 1690 | 517 | 482 | 1931 |  | 517 | 1486 |  | 299 | 1086 | 335 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter（l） | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay（d），s／veh | 57.0 | 40.6 | 31.9 | 52.5 | 39.5 | 0.0 | 54.0 | 40.9 | 0.0 | 57.0 | 48.7 | 28.4 |
| Incr Delay（d2），s／veh | 28.7 | 4.6 | 0.3 | 5.7 | 35.5 | 0.0 | 67.0 | 2.4 | 0.0 | 4.9 | 6.9 | 5.2 |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ（50\％），veh／In | 5.9 | 13.7 | 2.5 | 5.8 | 25.4 | 0.0 | 12.8 | 10.6 | 0.0 | 3.1 | 9.5 | 5.0 |
| Unsig．Movement Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay（d），s／veh | 85.6 | 45.2 | 32.2 | 58.1 | 75.0 | 0.0 | 121.0 | 43.2 | 0.0 | 61.9 | 55.6 | 33.6 |
| LnGrp LOS | F | D | C | E | F |  | F | D |  | E | E | C |
| Approach Vol，veh／h |  | 1797 |  |  | 2391 | A |  | 1685 | A |  | 1293 |  |
| Approach Delay，s／veh |  | 51.1 |  |  | 72.4 |  |  | 69.3 |  |  | 52.9 |  |
| Approach LOS |  | D |  |  | E |  |  | E |  |  | D |  |


| Timer－Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Phs Duration（G＋Y＋Rc），s | 23.7 | 46.3 | 25.0 | 31.9 | 16.0 | 54.0 | 14.0 | 42.9 |
| Change Period（Y＋Rc），s | 6.0 | 6.0 | 6.0 | $* 6$ | 4.0 | 6.0 | 4.0 | 6.0 |
| Max Green Setting（Gmax），s | 16.0 | 42.0 | 19.0 | $* 27$ | 12.0 | 48.0 | 11.0 | 35.0 |
| Max Q Clear Time（g＿c＋I1），s | 14.7 | 34.3 | 21.0 | 23.3 | 12.9 | 50.0 | 8.8 | 27.3 |
| Green Ext Time（p＿c），s | 0.1 | 6.0 | 0.0 | 2.5 | 0.0 | 0.0 | 0.1 | 4.8 |

## Intersection Summary

| HCM 6th Ctrl Delay | 62.8 |
| :--- | ---: |
| HCM 6th LOS | E |

## Notes

User approved pedestrian interval to be less than phase max green．
＊HCM 6th computational engine requires equal clearance times for the phases crossing the barrier．
Unsignalized Delay for［NBR，WBR］is excluded from calculations of the approach delay and intersection delay．

| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay，s／veh 4 |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \＃ | 中4 | 「 | \＃ | 中 ${ }^{\text {a }}$ |  |  | $\uparrow$ | 「 |  | $\uparrow$ | 「 |
| Traffic Vol，veh／h | 40 | 1433 | 55 | 87 | 1857 | 7 | 20 | 0 | 69 | 0 | 1 | 100 |
| Future Vol，veh／h | 40 | 1433 | 55 | 87 | 1857 | 7 | 20 | 0 | 69 | 0 | 1 | 100 |
| Conflicting Peds，\＃／hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | － | － | None | － | － | None | － | － | None | － | － | None |
| Storage Length | 150 | － | 100 | 175 | － | － | － | － | 125 | － | － | 25 |
| Veh in Median Storage，\＃ | － | 0 | － | － | 0 | － | － | 0 | － | － | 0 | － |
| Grade，\％ | － | 0 | － | － | 0 | － | － | 0 | － | － | 0 | － |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles，\％ | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 43 | 1558 | 60 | 95 | 2018 | 8 | 22 | 0 | 75 | 0 | 1 | 109 |


| Major／Minor | Major1 |  |  |  | Major2 |  |  | Minor1 |  |  | Minor2 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 2026 | 0 | 0 |  | 1618 | 0 |  | 02844 | 3860 | 779 | 3077 | 3916 | 1013 |
| Stage 1 |  | － | － |  | － | － |  | 1644 | 1644 | － | 2212 | 2212 | － |
| Stage 2 |  | － | － |  |  | － |  | 1200 | 2216 | － | 865 | 1704 |  |
| Critical Hdwy | 4.14 | － | － |  | 4.14 | － |  | 7.54 | 6.54 | 6.94 | 7.54 | 6.54 | 6.94 |
| Critical Hdwy Stg 1 |  | － | － |  |  | － |  | 6.54 | 5.54 | － | 6.54 | 5.54 | － |
| Critical Hdwy Stg 2 | － | － | － |  | － | － |  | 6.54 | 5.54 | － | 6.54 | 5.54 | － |
| Follow－up Hdwy | 2.22 | － | － |  | 2.22 | － |  | 3.52 | 4.02 | 3.32 | 3.52 | 4.02 | 3.32 |
| Pot Cap－1 Maneuver | 276 | － | － |  | 399 | － |  | ～ 8 | 4 | 339 | 5 | 3 | 237 |
| Stage 1 |  | － | － |  |  |  |  | 104 | 156 | － | 45 | 80 |  |
| Stage 2 | － | － | － |  | － | － |  | 196 | 80 | － | 315 | 145 | － |
| Platoon blocked，\％ |  | － | － |  |  | － |  | － |  |  |  |  |  |
| Mov Cap－1 Maneuver | 276 | － | － |  | 399 | － |  | $\sim 2$ | 3 | 339 | 3 | 2 | 237 |
| Mov Cap－2 Maneuver | － | － | － |  | － | － |  | $\sim 2$ | 3 | － | 3 | 2 | － |
| Stage 1 | － | － |  |  | － |  |  | 88 | 132 | － | 38 | 61 |  |
| Stage 2 | － | － |  |  | － |  |  | 79 | 61 | － | 207 | 122 | － |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Approach | EB |  |  |  | WB |  |  | NB |  |  | SB |  |  |
| HCM Control Delay，s | 0.5 |  |  |  | 0.7 |  |  | \＄ 1751.9 |  |  | 55.6 |  |  |
| HCM LOS |  |  |  |  |  |  |  | F |  |  | F |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Minor Lane／Major Mvmt | NBLn1 | NBLn2 | EBL | EBT | EBR | WBL | WBT | T WBR | SBLn1 | SBLn2 |  |  |  |
| Capacity（veh／h） | 2 | 339 | 276 | － | － | 399 |  | － | 2 | 237 |  |  |  |
| HCM Lane V／C Ratio | 10.87 | 0.221 | 0.158 | － | － | 0.237 |  |  | 0.543 | 0.459 |  |  |  |
| HCM Control Delay（s） | \＄ 7731.8 | 18.6 | 20.5 | － | － | 16.8 |  | \＄ | 2373.7 | 32.4 |  |  |  |
| HCM Lane LOS | F | C | C |  |  | C |  | －－ | F | D |  |  |  |
| HCM 95th \％otile Q（veh） | 4.3 | 0.8 | 0.6 |  | － | 0.9 |  | －－ | 0.6 | 2.2 |  |  |  |
| Notes |  |  |  |  |  |  |  |  |  |  |  |  |  |
| $\sim$ Volume exceeds cap | \＄：Delay exceeds 300s |  |  |  | ＋：Computation Not Defined |  |  |  | ＊：All major volume in platoon |  |  |  |  |


|  | $y$ |  |  | 7 | $\downarrow$ |  | 4 | 4 |  |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \% | 性 |  | * | 性 |  |  | \$ |  |  | $\uparrow$ | F |
| Traffic Volume (veh/h) | 75 | 1467 | 8 | 5 | 1917 | 85 | 25 | 2 | 9 | 55 | 1 | 50 |
| Future Volume (veh/h) | 75 | 1467 | 8 | 5 | 1917 | 85 | 25 | 2 | 9 | 55 | 1 | 50 |
| Initial $Q(Q b)$, veh | 0 | 0 | O | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 |  | 1.00 | 1.00 |  | 0.98 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow, veh/h/ln | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 |
| Adj Flow Rate, veh/h | 82 | 1595 | 9 | 5 | 2084 | 90 | 27 | 2 | 10 | 60 | 1 | 18 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh, \% | 2 | 2 | , | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap, veh/h | 103 | 2717 | 15 | 7 | 2413 | 103 | 39 | 3 | 14 | 86 | 1 | 78 |
| Arrive On Green | 0.06 | 0.75 | 0.75 | 0.00 | 0.70 | 0.70 | 0.03 | 0.03 | 0.03 | 0.05 | 0.05 | 0.05 |
| Sat Flow, veh/h | 1781 | 3623 | 20 | 1781 | 3468 | 149 | 1198 | 89 | 444 | 1753 | 29 | 1585 |
| Grp Volume(v), veh/h | 82 | 782 | 822 | 5 | 1059 | 1115 | 39 | 0 | 0 | 61 | 0 | 18 |
| Grp Sat Flow(s),veh/h/ln | 1781 | 1777 | 1867 | 1781 | 1777 | 1840 | 1731 | 0 | 0 | 1783 | 0 | 1585 |
| Q Serve(g_s), s | 4.7 | 20.3 | 20.4 | 0.3 | 46.4 | 48.4 | 2.3 | 0.0 | 0.0 | 3.5 | 0.0 | 1.1 |
| Cycle Q Clear(g_c), s | 4.7 | 20.3 | 20.4 | 0.3 | 46.4 | 48.4 | 2.3 | 0.0 | 0.0 | 3.5 | 0.0 | 1.1 |
| Prop In Lane | 1.00 |  | 0.01 | 1.00 |  | 0.08 | 0.69 |  | 0.26 | 0.98 |  | 1.00 |
| Lane Grp Cap(c), veh/h | 103 | 1332 | 1400 | 7 | 1236 | 1280 | 56 | 0 | 0 | 88 | 0 | 78 |
| V/C Ratio(X) | 0.79 | 0.59 | 0.59 | 0.72 | 0.86 | 0.87 | 0.69 | 0.00 | 0.00 | 0.70 | 0.00 | 0.23 |
| Avail Cap(c_a), veh/h | 103 | 1478 | 1552 | 52 | 1426 | 1477 | 301 | 0 | 0 | 448 | 0 | 399 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 0.00 | 1.00 | 0.00 | 1.00 |
| Uniform Delay (d), s/veh | 48.1 | 5.8 | 5.8 | 51.4 | 11.8 | 12.1 | 49.5 | 0.0 | 0.0 | 48.4 | 0.0 | 47.3 |
| Incr Delay (d2), s/veh | 31.1 | 0.5 | 0.5 | 41.0 | 4.8 | 5.3 | 14.1 | 0.0 | 0.0 | 3.7 | 0.0 | 0.6 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile BackOfQ(50\%),veh/ln | 2.9 | 4.6 | 4.8 | 0.2 | 14.1 | 15.3 | 1.2 | 0.0 | 0.0 | 1.6 | 0.0 | 0.5 |
| Unsig. Movement Delay, s/veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay ${ }^{\text {d }}$ ),s/veh | 79.2 | 6.3 | 6.3 | 92.4 | 16.7 | 17.5 | 63.6 | 0.0 | 0.0 | 52.0 | 0.0 | 47.8 |
| LnGrp LOS | E | A | A | F | B | B | E | A | A | D | A | D |
| Approach Vol, veh/h |  | 1686 |  |  | 2179 |  |  | 39 |  |  | 79 |  |
| Approach Delay, s/veh |  | 9.8 |  |  | 17.3 |  |  | 63.6 |  |  | 51.1 |  |
| Approach LOS |  | A |  |  | B |  |  | E |  |  | D |  |
| Timer - Assigned Phs | 1 | 2 |  | 4 | 5 | 6 |  | 8 |  |  |  |  |
| Phs Duration ( $G+Y+R \mathrm{c}$ ), $s$ | 9.0 | 77.9 |  | 8.6 | 3.4 | 83.5 |  | 7.9 |  |  |  |  |
| Change Period ( $\mathrm{Y}+\mathrm{Rc}$ ), s | 3.0 | 6.0 |  | 3.5 | 3.0 | 6.0 |  | 4.5 |  |  |  |  |
| Max Green Setting (Gmax), s | 6.0 | 83.0 |  | 26.0 | 3.0 | 86.0 |  | 18.0 |  |  |  |  |
| Max Q Clear Time (g_c+11), s | 6.7 | 50.4 |  | 5.5 | 2.3 | 22.4 |  | 4.3 |  |  |  |  |
| Green Ext Time (p_c), s | 0.0 | 21.6 |  | 0.2 | 0.0 | 14.9 |  | 0.1 |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 6th Ctrl DelayHCM 6th LOS |  |  | 15.2 |  |  |  |  |  |  |  |  |  |
|  |  |  | B |  |  |  |  |  |  |  |  |  |

## Notes

User approved ignoring U-Turning movement.

| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |


| Major/Minor | Major1 |  | Major2 | Minor1 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 0 | 0 | 1655 | 0 |  | 828 |
| Stage 1 |  |  |  | - |  |  |
| Stage 2 |  | - |  | - |  |  |
| Critical Hdwy |  |  | 4.14 | - |  | 6.94 |
| Critical Hdwy Stg 1 | - | - | - | - |  |  |
| Critical Hdwy Stg 2 | - | - | - | - |  |  |
| Follow-up Hdwy | - | - | 2.22 | - | - | 3.32 |
| Pot Cap-1 Maneuver | - | - | 386 | - | 0 | 314 |
| Stage 1 |  | - |  | - | 0 |  |
| Stage 2 |  | - |  | - | 0 |  |
| Platoon blocked, \% |  | - |  | - |  |  |
| Mov Cap-1 Maneuver |  |  | 386 | - | - | 314 |
| Mov Cap-2 Maneuver | - | - | - | - | - |  |
| Stage 1 |  | - |  | - | - |  |
| Stage 2 | - | - | - | - | - |  |


|  | EB | WB | NB |
| :--- | ---: | ---: | ---: |
| Approach | 0 | 0.6 | 21.2 |
| HCM Control Delay, $s$ | 0 | $C$ |  |



| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay，s／veh | 1.7 |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ＊ | 性 |  | \％ | 性 |  |  |  | 「 |  |  | 「 |
| Traffic Vol，veh／h | 107 | 1428 | 15 | 75 | 1850 | 7 | 0 | 0 | 2 | 0 | 0 | 90 |
| Future Vol，veh／h | 107 | 1428 | 15 | 75 | 1850 | 7 | 0 | 0 | 2 | 0 | 0 | 90 |
| Conflicting Peds，\＃／hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | － | － | None | － | － | None | － |  | None | － | － | None |
| Storage Length | 250 | － | － | 325 | － | － | － | － | 0 | － | － | 0 |
| Veh in Median Storage，\＃ | － | 0 | － | － | 0 |  |  | 0 |  |  | 0 | － |
| Grade，\％ | － | 0 | － | － | 0 | － | － | 0 | － |  | 0 | － |
| Peak Hour Factor | 96 | 96 | 96 | 96 | 96 | 96 | 96 | 96 | 96 | 96 | 96 | 96 |
| Heavy Vehicles，\％ | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| Mumt Flow | 111 | 1488 | 16 | 78 | 1927 | 7 | 0 | 0 | 2 | 0 | 0 | 94 |



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations |  | 个个 | 「 | 离 | 个4 | F | ${ }^{7}$ | $\uparrow$ | 「 | \％ | $\uparrow$ | F |
| Traffic Volume（veh／h） | 65 | 1239 | 134 | 150 | 1643 | 175 | 210 | 195 | 115 | 225 | 165 | 40 |
| Future Volume（veh／h） | 65 | 1239 | 134 | 150 | 1643 | 175 | 210 | 195 | 115 | 225 | 165 | 40 |
| Initial $Q(Q b)$ ，veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 1.00 | 1.00 |  | 0.98 | 1.00 |  | 1.00 | 1.00 |  | 0.99 |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow，veh／h／ln | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 |
| Adj Flow Rate，veh／h | 69 | 1318 | 90 | 160 | 1748 | 80 | 215 | 218 | 0 | 208 | 220 | 14 |
| Peak Hour Factor | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 |
| Percent Heavy Veh，\％ | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| Cap，veh／h | 89 | 1663 | 742 | 189 | 1862 | 812 | 246 | 258 |  | 241 | 253 | 211 |
| Arrive On Green | 0.05 | 0.46 | 0.46 | 0.11 | 0.52 | 0.52 | 0.14 | 0.14 | 0.00 | 0.13 | 0.13 | 0.13 |
| Sat Flow，veh／h | 1795 | 3582 | 1598 | 1795 | 3582 | 1562 | 1795 | 1885 | 1598 | 1795 | 1885 | 1576 |
| Grp Volume（v），veh／h | 69 | 1318 | 90 | 160 | 1748 | 80 | 215 | 218 | 0 | 208 | 220 | 14 |
| Grp Sat Flow（s），veh／h／ln | 1795 | 1791 | 1598 | 1795 | 1791 | 1562 | 1795 | 1885 | 1598 | 1795 | 1885 | 1576 |
| Q Serve（g＿s），s | 4.2 | 34.8 | 3.6 | 9.8 | 51.0 | 2.9 | 13.1 | 12.6 | 0.0 | 12.7 | 12.8 | 0.9 |
| Cycle Q Clear（g＿c），s | 4.2 | 34.8 | 3.6 | 9.8 | 51.0 | 2.9 | 13.1 | 12.6 | 0.0 | 12.7 | 12.8 | 0.9 |
| Prop In Lane | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Lane Grp Cap（c），veh／h | 89 | 1663 | 742 | 189 | 1862 | 812 | 246 | 258 |  | 241 | 253 | 211 |
| V／C Ratio（X） | 0.78 | 0.79 | 0.12 | 0.85 | 0.94 | 0.10 | 0.87 | 0.84 |  | 0.86 | 0.87 | 0.07 |
| Avail Cap（c＿a），veh／h | 113 | 2331 | 1040 | 290 | 2684 | 1170 | 467 | 490 |  | 364 | 382 | 319 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter（l） | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay（d），s／veh | 52.4 | 25.3 | 17.0 | 49.0 | 25.1 | 13.5 | 47.2 | 47.0 | 0.0 | 47.3 | 47.3 | 42.2 |
| Incr Delay（d2），s／veh | 17.4 | 0.8 | 0.0 | 8.4 | 4.5 | 0.0 | 3.8 | 2.9 | 0.0 | 8.8 | 9.1 | 0.0 |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ（50\％），veh／ln | 2.3 | 13.3 | 1.2 | 4.6 | 20.1 | 0.9 | 6.0 | 6.0 | 0.0 | 6.2 | 6.5 | 0.3 |
| Unsig．Movement Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay（d），s／veh | 69.9 | 26.2 | 17.0 | 57.4 | 29.7 | 13.6 | 51.0 | 49.9 | 0.0 | 56.1 | 56.4 | 42.2 |
| LnGrp LOS | E | C | B | E | C | B | D | D |  | E | E | D |
| Approach Vol，veh／h |  | 1477 |  |  | 1988 |  |  | 433 | A |  | 442 |  |
| Approach Delay，s／veh |  | 27.6 |  |  | 31.2 |  |  | 50.4 |  |  | 55.8 |  |
| Approach LOS |  | C |  |  | C |  |  | D |  |  | E |  |


| Timer－Assigned Phs | 1 | 2 | 4 | 5 | 6 | 8 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Phs Duration $(G+Y+R c)$ ，s | 14.7 | 57.8 | 19.4 | 8.5 | 64.0 | 19.7 |
| Change Period（Y＋Rc），s | 3.0 | 6.0 | 4.4 | 3.0 | 6.0 | 4.4 |
| Max Green Setting（Gmax），s | 18.0 | 72.6 | 22.6 | 7.0 | 83.6 | 29.0 |
| Max Q Clear Time（g＿c＋11），s | 11.8 | 36.8 | 14.8 | 6.2 | 53.0 | 15.1 |
| Green Ext Time（p＿C），s | 0.0 | 3.0 | 0.2 | 0.0 | 4.9 | 0.2 |

## Intersection Summary

| HCM 6th Ctrl Delay | 34.4 |
| :--- | ---: |
| HCM 6th LOS | C |

## Notes

User approved pedestrian interval to be less than phase max green．
User approved volume balancing among the lanes for turning movement．
Unsignalized Delay for［NBR］is excluded from calculations of the approach delay and intersection delay．

|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |

Unsignalized Delay for [NBR, EBR, WBR, SBR] is excluded from calculations of the approach delay and intersection delay.




| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | ＊＊ | 中4去 | F | ${ }^{\text {a }}$ | 帆 | 「 | ${ }^{\text {a }}$ | 帆 | 「 | ${ }^{\text {a }}$ | 个4ヶ | 「 |
| Traffic Volume（veh／h） | 545 | 1665 | 325 | 427 | 1526 | 240 | 470 | 1140 | 268 | 251 | 1060 | 220 |
| Future Volume（veh／h） | 545 | 1665 | 325 | 427 | 1526 | 240 | 470 | 1140 | 268 | 251 | 1060 | 220 |
| Initial $Q(Q b)$ ，veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow，veh／h／ln | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 |
| Adj Flow Rate，veh／h | 580 | 1771 | 133 | 454 | 1623 | 0 | 500 | 1213 | 0 | 267 | 1128 | 207 |
| Peak Hour Factor | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 |
| Percent Heavy Veh，\％ | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| Cap，veh／h | 604 | 1784 | 553 | 488 | 1681 |  | 511 | 1426 |  | 312 | 1132 | 351 |
| Arrive On Green | 0.17 | 0.35 | 0.35 | 0.14 | 0.33 | 0.00 | 0.20 | 0.37 | 0.00 | 0.06 | 0.15 | 0.15 |
| Sat Flow，veh／h | 3483 | 5147 | 1596 | 3483 | 5147 | 1598 | 3483 | 5147 | 1598 | 3483 | 5147 | 1595 |
| Grp Volume（v），veh／h | 580 | 1771 | 133 | 454 | 1623 | 0 | 500 | 1213 | 0 | 267 | 1128 | 207 |
| Grp Sat Flow（s），veh／h／ln | 1742 | 1716 | 1596 | 1742 | 1716 | 1598 | 1742 | 1716 | 1598 | 1742 | 1716 | 1595 |
| Q Serve（g＿s），s | 24.8 | 51.4 | 6.0 | 19.3 | 46.5 | 0.0 | 21.4 | 32.5 | 0.0 | 11.4 | 32.9 | 18.2 |
| Cycle Q Clear（g＿c），s | 24.8 | 51.4 | 6.0 | 19.3 | 46.5 | 0.0 | 21.4 | 32.5 | 0.0 | 11.4 | 32.9 | 18.2 |
| Prop In Lane | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Lane Grp Cap（c），veh／h | 604 | 1784 | 553 | 488 | 1681 |  | 511 | 1426 |  | 312 | 1132 | 351 |
| V／C Ratio（X） | 0.96 | 0.99 | 0.24 | 0.93 | 0.97 |  | 0.98 | 0.85 |  | 0.86 | 1.00 | 0.59 |
| Avail Cap（c＿a），veh／h | 604 | 1784 | 553 | 488 | 1681 |  | 511 | 1426 |  | 325 | 1132 | 351 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.33 | 1.33 | 1.33 | 0.67 | 0.67 | 0.67 |
| Upstream Filter（l） | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay（d），s／veh | 61.5 | 48.8 | 15.8 | 63.8 | 49.7 | 0.0 | 60.1 | 44.5 | 0.0 | 69.5 | 63.9 | 57.6 |
| Incr Delay（d2），s／veh | 26.8 | 19.6 | 1.0 | 24.4 | 15.1 | 0.0 | 34.1 | 5.2 | 0.0 | 18.0 | 25.8 | 3.2 |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ（50\％），veh／ln | 13.0 | 24.5 | 3.5 | 10.1 | 21.7 | 0.0 | 11.3 | 13.4 | 0.0 | 5.9 | 17.3 | 7.8 |
| Unsig．Movement Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay（d），s／veh | 88.3 | 68.4 | 16.9 | 88.2 | 64.8 | 0.0 | 94.3 | 49.7 | 0.0 | 87.6 | 89.7 | 60.8 |
| LnGrp LOS | F | E | B | F | E |  | F | D |  | F | F | E |
| Approach Vol，veh／h |  | 2484 |  |  | 2077 | A |  | 1713 | A |  | 1602 |  |
| Approach Delay，s／veh |  | 70.3 |  |  | 69.9 |  |  | 62.7 |  |  | 85.6 |  |
| Approach LOS |  | E |  |  | E |  |  | E |  |  | F |  |


|  |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Timer－Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| Phs Duration $(\mathbf{G}+\mathrm{Y}+\mathrm{Rc}$ ），s | 27.0 | 58.0 | 26.0 | 39.0 | 30.0 | 55.0 | 17.4 | 47.6 |
| Change Period $(\mathrm{Y}+\mathrm{Rc}$ ），s | 6.0 | 6.0 | 4.0 | 6.0 | 4.0 | 6.0 | 4.0 | 6.0 |
| Max Green Setting（Gmax），s | 21.0 | 52.0 | 22.0 | 33.0 | 26.0 | 49.0 | 14.0 | 41.0 |
| Max Q Clear Time（g＿c＋11），s | 21.3 | 53.4 | 23.4 | 34.9 | 26.8 | 48.5 | 13.4 | 34.5 |
| Green Ext Time（p＿c），s | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.4 | 0.0 | 4.4 |

## Intersection Summary

HCM 6th Ctrl Delay 71.7
HCM 6th LOS
E

## Notes

User approved pedestrian interval to be less than phase max green．
Unsignalized Delay for［NBR，WBR］is excluded from calculations of the approach delay and intersection delay．

| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ＊ | 性 | 「 | \＃ | 性 |  |  | $\uparrow$ | 「 |  | $\uparrow$ | F |
| Traffic Vol，veh／h | 45 | 2003 | 70 | 52 | 1785 | 4 | 15 | 0 | 50 | 0 | 1 | 40 |
| Future Vol，veh／h | 45 | 2003 | 70 | 52 | 1785 | 4 | 15 | 0 | 50 | 0 | 1 | 40 |
| Conflicting Peds，\＃hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | － | － | None | － |  | None | ． |  | None | － | － | None |
| Storage Length | 150 | － | 100 | 175 |  | － |  | － | 125 | － | － | 25 |
| Veh in Median Storage，\＃ |  | 0 | － | － | 0 | － |  | 0 |  |  | 0 |  |
| Grade，\％ |  | 0 | － | － | 0 | － |  | 0 | － |  | 0 | － |
| Peak Hour Factor | 94 | 94 | 94 | 94 | 94 | 94 | 94 | 94 | 94 | 94 | 94 | 94 |
| Heavy Vehicles，\％ | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| Mumt Flow | 48 | 2131 | 74 | 55 | 1899 | 4 | 16 | 0 | 53 | 0 | 1 | 43 |



|  | 4 |  |  | $t$ | - |  | 4 | 4 | $p$ |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | $\stackrel{y}{4}$ | 中t |  | \% | 个t |  |  | $\dagger$ |  |  | $\uparrow$ | F |
| Traffic Volume (veh/h) | 55 | 2033 | 30 | 9 | 1803 | 20 | 20 | 0 | 6 | 30 | 1 | 25 |
| Future Volume (veh/h) | 55 | 2033 | 30 | 9 | 1803 | 20 | 20 | 0 | 6 | 30 | 1 | 25 |
| Initial $\mathrm{Q}(\mathrm{Qb})$, veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 |  | 1.00 | 1.00 |  | 0.98 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow, veh/h/ln | 1885 | 1885 | 1885 | 1870 | 1885 | 1885 | 1870 | 1870 | 1870 | 1870 | 1870 | 1885 |
| Adj Flow Rate, veh/h | 59 | 2163 | 33 | 10 | 1918 | 21 | 22 | 0 | 7 | 32 | 1 | 6 |
| Peak Hour Factor | 0.94 | 0.94 | 0.92 | 0.92 | 0.94 | 0.94 | 0.92 | 0.92 | 0.92 | 0.94 | 0.92 | 0.94 |
| Percent Heavy Veh, \% | 1 | 1 | 1 | 2 | 1 | 1 | 2 | 2 | 2 | 2 | 2 | 1 |
| Cap, veh/h | 60 | 2897 | 44 | 12 | 2815 | 31 | 31 | 0 | 10 | 65 | 2 | 60 |
| Arrive On Green | 0.03 | 0.80 | 0.80 | 0.01 | 0.78 | 0.78 | 0.02 | 0.00 | 0.02 | 0.04 | 0.04 | 0.04 |
| Sat Flow, veh/h | 1795 | 3611 | 55 | 1781 | 3628 | 40 | 1312 | 0 | 417 | 1730 | 54 | 1598 |
| Grp Volume(v), veh/h | 59 | 1070 | 1126 | 10 | 945 | 994 | 29 | 0 | 0 | 33 | 0 | 6 |
| Grp Sat Flow(s),veh/h/ln | 1795 | 1791 | 1875 | 1781 | 1791 | 1877 | 1730 | 0 | 0 | 1784 | 0 | 1598 |
| Q Serve(g_s), s | 4.9 | 44.0 | 44.6 | 0.8 | 37.5 | 37.9 | 2.5 | 0.0 | 0.0 | 2.7 | 0.0 | 0.5 |
| Cycle Q Clear(g_c), s | 4.9 | 44.0 | 44.6 | 0.8 | 37.5 | 37.9 | 2.5 | 0.0 | 0.0 | 2.7 | 0.0 | 0.5 |
| Prop In Lane | 1.00 |  | 0.03 | 1.00 |  | 0.02 | 0.76 |  | 0.24 | 0.97 |  | 1.00 |
| Lane Grp Cap(c), veh/h | 60 | 1437 | 1505 | 12 | 1389 | 1456 | 40 | 0 | 0 | 67 | 0 | 60 |
| V/C Ratio(X) | 0.99 | 0.74 | 0.75 | 0.82 | 0.68 | 0.68 | 0.72 | 0.00 | 0.00 | 0.49 | 0.00 | 0.10 |
| Avail Cap(c_a), veh/h | 60 | 1437 | 1505 | 36 | 1389 | 1456 | 209 | 0 | 0 | 309 | 0 | 277 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 0.00 | 1.00 | 0.00 | 1.00 |
| Uniform Delay (d), s/veh | 72.5 | 7.3 | 7.3 | 74.4 | 8.0 | 8.0 | 72.8 | 0.0 | 0.0 | 70.8 | 0.0 | 69.7 |
| Incr Delay (d2), s/veh | 110.9 | 3.5 | 3.5 | 37.6 | 2.7 | 2.6 | 20.9 | 0.0 | 0.0 | 5.5 | 0.0 | 0.7 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile BackOfQ(50\%),veh/ln | 4.1 | 12.7 | 13.4 | 0.5 | 11.7 | 12.4 | 1.4 | 0.0 | 0.0 | 1.4 | 0.0 | 0.2 |
| Unsig. Movement Delay, s/veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay (d),s/veh | 183.3 | 10.8 | 10.8 | 112.0 | 10.7 | 10.6 | 93.7 | 0.0 | 0.0 | 76.3 | 0.0 | 70.5 |
| LnGrp LOS | F | B | B | F | B | B | F | A | A | E | A | E |
| Approach Vol, veh/h |  | 2255 |  |  | 1949 |  |  | 29 |  |  | 39 |  |
| Approach Delay, s/veh |  | 15.3 |  |  | 11.2 |  |  | 93.7 |  |  | 75.4 |  |
| Approach LOS |  | B |  |  | B |  |  | F |  |  | E |  |
| Timer - Assigned Phs | 1 | 2 |  | 4 | 5 | 6 |  | 8 |  |  |  |  |
| Phs Duration ( $G+Y+R \mathrm{c}$ ), $s$ | 8.0 | 122.4 |  | 11.6 | 4.0 | 126.3 |  | 8.0 |  |  |  |  |
| Change Period ( $\mathrm{Y}+\mathrm{Rc}$ ), s | 3.0 | 6.0 |  | 6.0 | 3.0 | 6.0 |  | 4.5 |  |  |  |  |
| Max Green Setting (Gmax), s | 5.0 | 81.4 |  | 26.0 | 3.0 | 83.4 |  | 18.1 |  |  |  |  |
| Max Q Clear Time (g_c+11), s | 6.9 | 39.9 |  | 4.7 | 2.8 | 46.6 |  | 4.5 |  |  |  |  |
| Green Ext Time (p_c), s | 0.0 | 20.0 |  | 0.1 | 0.0 | 23.6 |  | 0.1 |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 6th Ctrr Delay |  |  | 14.5 |  |  |  |  |  |  |  |  |  |
| HCM 6th LOS |  |  | B |  |  |  |  |  |  |  |  |  |

## Notes

User approved ignoring U-Turning movement.

| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |


| Major/Minor | Major1 | Major2 |  | Minor1 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 0 | 0 | 2172 | 0 |  | 1086 |
| Stage 1 | - |  |  |  |  |  |
| Stage 2 |  | - |  |  |  |  |
| Critical Hdwy | - |  | 4.14 | - | - | 6.94 |
| Critical Hdwy Stg 1 | - | - | - | - | - |  |
| Critical Hdwy Stg 2 | - | - |  | - | - |  |
| Follow-up Hdwy | - | - | 2.22 | - | - | 3.32 |
| Pot Cap-1 Maneuver | - | - | 242 | - | 0 | 212 |
| Stage 1 | - | - | - | - | 0 |  |
| Stage 2 |  | - |  | - | 0 |  |
| Platoon blocked, \% |  | - |  | - |  |  |
| Mov Cap-1 Maneuver | - |  | 242 | - | - | 212 |
| Mov Cap-2 Maneuver | - | - | - | - | - |  |
| Stage 1 | - | - |  | - | - |  |
| Stage 2 | - | - | - | - | - |  |


| Approach | EB | WB | NB |
| :--- | ---: | ---: | ---: |
| HCM Control Delay, s | 0 | 0.7 | 56 |
| HCM LOS |  |  | F |


| Minor Lane/Major Mvmt | NBLn1 | EBT | EBR | WBL | WBT |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Capacity (veh/h) | 212 | - | - | 242 | - |  |
| HCM Lane V/C Ratio | 0.718 | - | - | 0.247 | - |  |
| HCM Control Delay (s) | 56 | - | - | 24.7 | - |  |
| HCM Lane LOS | F | - | - | C | - |  |
| HCM 95th \%tile $Q$ (veh) | 4.7 | - | - | 0.9 | - |  |


| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ＊ | 性 |  | \％ | 性 |  |  |  | F |  |  | 「 |
| Traffic Vol，veh／h | 138 | 1930 | 30 | 55 | 1750 | 21 | 0 | 0 | 15 | 0 | 0 | 73 |
| Future Vol，veh／h | 138 | 1930 | 30 | 55 | 1750 | 21 | 0 | 0 | 15 | 0 | 0 | 73 |
| Conflicting Peds，\＃／hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | － | － | None | － | － | None | － |  | None | － | － | None |
| Storage Length | 250 | － | － | 325 | － | － | － |  | 0 | － | － | 0 |
| Veh in Median Storage，\＃ | － | 0 | － | － | 0 |  |  | 0 |  | － | 0 | － |
| Grade，\％ | － | 0 | － | － | 0 | － | － | 0 | － | － | 0 | － |
| Peak Hour Factor | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 |
| Heavy Vehicles，\％ | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| Mumt Flow | 145 | 2032 | 32 | 58 | 1842 | 22 | 0 | 0 | 16 | 0 | 0 | 77 |



Stage 2

| Approach | EB | WB | NB | SB |
| :--- | :--- | :---: | :---: | :---: |
| HCM Control Delay，s | 1.6 | 0.7 | 21.6 | 23.6 |
| HCM LOS |  |  | C | C |


| Minor Lane／Major Mvmt | NBLn1 | EBL | EBT | EBR | WBL | WBT | WBR SBLn1 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Capacity（veh／h） | 232 | 324 | - | -271 | - | -270 |  |
| HCM Lane V／C Ratio | 0.068 | 0.448 | - | -0.214 | - | -0.285 |  |
| HCM Control Delay（s） | 21.6 | 24.8 | - | - | 21.9 | - | -23.6 |
| HCM Lane LOS | C | C | - | - | C | - | - |
| HCM 95th \％tile Q（veh） | 0.2 | 2.2 | - | - | 0.8 | - | -1.1 |


| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | $\stackrel{y}{4}$ | 个 $\uparrow$ | 「 | \％ | 个 $\uparrow$ | F | ${ }^{*}$ | $\uparrow$ | 「 | ${ }^{7}$ | $\uparrow$ | 「 |
| Traffic Volume（veh／h） | 75 | 1678 | 192 | 135 | 1528 | 220 | 158 | 150 | 145 | 245 | 155 | 65 |
| Future Volume（veh／h） | 75 | 1678 | 192 | 135 | 1528 | 220 | 158 | 150 | 145 | 245 | 155 | 65 |
| Initial $Q(Q b)$ ，veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 0.98 | 1.00 |  | 0.92 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow，veh／h／ln | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Adj Flow Rate，veh／h | 77 | 1730 | 146 | 139 | 1575 | 185 | 159 | 161 | 0 | 206 | 225 | 22 |
| Peak Hour Factor | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 |
| Percent Heavy Veh，\％ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Cap，veh／h | 99 | 1836 | 802 | 167 | 1972 | 814 | 191 | 200 |  | 245 | 257 | 218 |
| Arrive On Green | 0.05 | 0.51 | 0.51 | 0.09 | 0.55 | 0.55 | 0.11 | 0.11 | 0.00 | 0.14 | 0.14 | 0.14 |
| Sat Flow，veh／h | 1810 | 3610 | 1577 | 1810 | 3610 | 1489 | 1810 | 1900 | 1610 | 1810 | 1900 | 1610 |
| Grp Volume（v），veh／h | 77 | 1730 | 146 | 139 | 1575 | 185 | 159 | 161 | 0 | 206 | 225 | 22 |
| Grp Sat Flow（s），veh／h／ln | 1810 | 1805 | 1577 | 1810 | 1805 | 1489 | 1810 | 1900 | 1610 | 1810 | 1900 | 1610 |
| Q Serve（g＿s），s | 4.7 | 50.7 | 5.6 | 8.5 | 39.4 | 7.2 | 9.7 | 9.3 | 0.0 | 12.5 | 13.0 | 1.3 |
| Cycle Q Clear（g＿c），s | 4.7 | 50.7 | 5.6 | 8.5 | 39.4 | 7.2 | 9.7 | 9.3 | 0.0 | 12.5 | 13.0 | 1.3 |
| Prop In Lane | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Lane Grp Cap（c），veh／h | 99 | 1836 | 802 | 167 | 1972 | 814 | 191 | 200 |  | 245 | 257 | 218 |
| V／C Ratio（X） | 0.78 | 0.94 | 0.18 | 0.83 | 0.80 | 0.23 | 0.83 | 0.80 |  | 0.84 | 0.88 | 0.10 |
| Avail Cap（c＿a），veh／h | 145 | 2337 | 1021 | 194 | 2433 | 1004 | 468 | 491 |  | 300 | 315 | 267 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter（1） | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay（d），s／veh | 52.4 | 26.0 | 14.9 | 50.1 | 20.5 | 13.2 | 49.2 | 49.0 | 0.0 | 47.3 | 47.6 | 42.5 |
| Incr Delay（d2），s／veh | 8.2 | 6.7 | 0.0 | 20.4 | 1.3 | 0.1 | 3.6 | 2.9 | 0.0 | 13.9 | 17.8 | 0.1 |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \％oile BackOfQ（50\％），veh／ln | 2.3 | 20.5 | 1.8 | 4.6 | 14.8 | 2.2 | 4.5 | 4.5 | 0.0 | 6.5 | 7.3 | 0.5 |
| Unsig．Movement Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay（d），s／veh | 60.5 | 32.7 | 15.0 | 70.4 | 21.7 | 13.2 | 52.9 | 51.9 | 0.0 | 61.2 | 65.4 | 42.6 |
| LnGrp LOS | E | C | B | E | C | B | D | D |  | E | E | D |
| Approach Vol，veh／h |  | 1953 |  |  | 1899 |  |  | 320 | A |  | 453 |  |
| Approach Delay，s／veh |  | 32.4 |  |  | 24.5 |  |  | 52.4 |  |  | 62.4 |  |
| Approach LOS |  | C |  |  | C |  |  | D |  |  | E |  |


| Timer－Assigned Phs | 1 | 2 | 4 | 5 | 6 | 8 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Phs Duration $(G+Y+R c)$ ，s | 13.3 | 63.0 | 19.6 | 9.1 | 67.3 | 16.2 |
| Change Period（Y＋Rc），s | 3.0 | 6.0 | 4.4 | 3.0 | 6.0 | 4.4 |
| Max Green Setting（Gmax），s | 12.0 | 72.6 | 18.6 | 9.0 | 75.6 | 29.0 |
| Max Q Clear Time（g＿c＋11），s | 10.5 | 52.7 | 15.0 | 6.7 | 41.4 | 11.7 |
| Green Ext Time（p＿C），s | 0.0 | 4.3 | 0.1 | 0.0 | 4.3 | 0.1 |

## Intersection Summary

| HCM 6th Ctrl Delay | 33.5 |
| :--- | ---: |
| HCM 6th LOS | C |

## Notes

User approved pedestrian interval to be less than phase max green．
User approved volume balancing among the lanes for turning movement．
Unsignalized Delay for［NBR］is excluded from calculations of the approach delay and intersection delay．

## $\rightarrow \rightarrow\rangle \vdash \leftarrow \uparrow \uparrow \uparrow \vdash \downarrow \downarrow \downarrow$




## Notes

User approved pedestrian interval to be less than phase max green.
User approved volume balancing among the lanes for turning movement.

* HCM 6th computational engine requires equal clearance times for the phases crossing the barrier.

Unsignalized Delay for [NBR, EBR, WBR, SBR] is excluded from calculations of the approach delay and intersection delay.




| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | ＊＊ | 帆 | 「 | ${ }^{\text {® }}$ | 帆 | 「 | ＊＊ | 帆4 | 「 | ${ }^{1}$ | 个4ヶ | 「 |
| Traffic Volume（veh／h） | 310 | 1290 | 220 | 333 | 1870 | 115 | 520 | 1030 | 160 | 176 | 820 | 295 |
| Future Volume（veh／h） | 310 | 1290 | 220 | 333 | 1870 | 115 | 520 | 1030 | 160 | 176 | 820 | 295 |
| Initial $Q(Q b)$ ，veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 0.99 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 0.99 |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow，veh／h／ln | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 |
| Adj Flow Rate，veh／h | 337 | 1402 | 112 | 362 | 2033 | 0 | 565 | 1120 | 0 | 191 | 891 | 212 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh，\％ | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap，veh／h | 327 | 1628 | 498 | 478 | 1931 |  | 517 | 1486 |  | 272 | 1043 | 322 |
| Arrive On Green | 0.09 | 0.32 | 0.32 | 0.14 | 0.38 | 0.00 | 0.15 | 0.29 | 0.00 | 0.08 | 0.20 | 0.20 |
| Sat Flow，veh／h | 3456 | 5106 | 1563 | 3456 | 5106 | 1585 | 3456 | 5106 | 1585 | 3456 | 5106 | 1576 |
| Grp Volume（v），veh／h | 337 | 1402 | 112 | 362 | 2033 | 0 | 565 | 1120 | 0 | 191 | 891 | 212 |
| Grp Sat Flow（s），veh／h／ln | 1728 | 1702 | 1563 | 1728 | 1702 | 1585 | 1728 | 1702 | 1585 | 1728 | 1702 | 1576 |
| Q Serve（g＿s），s | 12.0 | 32.7 | 6.7 | 12.8 | 48.0 | 0.0 | 19.0 | 25.3 | 0.0 | 6.8 | 21.3 | 12.3 |
| Cycle Q Clear（g＿c），s | 12.0 | 32.7 | 6.7 | 12.8 | 48.0 | 0.0 | 19.0 | 25.3 | 0.0 | 6.8 | 21.3 | 12.3 |
| Prop In Lane | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Lane Grp Cap（c），veh／h | 327 | 1628 | 498 | 478 | 1931 |  | 517 | 1486 |  | 272 | 1043 | 322 |
| V／C Ratio（X） | 1.03 | 0.86 | 0.22 | 0.76 | 1.05 |  | 1.09 | 0.75 |  | 0.70 | 0.85 | 0.66 |
| Avail Cap（c＿a），veh／h | 327 | 1690 | 517 | 478 | 1931 |  | 517 | 1486 |  | 299 | 1086 | 335 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter（l） | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay（d），s／veh | 57.5 | 40.6 | 31.7 | 52.6 | 39.5 | 0.0 | 54.0 | 40.9 | 0.0 | 57.0 | 48.7 | 28.4 |
| Incr Delay（d2），s／veh | 58.1 | 4.9 | 0.3 | 6.2 | 36.0 | 0.0 | 67.0 | 2.4 | 0.0 | 5.0 | 6.9 | 5.2 |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ（50\％），veh／ln | 7.8 | 13.9 | 2.5 | 5.8 | 25.4 | 0.0 | 12.8 | 10.6 | 0.0 | 3.1 | 9.5 | 5.0 |
| Unsig．Movement Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay（d），s／veh | 115.6 | 45.5 | 32.1 | 58.8 | 75.5 | 0.0 | 121.0 | 43.2 | 0.0 | 62.0 | 55.6 | 33.6 |
| LnGrp LOS | F | D | C | E | F |  | F | D |  | E | E | C |
| Approach Vol，veh／h |  | 1851 |  |  | 2395 | A |  | 1685 | A |  | 1294 |  |
| Approach Delay，s／veh |  | 57.4 |  |  | 73.0 |  |  | 69.3 |  |  | 52.9 |  |
| Approach LOS |  | E |  |  | E |  |  | E |  |  | D |  |


|  |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Timer－Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| Phs Duration $(\mathrm{G}+\mathrm{Y}+\mathrm{Rc}$ ），s | 23.5 | 46.5 | 25.0 | 31.9 | 16.0 | 54.0 | 14.0 | 42.9 |
| Change Period $(\mathrm{Y}+\mathrm{Rc}$ ），s | 6.0 | 6.0 | 6.0 | $* 6$ | 4.0 | 6.0 | 4.0 | 6.0 |
| Max Green Setting（Gmax），s | 16.0 | 42.0 | 19.0 | $* 27$ | 12.0 | 48.0 | 11.0 | 35.0 |
| Max Q Clear Time（g＿c＋11），s | 14.8 | 34.7 | 21.0 | 23.3 | 14.0 | 50.0 | 8.8 | 27.3 |
| Green Ext Time（p＿c），s | 0.1 | 5.7 | 0.0 | 2.5 | 0.0 | 0.0 | 0.1 | 4.8 |

## Intersection Summary

| HCM 6th Ctrl Delay | 64.5 |
| :--- | ---: |
| HCM 6th LOS | $E$ |

## Notes

User approved pedestrian interval to be less than phase max green．
＊HCM 6th computational engine requires equal clearance times for the phases crossing the barrier．
Unsignalized Delay for［NBR，WBR］is excluded from calculations of the approach delay and intersection delay．

| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \＃ | 中4 | 「 | \＃ | 中 ${ }^{\text {a }}$ |  |  | $\uparrow$ | 「 |  | $\uparrow$ | 「 |
| Traffic Vol，veh／h | 40 | 1480 | 55 | 85 | 1860 | 7 | 20 | 0 | 70 | 0 | 1 | 100 |
| Future Vol，veh／h | 40 | 1480 | 55 | 85 | 1860 | 7 | 20 | 0 | 70 | 0 | 1 | 100 |
| Conflicting Peds，\＃／hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | － | － | None | － | － | None | － | － | None | － | － | None |
| Storage Length | 150 | － | 100 | 175 | － | － | － | － | 125 | － | － | 25 |
| Veh in Median Storage，\＃ | － | 0 | － | － | 0 | － | － | 0 | － | － | 0 | － |
| Grade，\％ | － | 0 | － | － | 0 | － | － | 0 | － | － | 0 | － |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles，\％ | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 43 | 1609 | 60 | 92 | 2022 | 8 | 22 | 0 | 76 | 0 | 1 | 109 |



|  | $y$ |  |  | 7 | $\downarrow$ |  | 4 | 4 |  |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \% | 性 |  | * | 性 |  |  | \$ |  |  | $\uparrow$ | F |
| Traffic Volume (veh/h) | 75 | 1490 | 8 | 5 | 1920 | 85 | 25 | 2 | 9 | 55 | 1 | 50 |
| Future Volume (veh/h) | 75 | 1490 | 8 | 5 | 1920 | 85 | 25 | 2 | 9 | 55 | 1 | 50 |
| Initial $Q(Q b)$, veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 |  | 1.00 | 1.00 |  | 0.98 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow, veh/h/ln | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 |
| Adj Flow Rate, veh/h | 82 | 1620 | 9 | 5 | 2087 | 90 | 27 | 2 | 10 | 60 | 1 | 18 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh, \% | 2 | 2 | , |  | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap, veh/h | 103 | 2718 | 15 | 7 | 2415 | 103 | 39 | 3 | 14 | 86 | 1 | 78 |
| Arrive On Green | 0.06 | 0.75 | 0.75 | 0.00 | 0.70 | 0.70 | 0.03 | 0.03 | 0.03 | 0.05 | 0.05 | 0.05 |
| Sat Flow, veh/h | 1781 | 3623 | 20 | 1781 | 3468 | 148 | 1198 | 89 | 444 | 1753 | 29 | 1585 |
| Grp Volume(v), veh/h | 82 | 794 | 835 | 5 | 1061 | 1116 | 39 | 0 | 0 | 61 | 0 | 18 |
| Grp Sat Flow(s),veh/h/ln | 1781 | 1777 | 1867 | 1781 | 1777 | 1840 | 1731 | 0 | 0 | 1783 | 0 | 1585 |
| Q Serve(g_s), s | 4.7 | 20.9 | 20.9 | 0.3 | 46.6 | 48.6 | 2.3 | 0.0 | 0.0 | 3.5 | 0.0 | 1.1 |
| Cycle Q Clear(g_c), s | 4.7 | 20.9 | 20.9 | 0.3 | 46.6 | 48.6 | 2.3 | 0.0 | 0.0 | 3.5 | 0.0 | 1.1 |
| Prop In Lane | 1.00 |  | 0.01 | 1.00 |  | 0.08 | 0.69 |  | 0.26 | 0.98 |  | 1.00 |
| Lane Grp Cap(c), veh/h | 103 | 1333 | 1400 | 7 | 1237 | 1281 | 56 | 0 | 0 | 88 | 0 | 78 |
| V/C Ratio(X) | 0.79 | 0.60 | 0.60 | 0.72 | 0.86 | 0.87 | 0.69 | 0.00 | 0.00 | 0.70 | 0.00 | 0.23 |
| Avail Cap(c_a), veh/h | 103 | 1475 | 1550 | 52 | 1424 | 1475 | 301 | 0 | 0 | 448 | 0 | 398 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 0.00 | 1.00 | 0.00 | 1.00 |
| Uniform Delay (d), s/veh | 48.2 | 5.8 | 5.8 | 51.5 | 11.9 | 12.2 | 49.6 | 0.0 | 0.0 | 48.5 | 0.0 | 47.3 |
| Incr Delay (d2), s/veh | 31.3 | 0.5 | 0.5 | 41.0 | 4.9 | 5.4 | 14.1 | 0.0 | 0.0 | 3.7 | 0.0 | 0.6 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile BackOfQ(50\%),veh/ln | 2.9 | 4.7 | 5.0 | 0.2 | 14.1 | 15.4 | 1.2 | 0.0 | 0.0 | 1.6 | 0.0 | 0.5 |
| Unsig. Movement Delay, s/veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay ${ }^{\text {d }}$ ),s/veh | 79.5 | 6.4 | 6.4 | 92.5 | 16.7 | 17.6 | 63.7 | 0.0 | 0.0 | 52.1 | 0.0 | 47.9 |
| LnGrp LOS | E | A | A | F | B | B | E | A | A | D | A | D |
| Approach Vol, veh/h |  | 1711 |  |  | 2182 |  |  | 39 |  |  | 79 |  |
| Approach Delay, s/veh |  | 9.9 |  |  | 17.3 |  |  | 63.7 |  |  | 51.2 |  |
| Approach LOS |  | A |  |  | B |  |  | E |  |  | D |  |
| Timer - Assigned Phs | 1 | 2 |  | 4 | 5 | 6 |  | 8 |  |  |  |  |
| Phs Duration ( $G+Y+R \mathrm{c}$ ), $s$ | 9.0 | 78.1 |  | 8.6 | 3.4 | 83.7 |  | 7.9 |  |  |  |  |
| Change Period ( $\mathrm{Y}+\mathrm{Rc}$ ), s | 3.0 | 6.0 |  | 3.5 | 3.0 | 6.0 |  | 4.5 |  |  |  |  |
| Max Green Setting (Gmax), s | 6.0 | 83.0 |  | 26.0 | 3.0 | 86.0 |  | 18.0 |  |  |  |  |
| Max Q Clear Time (g_c+11), s | 6.7 | 50.6 |  | 5.5 | 2.3 | 22.9 |  | 4.3 |  |  |  |  |
| Green Ext Time (p_c), s | 0.0 | 21.5 |  | 0.2 | 0.0 | 15.4 |  | 0.1 |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 6th Ctrl DelayHCM 6th LOS |  |  | 15.3 |  |  |  |  |  |  |  |  |  |
|  |  |  | B |  |  |  |  |  |  |  |  |  |

## Notes

User approved ignoring U-Turning movement.

| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |


| Major/Minor | Major1 | Major2 |  |  |  |  |  | Minor1 |  |
| :--- | ---: | ---: | ---: | ---: | ---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 0 | 0 | 1680 | 0 | - |  |  |  |  |
| $\quad$ Stage 1 | - | - | - | - | - |  |  |  |  |


| Approach | EB | WB | NB |
| :--- | ---: | ---: | ---: |
| HCM Control Delay, $s$ | 0 | 0.6 | 21.5 |

HCM LOS C

| Minor Lane/Major Mvmt | NBLn1 | EBT | EBR | WBL | WBT |
| :--- | ---: | ---: | ---: | ---: | :--- |
| Capacity (veh/h) | 309 | - | -377 | - |  |
| HCM Lane V/C Ratio | 0.299 | - | -0.216 | - |  |
| HCM Control Delay (s) | 21.5 | - | -17.2 | - |  |
| HCM Lane LOS | C | - | - | C | - |
| HCM 95th \%tile Q(veh) | 1.2 | - | - | 0.8 | - |


| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | \％ | 个4 | 「 | \％ | 个 $\uparrow$ | 「 | 7 | $\uparrow$ | 「 | \％ | $\uparrow$ | 「 |
| Traffic Volume（veh／h） | 65 | 1240 | 135 | 150 | 1650 | 175 | 215 | 195 | 115 | 225 | 165 | 40 |
| Future Volume（veh／h） | 65 | 1240 | 135 | 150 | 1650 | 175 | 215 | 195 | 115 | 225 | 165 | 40 |
| Initial $\mathrm{Q}(\mathrm{Qb})$ ，veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 1.00 | 1.00 |  | 0.98 | 1.00 |  | 1.00 | 1.00 |  | 0.99 |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow，veh／h／ln | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 |
| Adj Flow Rate，veh／h | 69 | 1319 | 91 | 160 | 1755 | 80 | 218 | 222 | 0 | 208 | 220 | 14 |
| Peak Hour Factor | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 |
| Percent Heavy Veh，\％ | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| Cap，veh／h | 89 | 1669 | 744 | 188 | 1867 | 814 | 249 | 261 |  | 240 | 252 | 211 |
| Arrive On Green | 0.05 | 0.47 | 0.47 | 0.10 | 0.52 | 0.52 | 0.14 | 0.14 | 0.00 | 0.13 | 0.13 | 0.13 |
| Sat Flow，veh／h | 1795 | 3582 | 1598 | 1795 | 3582 | 1562 | 1795 | 1885 | 1598 | 1795 | 1885 | 1576 |
| Grp Volume（v），veh／h | 69 | 1319 | 91 | 160 | 1755 | 80 | 218 | 222 | 0 | 208 | 220 | 14 |
| Grp Sat Flow（s），veh／h／ln | 1795 | 1791 | 1598 | 1795 | 1791 | 1562 | 1795 | 1885 | 1598 | 1795 | 1885 | 1576 |
| Q Serve（g＿s），s | 4.3 | 35.3 | 3.7 | 9.9 | 52.1 | 2.9 | 13.5 | 13.0 | 0.0 | 12.9 | 13.0 | 0.9 |
| Cycle Q Clear（g＿c），s | 4.3 | 35.3 | 3.7 | 9.9 | 52.1 | 2.9 | 13.5 | 13.0 | 0.0 | 12.9 | 13.0 | 0.9 |
| Prop In Lane | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Lane Grp Cap（c），veh／h | 89 | 1669 | 744 | 188 | 1867 | 814 | 249 | 261 |  | 240 | 252 | 211 |
| V／C Ratio（X） | 0.78 | 0.79 | 0.12 | 0.85 | 0.94 | 0.10 | 0.88 | 0.85 |  | 0.87 | 0.87 | 0.07 |
| Avail Cap（c＿a），veh／h | 111 | 2294 | 1023 | 285 | 2642 | 1152 | 459 | 482 |  | 358 | 376 | 314 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter（l） | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay（d），s／veh | 53.3 | 25.6 | 17.1 | 49.9 | 25.5 | 13.7 | 47.9 | 47.7 | 0.0 | 48.1 | 48.1 | 42.9 |
| Incr Delay（d2），s／veh | 18.4 | 0.9 | 0.0 | 9.2 | 4.9 | 0.0 | 3.9 | 3.0 | 0.0 | 9.6 | 9.8 | 0.0 |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ（50\％），veh／ln | 2.3 | 13.6 | 1.2 | 4.8 | 20.7 | 1.0 | 6.2 | 6.2 | 0.0 | 6.3 | 6.7 | 0.3 |
| Unsig．Movement Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay（d），s／veh | 71.7 | 26.5 | 17.2 | 59.0 | 30.3 | 13.7 | 51.7 | 50.7 | 0.0 | 57.7 | 58.0 | 42.9 |
| LnGrp LOS | E | C | B | E | C | B | D | D |  | E | E | D |
| Approach Vol，veh／h |  | 1479 |  |  | 1995 |  |  | 440 | A |  | 442 |  |
| Approach Delay，s／veh |  | 28.0 |  |  | 32.0 |  |  | 51.2 |  |  | 57.4 |  |
| Approach LOS |  | C |  |  | C |  |  | D |  |  | E |  |


| Timer－Assigned Phs | 1 | 2 | 4 | 5 | 6 | 8 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Phs Duration $(G+Y+R c)$ ，s | 14.9 | 58.8 | 19.6 | 8.6 | 65.1 | 20.1 |
| Change Period（Y＋Rc），s | 3.0 | 6.0 | 4.4 | 3.0 | 6.0 | 4.4 |
| Max Green Setting（Gmax），s | 18.0 | 72.6 | 22.6 | 7.0 | 83.6 | 29.0 |
| Max Q Clear Time（g＿c＋11），s | 11.9 | 37.3 | 15.0 | 6.3 | 54.1 | 15.5 |
| Green Ext Time（p＿C），s | 0.0 | 3.0 | 0.2 | 0.0 | 5.0 | 0.2 |

## Intersection Summary

| HCM 6th Ctrl Delay | 35.1 |
| :--- | ---: |
| HCM 6th LOS |  |

## Notes

User approved pedestrian interval to be less than phase max green．
User approved volume balancing among the lanes for turning movement．
Unsignalized Delay for［NBR］is excluded from calculations of the approach delay and intersection delay．

| 4 | $\rightarrow$ | $\checkmark$ | 7 |  | $4$ | $4$ | $\dagger$ | \% | ( | $\frac{1}{\dagger}$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 44 | 7 | ${ }^{1}$ | 44 | 7 | ${ }^{7}$ | ¢4 | 7 | ${ }^{7}$ | 44 | F' |
| Traffic Volume (veh/h) 135 | 160 | 1120 | 75 | 245 | 100 | 1315 | 455 | 45 | 95 | 715 | 260 |
| Future Volume (veh/h) 135 | 160 | 1120 | 75 | 245 | 100 | 1315 | 455 | 45 | 95 | 715 | 260 |
| Initial Q (Qb), veh 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus, Adj 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow, veh/h/ln 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 |
| Adj Flow Rate, veh/h 150 | 178 | 0 | 83 | 272 | 0 | 1461 | 506 | 0 | 106 | 794 | 0 |
| Peak Hour Factor 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Percent Heavy Veh, \% 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| Cap, veh/h 168 | 463 |  | 104 | 336 |  | 1527 | 802 |  | 425 | 848 |  |
| Arrive On Green 0.09 | 0.13 | 0.00 | 0.06 | 0.09 | 0.00 | 0.43 | 0.43 | 0.00 | 0.24 | 0.24 | 0.00 |
| Sat Flow, veh/h 1795 | 3582 | 1598 | 1795 | 3582 | 1598 | 3591 | 1885 | 1598 | 1795 | 3582 | 1598 |
| Grp Volume(v), veh/h 150 | 178 | 0 | 83 | 272 | 0 | 1461 | 506 | 0 | 106 | 794 | 0 |
| Grp Sat Flow(s),veh/h/ln1795 | 1791 | 1598 | 1795 | 1791 | 1598 | 1795 | 1885 | 1598 | 1795 | 1791 | 1598 |
| Q Serve(g_s), s 10.6 | 5.8 | 0.0 | 5.9 | 9.5 | 0.0 | 50.5 | 27.0 | 0.0 | 6.1 | 27.9 | 0.0 |
| Cycle Q Clear(g_c), s 10.6 | 5.8 | 0.0 | 5.9 | 9.5 | 0.0 | 50.5 | 27.0 | 0.0 | 6.1 | 27.9 | 0.0 |
| Prop In Lane 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Lane Grp Cap(c), veh/h 168 | 463 |  | 104 | 336 |  | 1527 | 802 |  | 425 | 848 |  |
| V/C Ratio(X) 0.89 | 0.38 |  | 0.80 | 0.81 |  | 0.96 | 0.63 |  | 0.25 | 0.94 |  |
| Avail Cap(c_a), veh/h 168 | 707 |  | 140 | 673 |  | 1784 | 937 |  | 444 | 886 |  |
| HCM Platoon Ratio 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 |
| Uniform Delay (d), s/veh 57.5 | 51.1 | 0.0 | 59.6 | 57.0 | 0.0 | 35.7 | 28.9 | 0.0 | 39.7 | 48.0 | 0.0 |
| Incr Delay (d2), s/veh 39.4 | 0.2 | 0.0 | 14.5 | 1.8 | 0.0 | 11.1 | 0.6 | 0.0 | 0.1 | 16.1 | 0.0 |
| Initial Q Delay(d3),s/veh 0.0 \%ile BackOfQ( $50 \%$ ), veh/If6. 5 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
|  | 2.6 | 0.0 | 3.0 | 4.3 | 0.0 | 23.4 | 12.0 | 0.0 | 2.7 | 13.9 | 0.0 |
| Unsig. Movement Delay, s/veh |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay(d),s/veh 96.8 | 51.3 | 0.0 | 74.2 | 58.8 | 0.0 | 46.8 | 29.5 | 0.0 | 39.8 | 64.1 | 0.0 |
| LnGrp LOS F | D |  | E | E |  | D | C |  | D | E |  |
| Approach Vol, veh/h | 328 | A |  | 355 | A |  | 1967 | A |  | 900 | A |
| Approach Delay, s/veh | 72.1 |  |  | 62.4 |  |  | 42.3 |  |  | 61.2 |  |
| Approach LOS | E |  |  | E |  |  | D |  |  | E |  |
| Timer - Assigned Phs 1 | 2 |  | 4 | 5 | 6 |  | 8 |  |  |  |  |
| Phs Duration (G+Y+Rc), \$0.4 | 22.3 |  | 35.7 | 15.0 | 17.7 |  | 59.8 |  |  |  |  |
| Change Period (Y+Rc), s 3.0 | 5.7 |  | 5.3 | 3.0 | * 5.7 |  | 5.3 |  |  |  |  |
| Max Green Setting (GmakQ).s | 25.3 |  | 31.7 | 12.0 | * 24 |  | 63.7 |  |  |  |  |
| Max Q Clear Time (g_c+117,9s | 7.8 |  | 29.9 | 12.6 | 11.5 |  | 52.5 |  |  |  |  |
| Green Ext Time (p_c), s 0.0 | 0.3 |  | 0.5 | 0.0 | 0.5 |  | 2.0 |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |
| HCM 6th Ctrl Delay 51.9 |  |  |  |  |  |  |  |  |  |  |  |
| HCM 6th LOS D |  |  |  |  |  |  |  |  |  |  |  |
| Notes |  |  |  |  |  |  |  |  |  |  |  |
| User approved pedestrian interval to be less than phase max green. |  |  |  |  |  |  |  |  |  |  |  |
| User approved volume balancing among the lanes for turning movement. |  |  |  |  |  |  |  |  |  |  |  |
| * HCM 6th computational engine requires equal clearance times for the phases crossing the barrier. |  |  |  |  |  |  |  |  |  |  |  |

Unsignalized Delay for [NBR, EBR, WBR, SBR] is excluded from calculations of the approach delay and intersection delay.




| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | ＊＊ | 种中 | 「 | $\mathbf{H}^{*}{ }^{*}$ | 个种 | 「 | ${ }^{\text {a }}$ | 个个中 | 「 | ${ }^{\text {a }}$ | 个乐中 | F |
| Traffic Volume（veh／h） | 545 | 1670 | 325 | 436 | 1550 | 240 | 470 | 1140 | 270 | 251 | 1060 | 220 |
| Future Volume（veh／h） | 545 | 1670 | 325 | 436 | 1550 | 240 | 470 | 1140 | 270 | 251 | 1060 | 220 |
| Initial $Q(Q b)$ ，veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow，veh／h／ln | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 |
| Adj Flow Rate，veh／h | 580 | 1777 | 133 | 464 | 1649 | 0 | 500 | 1213 | 0 | 267 | 1128 | 207 |
| Peak Hour Factor | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 |
| Percent Heavy Veh，\％ | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| Cap，veh／h | 604 | 1784 | 553 | 488 | 1681 |  | 511 | 1426 |  | 312 | 1132 | 351 |
| Arrive On Green | 0.17 | 0.35 | 0.35 | 0.14 | 0.33 | 0.00 | 0.20 | 0.37 | 0.00 | 0.06 | 0.15 | 0.15 |
| Sat Flow，veh／h | 3483 | 5147 | 1596 | 3483 | 5147 | 1598 | 3483 | 5147 | 1598 | 3483 | 5147 | 1595 |
| Grp Volume（v），veh／h | 580 | 1777 | 133 | 464 | 1649 | 0 | 500 | 1213 | 0 | 267 | 1128 | 207 |
| Grp Sat Flow（s），veh／h／ln | 1742 | 1716 | 1596 | 1742 | 1716 | 1598 | 1742 | 1716 | 1598 | 1742 | 1716 | 1595 |
| Q Serve（g＿s），s | 24.8 | 51.7 | 6.0 | 19.8 | 47.6 | 0.0 | 21.4 | 32.5 | 0.0 | 11.4 | 32.9 | 18.2 |
| Cycle Q Clear（g＿c），s | 24.8 | 51.7 | 6.0 | 19.8 | 47.6 | 0.0 | 21.4 | 32.5 | 0.0 | 11.4 | 32.9 | 18.2 |
| Prop In Lane | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Lane Grp Cap（c），veh／h | 604 | 1784 | 553 | 488 | 1681 |  | 511 | 1426 |  | 312 | 1132 | 351 |
| V／C Ratio（X） | 0.96 | 1.00 | 0.24 | 0.95 | 0.98 |  | 0.98 | 0.85 |  | 0.86 | 1.00 | 0.59 |
| Avail Cap（c＿a），veh／h | 604 | 1784 | 553 | 488 | 1681 |  | 511 | 1426 |  | 325 | 1132 | 351 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.33 | 1.33 | 1.33 | 0.67 | 0.67 | 0.67 |
| Upstream Filter（l） | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay（d），s／veh | 61.5 | 48.9 | 15.8 | 64.0 | 50.0 | 0.0 | 60.1 | 44.5 | 0.0 | 69.5 | 63.9 | 57.6 |
| Incr Delay（d2），s／veh | 26.8 | 20.4 | 1.0 | 28.6 | 17.9 | 0.0 | 34.1 | 5.2 | 0.0 | 18.0 | 25.8 | 3.2 |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ（50\％），veh／ln | 13.0 | 24.8 | 3.5 | 10.6 | 22.6 | 0.0 | 11.3 | 13.4 | 0.0 | 5.9 | 17.3 | 7.8 |
| Unsig．Movement Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay（d），s／veh | 88.3 | 69.3 | 16.9 | 92.6 | 67.9 | 0.0 | 94.3 | 49.7 | 0.0 | 87.6 | 89.7 | 60.8 |
| LnGrp LOS | F | E | B | F | E |  | F | D |  | F | F | E |
| Approach Vol，veh／h |  | 2490 |  |  | 2113 | A |  | 1713 | A |  | 1602 |  |
| Approach Delay，s／veh |  | 70.9 |  |  | 73.3 |  |  | 62.7 |  |  | 85.6 |  |
| Approach LOS |  | E |  |  | E |  |  | E |  |  | F |  |


|  |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Timer－Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| Phs Duration $(\mathbf{G}+\mathrm{Y}+\mathrm{Rc}$ ），s | 27.0 | 58.0 | 26.0 | 39.0 | 30.0 | 55.0 | 17.4 | 47.6 |
| Change Period $(\mathrm{Y}+\mathrm{Rc}$ ），s | 6.0 | 6.0 | 4.0 | 6.0 | 4.0 | 6.0 | 4.0 | 6.0 |
| Max Green Setting（Gmax），s | 21.0 | 52.0 | 22.0 | 33.0 | 26.0 | 49.0 | 14.0 | 41.0 |
| Max Q Clear Time（g＿c＋11），s | 21.8 | 53.7 | 23.4 | 34.9 | 26.8 | 49.6 | 13.4 | 34.5 |
| Green Ext Time（p＿c），s | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 4.4 |

## Intersection Summary

| HCM 6th Ctrl Delay | 72.8 |
| :--- | ---: |
| HCM 6th LOS | $E$ |

## Notes

User approved pedestrian interval to be less than phase max green．
Unsignalized Delay for［NBR，WBR］is excluded from calculations of the approach delay and intersection delay．

| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ＊ | 44 | F | \＃ | 中 ${ }^{\text {a }}$ |  |  | $\uparrow$ | 「 |  | $\uparrow$ | 「 |
| Traffic Vol，veh／h | 45 | 2010 | 70 | 55 | 1820 | 4 | 15 | 0 | 50 | 0 | 1 | 40 |
| Future Vol，veh／h | 45 | 2010 | 70 | 55 | 1820 | 4 | 15 | 0 | 50 | 0 | 1 | 40 |
| Conflicting Peds，\＃／hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | － | － | None | － | － | None | － | － | None | － | － | None |
| Storage Length | 150 | － | 100 | 175 | － | － | － | － | 125 | － | － | 25 |
| Veh in Median Storage，\＃ | － | 0 | － | － | 0 | － | － | 0 | － | － | 0 | － |
| Grade，\％ | － | 0 | － | － | 0 | － | － | 0 | － | － | 0 | － |
| Peak Hour Factor | 94 | 94 | 94 | 94 | 94 | 94 | 94 | 94 | 94 | 94 | 94 | 94 |
| Heavy Vehicles，\％ | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| Mvmt Flow | 48 | 2138 | 74 | 59 | 1936 | 4 | 16 | 0 | 53 | 0 | 1 | 43 |


| Major／Minor | Major1 |  |  | Major2 |  | Minor1 |  |  | Minor2 |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 1940 | 0 | 0 | 2212 | 0 | 0 | 3321 | 4292 | 1069 | 3221 | 4364 | 970 |
| Stage 1 |  | － | － | － | － | － | 2234 | 2234 |  | 2056 | 2056 | － |
| Stage 2 |  | － | － | － | － | － | 1087 | 2058 |  | 1165 | 2308 |  |
| Critical Hdwy | 4.12 | － | － | 4.12 | － | － | 7.52 | 6.52 | 6.92 | 7.52 | 6.52 | 6.92 |
| Critical Hdwy Stg 1 | － | － | － | － | － | － | 6.52 | 5.52 | － | 6.52 | 5.52 | － |
| Critical Hdwy Stg 2 | － | － | － | － | － | － | 6.52 | 5.52 | － | 6.52 | 5.52 | － |
| Follow－up Hdwy | 2.21 | － | － | 2.21 | － | － | 3.51 | 4.01 | 3.31 | 3.51 | 4.01 | 3.31 |
| Pot Cap－1 Maneuver | 303 | － | － | 237 | － | － | － 3 | 2 | 219 | 4 | 2 | 255 |
| Stage 1 | － | － | － | － | － | － | 44 | 79 | － | 57 | 98 | － |
| Stage 2 | － | － | － | － | － | － | 232 | 98 | － | 208 | 73 | － |
| Platoon blocked，\％ |  | － | － |  | － | － |  |  |  |  |  |  |
| Mov Cap－1 Maneuver | 303 | － | － | 237 | － | － | － | 1 | 219 | 2 | $\sim 1$ | 255 |
| Mov Cap－2 Maneuver | － | － | － | － | － | － | － | 1 | － | 2 | $\sim 1$ | － |
| Stage 1 | － | － | － | － | － | － | 37 | 67 | － | 48 | 74 | － |
| Stage 2 | － | － | － | － | － | － | 143 | 74 | － | 133 | 61 | － |
|  |  |  |  |  |  |  |  |  |  |  |  |  |
| Approach | EB |  |  | WB |  |  | NB |  |  | SB |  |  |
| HCM Control Delay，s | 0.4 |  |  | 0.7 |  |  |  |  |  | 141.7 |  |  |
| HCM LOS |  |  |  |  |  |  |  |  |  | F |  |  |


| Minor Lane／Major Mvmt | NBLn1 NBLn2 | EBL | EBT | EBR | WBL | WBT | WBR SBLn1 SBLn2 |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Capacity（veh／h） | -219 | 303 | - | -237 | - | 1 | 255 |  |
| HCM Lane V／C Ratio | -0.243 | 0.158 | - | -0.247 | - | -1.064 | 0.167 |  |
| HCM Control Delay（s） | -26.6 | 19.1 | - | - | 25.1 | - | $\$ 4932.2$ | 21.9 |
| HCM Lane LOS | - | D | C | - | - | D | - | - |
| HCM 95th \％tile Q（veh） | - | 0.9 | 0.6 | - | - | 0.9 | - | - |

## Notes

$\sim$ ：Volume exceeds capacity $\$$ ：Delay exceeds 300s $\quad+$ ：Computation Not Defined $\quad$ ：All major volume in platoon

|  | 4 |  |  | 7 |  |  |  | $\uparrow$ |  |  | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \% | 个t |  | \% | 个 ${ }^{\text {a }}$ |  |  | \$ |  |  | $\uparrow$ | F |
| Traffic Volume (veh/h) | 55 | 2040 | 30 | 9 | 1840 | 20 | 20 | 0 | 6 | 30 | 1 | 25 |
| Future Volume (veh/h) | 55 | 2040 | 30 | 9 | 1840 | 20 | 20 | 0 | 6 | 30 | 1 | 25 |
| Initial $Q(Q b)$, veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 |  | 1.00 | 1.00 |  | 0.98 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow, veh/h/ln | 1885 | 1885 | 1885 | 1870 | 1885 | 1885 | 1870 | 1870 | 1870 | 1870 | 1870 | 1885 |
| Adj Flow Rate, veh/h | 59 | 2170 | 33 | 10 | 1957 | 21 | 22 | 0 | 7 | 32 | 1 | 6 |
| Peak Hour Factor | 0.94 | 0.94 | 0.92 | 0.92 | 0.94 | 0.94 | 0.92 | 0.92 | 0.92 | 0.94 | 0.92 | 0.94 |
| Percent Heavy Veh, \% | 1 | 1 | 1 | 2 | 1 | 1 | 2 | 2 | 2 | 2 | 2 | 1 |
| Cap, veh/h | 60 | 2898 | 44 | 12 | 2816 | 30 | 31 | 0 | 10 | 65 | 2 | 60 |
| Arrive On Green | 0.03 | 0.80 | 0.80 | 0.01 | 0.78 | 0.78 | 0.02 | 0.00 | 0.02 | 0.04 | 0.04 | 0.04 |
| Sat Flow, veh/h | 1795 | 3611 | 55 | 1781 | 3629 | 39 | 1312 | 0 | 417 | 1730 | 54 | 1598 |
| Grp Volume(v), veh/h | 59 | 1073 | 1130 | 10 | 964 | 1014 | 29 | 0 | 0 | 33 | 0 | 6 |
| Grp Sat Flow(s),veh/h/ln | 1795 | 1791 | 1875 | 1781 | 1791 | 1877 | 1730 | 0 | 0 | 1784 | 0 | 1598 |
| Q Serve(g_s), s | 4.9 | 44.3 | 44.9 | 0.8 | 39.2 | 39.5 | 2.5 | 0.0 | 0.0 | 2.7 | 0.0 | 0.5 |
| Cycle Q Clear(g_c), s | 4.9 | 44.3 | 44.9 | 0.8 | 39.2 | 39.5 | 2.5 | 0.0 | 0.0 | 2.7 | 0.0 | 0.5 |
| Prop In Lane | 1.00 |  | 0.03 | 1.00 |  | 0.02 | 0.76 |  | 0.24 | 0.97 |  | 1.00 |
| Lane Grp Cap(c), veh/h | 60 | 1437 | 1505 | 12 | 1389 | 1456 | 40 | 0 | 0 | 67 | 0 | 60 |
| V/C Ratio(X) | 0.99 | 0.75 | 0.75 | 0.82 | 0.69 | 0.70 | 0.72 | 0.00 | 0.00 | 0.49 | 0.00 | 0.10 |
| Avail Cap(c_a), veh/h | 60 | 1437 | 1505 | 36 | 1389 | 1456 | 209 | 0 | 0 | 309 | 0 | 277 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(1) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 0.00 | 1.00 | 0.00 | 1.00 |
| Uniform Delay (d), s/veh | 72.5 | 7.3 | 7.4 | 74.4 | 8.2 | 8.2 | 72.8 | 0.0 | 0.0 | 70.8 | 0.0 | 69.7 |
| Incr Delay (d2), s/veh | 110.9 | 3.6 | 3.5 | 37.6 | 2.9 | 2.8 | 20.9 | 0.0 | 0.0 | 5.5 | 0.0 | 0.7 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile BackOfQ(50\%),veh/ln | 4.1 | 12.8 | 13.5 | 0.5 | 12.2 | 12.9 | 1.4 | 0.0 | 0.0 | 1.4 | 0.0 | 0.2 |
| Unsig. Movement Delay, s/veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay(d),s/veh | 183.3 | 10.9 | 10.9 | 112.0 | 11.0 | 11.0 | 93.7 | 0.0 | 0.0 | 76.3 | 0.0 | 70.5 |
| LnGrp LOS | F | B | B | F | B | B | F | A | A | E | A | E |
| Approach Vol, veh/h |  | 2262 |  |  | 1988 |  |  | 29 |  |  | 39 |  |
| Approach Delay, s/veh |  | 15.4 |  |  | 11.5 |  |  | 93.7 |  |  | 75.4 |  |
| Approach LOS |  | B |  |  | B |  |  | F |  |  | E |  |
| Timer - Assigned Phs | 1 | 2 |  | 4 | 5 | 6 |  | 8 |  |  |  |  |
| Phs Duration ( $G+Y+R \mathrm{c}$ ), $s$ | 8.0 | 122.4 |  | 11.6 | 4.0 | 126.3 |  | 8.0 |  |  |  |  |
| Change Period ( $\mathrm{Y}+\mathrm{Rc}$ ), s | 3.0 | 6.0 |  | 6.0 | 3.0 | 6.0 |  | 4.5 |  |  |  |  |
| Max Green Setting (Gmax), s | 5.0 | 81.4 |  | 26.0 | 3.0 | 83.4 |  | 18.1 |  |  |  |  |
| Max Q Clear Time (g_c+11), s | 6.9 | 41.5 |  | 4.7 | 2.8 | 46.9 |  | 4.5 |  |  |  |  |
| Green Ext Time (p_c), s | 0.0 | 20.4 |  | 0.1 | 0.0 | 23.6 |  | 0.1 |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 6th Ctrr Delay |  |  | 14.7 |  |  |  |  |  |  |  |  |  |
| HCM 6th LOS B |  |  |  |  |  |  |  |  |  |  |  |  |

## Notes

User approved ignoring U-Turning movement.

| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |


| Major/Minor | Major1 | Major2 |  | Minor1 |  |  |
| :--- | ---: | ---: | :--- | :--- | :--- | :--- |
| Conflicting Flow All | 0 | 0 | 2179 | 0 | -1090 |  |
| $\quad$ Stage 1 | - | - | - | - | - | - |
| Stage 2 | - | - | - | - | - | - |
| Critical Hdwy | - | - | 4.14 | - | - | 6.94 |
| Critical Hdwy Stg 1 | - | - | - | - | - | - |
| Critical Hdwy Stg 2 | - | - | - | - | - | - |
| Follow-up Hdwy | - | - | 2.22 | - | - | 3.32 |
| Pot Cap-1 Maneuver | - | - | 241 | - | 0 | 210 |
| $\quad$ Stage 1 | - | - | - | - | 0 | - |
| Stage 2 | - | - | - | - | 0 | - |
| Platoon blocked, \% | - | - |  | - |  |  |
| Mov Cap-1 Maneuver | - | - | 241 | - | - | 210 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - |
| Stage 1 | - | - | - | - | - | - |
| Stage 2 | - | - | - | - | - | - |


|  | EB | WB | NB |
| :--- | :---: | :---: | :---: |
| Approach | 1.1 | 57.3 |  |
| HCM Control Delay, s | 0 | 1.1 | F |


| Minor Lane/Major Mvmt | NBLn1 | EBT | EBR | WBL |
| :--- | ---: | ---: | ---: | :--- | WBT $\quad$.


| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 2.3 |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \% | 性 |  | * | 个 ${ }^{\text {a }}$ |  |  |  | " |  |  | F |
| Traffic Vol, veh/h | 145 | 1950 | 30 | 55 | 1750 | 25 | 0 | 0 | 15 | 0 | 0 | 130 |
| Future Vol, veh/h | 145 | 1950 | 30 | 55 | 1750 | 25 | 0 | 0 | 15 | 0 | 0 | 130 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | 250 | - | - | 325 | - | - | - | - | 0 | - | - | 0 |
| Veh in Median Storage, \# | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 |
| Heavy Vehicles, \% | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| Mvmt Flow | 153 | 2053 | 32 | 58 | 1842 | 26 | 0 | 0 | 16 | 0 | 0 | 137 |


| Major/Minor | Major1 |  |  | Major2 |  | Minor1 |  | Minor2 |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 1868 | 0 | 0 | 2085 | 0 | 0 |  |  | 1043 |  | - | 934 |
| Stage 1 |  | - | - | - | - | - |  |  |  |  |  |  |
| Stage 2 | - | - | - | - | - | - | - | - | - |  | - |  |
| Critical Hdwy | 4.12 | - | - | 4.12 | - | - | - | - | 6.92 | - | - | 6.92 |
| Critical Hdwy Stg 1 | - | - | - | - | - | - | - | - | - | - | - | - |
| Critical Hdwy Stg 2 | - | - | - | - | - | - | - | - | - | - | - | - |
| Follow-up Hdwy | 2.21 | - | - | 2.21 | - | - | - | - | 3.31 | - | - | 3.31 |
| Pot Cap-1 Maneuver | 323 | - | - | 266 | - | - | 0 | 0 | 228 | 0 | 0 | 269 |
| Stage 1 | - | - | - | - | - | - | 0 | 0 | - | 0 | 0 | - |
| Stage 2 | - | - | - | - | - | - | 0 | 0 | - | 0 | 0 | - |
| Platoon blocked, \% |  | - | - |  | - | - |  |  |  |  |  |  |
| Mov Cap-1 Maneuver | 323 | - | - | 266 | - | - | - | - | 228 | - | - | 269 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | - | - | - | - | - | - |
| Stage 1 |  | - | - | - | - | - | - | - | - | - | - | - |

Stage 2

| Approach | EB | WB | NB | SB |
| :--- | :---: | :---: | :---: | :---: |
| HCM Control Delay, s | 1.8 | 0.7 | 22 | 31.5 |
| HCM LOS |  |  | C | D |


| Minor Lane/Major Mvmt | NBLn1 | EBL | EBT | EBR | WBL | WBT | WBR SBLn1 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 228 | 323 | - | -266 | - | -269 |  |
| HCM Lane V/C Ratio | 0.069 | 0.473 | - | -0.218 | - | -0.509 |  |
| HCM Control Delay (s) | 22 | 25.7 | - | - | 22.3 | - | -31.5 |
| HCM Lane LOS | C | D | - | - | C | - | - |
| HCM 95th \%tile Q(veh) | 0.2 | 2.4 | - | - | 0.8 | - | - |
| (ven |  |  |  |  |  |  |  |


| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | 幺 | 性 | 「 | \％ | 个 $\uparrow$ | F | ${ }^{7}$ | $\uparrow$ | 「 | ${ }^{7}$ | $\uparrow$ | 「 |
| Traffic Volume（veh／h） | 75 | 1690 | 200 | 135 | 1530 | 220 | 160 | 150 | 145 | 245 | 155 | 65 |
| Future Volume（veh／h） | 75 | 1690 | 200 | 135 | 1530 | 220 | 160 | 150 | 145 | 245 | 155 | 65 |
| Initial $Q(Q b)$ ，veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 0.98 | 1.00 |  | 0.93 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow，veh／h／ln | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Adj Flow Rate，veh／h | 77 | 1742 | 154 | 139 | 1577 | 185 | 160 | 162 | 0 | 206 | 225 | 22 |
| Peak Hour Factor | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 |
| Percent Heavy Veh，\％ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Cap，veh／h | 98 | 1846 | 806 | 167 | 1981 | 818 | 191 | 201 |  | 244 | 256 | 217 |
| Arrive On Green | 0.05 | 0.51 | 0.51 | 0.09 | 0.55 | 0.55 | 0.11 | 0.11 | 0.00 | 0.13 | 0.13 | 0.13 |
| Sat Flow，veh／h | 1810 | 3610 | 1577 | 1810 | 3610 | 1490 | 1810 | 1900 | 1610 | 1810 | 1900 | 1610 |
| Grp Volume（v），veh／h | 77 | 1742 | 154 | 139 | 1577 | 185 | 160 | 162 | 0 | 206 | 225 | 22 |
| Grp Sat Flow（s），veh／h／ln | 1810 | 1805 | 1577 | 1810 | 1805 | 1490 | 1810 | 1900 | 1610 | 1810 | 1900 | 1610 |
| Q Serve（g＿s），s | 4.8 | 51.9 | 6.0 | 8.6 | 39.9 | 7.3 | 9.9 | 9.5 | 0.0 | 12.7 | 13.2 | 1.4 |
| Cycle Q Clear（g＿c），s | 4.8 | 51.9 | 6.0 | 8.6 | 39.9 | 7.3 | 9.9 | 9.5 | 0.0 | 12.7 | 13.2 | 1.4 |
| Prop In Lane | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Lane Grp Cap（c），veh／h | 98 | 1846 | 806 | 167 | 1981 | 818 | 191 | 201 |  | 244 | 256 | 217 |
| V／C Ratio（X） | 0.78 | 0.94 | 0.19 | 0.83 | 0.80 | 0.23 | 0.84 | 0.81 |  | 0.84 | 0.88 | 0.10 |
| Avail Cap（c＿a），veh／h | 143 | 2300 | 1005 | 191 | 2395 | 989 | 461 | 484 |  | 295 | 310 | 263 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter（1） | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay（d），s／veh | 53.2 | 26.3 | 15.1 | 50.9 | 20.6 | 13.2 | 50.0 | 49.8 | 0.0 | 48.1 | 48.4 | 43.2 |
| Incr Delay（d2），s／veh | 9.1 | 7.1 | 0.0 | 21.3 | 1.3 | 0.1 | 3.7 | 2.9 | 0.0 | 14.6 | 18.6 | 0.1 |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ（50\％），veh／In | 2.3 | 21.1 | 2.0 | 4.7 | 15.0 | 2.2 | 4.6 | 4.6 | 0.0 | 6.6 | 7.5 | 0.5 |
| Unsig．Movement Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay（d），s／veh | 62.3 | 33.4 | 15.1 | 72.2 | 21.9 | 13.3 | 53.7 | 52.7 | 0.0 | 62.7 | 67.0 | 43.3 |
| LnGrp LOS | E | C | B | E | C | B | D | D |  | E | E | D |
| Approach Vol，veh／h |  | 1973 |  |  | 1901 |  |  | 322 | A |  | 453 |  |
| Approach Delay，s／veh |  | 33.1 |  |  | 24.7 |  |  | 53.2 |  |  | 63.9 |  |
| Approach LOS |  | C |  |  | C |  |  | D |  |  | E |  |


| Timer－Assigned Phs | 1 | 2 | 4 | 5 | 6 | 8 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Phs Duration $(G+Y+R c)$ ，s | 13.5 | 64.2 | 19.8 | 9.2 | 68.5 | 16.4 |
| Change Period（Y＋Rc），s | 3.0 | 6.0 | 4.4 | 3.0 | 6.0 | 4.4 |
| Max Green Setting（Gmax），s | 12.0 | 72.6 | 18.6 | 9.0 | 75.6 | 29.0 |
| Max Q Clear Time（g＿c＋11），s | 10.6 | 53.9 | 15.2 | 6.8 | 41.9 | 11.9 |
| Green Ext Time（p＿C），s | 0.0 | 4.3 | 0.1 | 0.0 | 4.3 | 0.1 |

## Intersection Summary

| HCM 6th Ctrl Delay | 34.1 |
| :--- | ---: |
| HCM 6th LOS | C |

## Notes

User approved pedestrian interval to be less than phase max green．
User approved volume balancing among the lanes for turning movement．
Unsignalized Delay for［NBR］is excluded from calculations of the approach delay and intersection delay．

| 4 | $\rightarrow$ | $\cdots$ | 7 |  | 4 | $4$ | $\dagger$ | $p$ |  |  | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 44 | 「 | ${ }^{7}$ | 44 | F' | ${ }^{7}$ | ¢4 | 7 | ${ }^{7}$ | 44 | 7 |
| Traffic Volume (veh/h) 215 | 315 | 1240 | 60 | 290 | 120 | 1190 | 750 | 80 | 120 | 520 | 205 |
| Future Volume (veh/h) 215 | 315 | 1240 | 60 | 290 | 120 | 1190 | 750 | 80 | 120 | 520 | 205 |
| Initial Q (Qb), veh 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus, Adj 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow, veh/h/ln 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 |
| Adj Flow Rate, veh/h 224 | 328 | 0 | 62 | 302 | 0 | 1240 | 781 | 0 | 125 | 542 | 0 |
| Peak Hour Factor 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 |
| Percent Heavy Veh, \% 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| Cap, veh/h 242 | 704 |  | 80 | 380 |  | 1534 | 806 |  | 303 | 605 |  |
| Arrive On Green 0.13 | 0.20 | 0.00 | 0.04 | 0.11 | 0.00 | 0.43 | 0.43 | 0.00 | 0.17 | 0.17 | 0.00 |
| Sat Flow, veh/h 1795 | 3582 | 1598 | 1795 | 3582 | 1598 | 3591 | 1885 | 1598 | 1795 | 3582 | 1598 |
| Grp Volume(v), veh/h 224 | 328 | 0 | 62 | 302 | 0 | 1240 | 781 | 0 | 125 | 542 | 0 |
| Grp Sat Flow(s),veh/h/ln1795 | 1791 | 1598 | 1795 | 1791 | 1598 | 1795 | 1885 | 1598 | 1795 | 1791 | 1598 |
| Q Serve(g_s), s 14.6 | 9.6 | 0.0 | 4.1 | 9.8 | 0.0 | 35.8 | 48.0 | 0.0 | 7.4 | 17.6 | 0.0 |
| Cycle Q Clear(g_c), s 14.6 | 9.6 | 0.0 | 4.1 | 9.8 | 0.0 | 35.8 | 48.0 | 0.0 | 7.4 | 17.6 | 0.0 |
| Prop In Lane $\quad 1.00$ |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Lane Grp Cap(c), veh/h 242 | 704 |  | 80 | 380 |  | 1534 | 806 |  | 303 | 605 |  |
| V/C Ratio(X) 0.92 | 0.47 |  | 0.78 | 0.79 |  | 0.81 | 0.97 |  | 0.41 | 0.90 |  |
| Avail Cap(c_a), veh/h 242 | 828 |  | 151 | 671 |  | 1554 | 816 |  | 333 | 665 |  |
| HCM Platoon Ratio 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) $\quad 1.00$ | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 |
| Uniform Delay (d), s/veh 50.7 | 42.1 | 0.0 | 56.0 | 51.7 | 0.0 | 29.7 | 33.2 | 0.0 | 44.0 | 48.2 | 0.0 |
| Incr Delay (d2), s/veh 37.3 | 0.2 | 0.0 | 5.9 | 1.4 | 0.0 | 3.0 | 23.9 | 0.0 | 0.3 | 13.2 | 0.0 |
| Initial Q Delay(d3),s/veh 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile BackOfQ(50\%),veh/lı8.8 | 4.1 | 0.0 | 1.9 | 4.4 | 0.0 | 15.3 | 26.0 | 0.0 | 3.2 | 8.7 | 0.0 |
| Unsig. Movement Delay, s/veh |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay(d),s/veh 87.9 | 42.3 | 0.0 | 62.0 | 53.2 | 0.0 | 32.7 | 57.1 | 0.0 | 44.3 | 61.5 | 0.0 |
| LnGrp LOS F | D |  | E | D |  | C | E |  | D | E |  |
|  | 552 | A |  | 364 | A |  | 2021 | A |  | 667 | A |
| Approach Delay, s/veh | 60.8 |  |  | 54.7 |  |  | 42.1 |  |  | 58.3 |  |
| Approach LOS | E |  |  | D |  |  | D |  |  | E |  |
| Timer - Assigned Phs 1 | 2 |  | 4 | 5 | 6 |  | 8 |  |  |  |  |
| Phs Duration ( $\mathrm{G}+\mathrm{Y}+\mathrm{Rc}$ ), s8.3 | 29.0 |  | 25.3 | 19.0 | 18.3 |  | 55.9 |  |  |  |  |
| Change Period (Y+Rc), s 3.0 | 5.7 |  | 5.3 | 3.0 | * 5.7 |  | 5.3 |  |  |  |  |
| Max Green Setting (GmakV).¢ | 27.4 |  | 22.0 | 16.0 | * 22 |  | 51.3 |  |  |  |  |
| Max Q Clear Time (g_c+lı, 1 , | 11.6 |  | 19.6 | 16.6 | 11.8 |  | 50.0 |  |  |  |  |
| Green Ext Time (p_c), s 0.0 | 0.6 |  | 0.4 | 0.0 | 0.5 |  | 0.6 |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |
| HCM 6th Ctrl Delay 49.2 |  |  |  |  |  |  |  |  |  |  |  |
| HCM 6th LOS D |  |  |  |  |  |  |  |  |  |  |  |
| Notes |  |  |  |  |  |  |  |  |  |  |  |
| User approved pedestrian interval to be less than phase max green. |  |  |  |  |  |  |  |  |  |  |  |
| User approved volume balancing among the lanes for turning movement. |  |  |  |  |  |  |  |  |  |  |  |
| * HCM 6th computational engine requires equal clearance times for the phases crossing the barrier. |  |  |  |  |  |  |  |  |  |  |  |

Unsignalized Delay for [NBR, EBR, WBR, SBR] is excluded from calculations of the approach delay and intersection delay.




| AM | Existing |  |  |  | Existing Plus Project |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | EB |  | WB | Approach | $\begin{aligned} & \text { NB } \\ & \text { Left } \end{aligned}$ | SB |  |  |  | EB |  | WB |  | NB |  | SB |  |  |
|  |  | Left | ıpproac | Left |  |  | Approach | Left | Approach |  | Left | Approach | Left | Approach | Left | Approach | Left | Approach |  |
| Woodgrove/Quail Oaks | vol | 39 |  | 41 |  |  | 62 |  | 100 |  | 39 |  | 41 |  |  | 63 |  | 100 |  |
|  | delay | 20.1 |  | 14.2 |  |  | 155.4 |  | 42.4 | 63.0 | 20.1 |  | 14.4 |  |  | 153.5 |  | 46.5 | 64.6 |
| Granite Estates | vol |  |  | 18 |  |  | 24 |  |  |  |  |  | 18 |  |  | 24 |  |  |  |
|  | delay |  |  | 14.5 |  |  | 16.8 |  |  | 15.8 |  |  | 14.5 |  |  | 17.1 |  |  | 16.0 |
| Berg | vol | 61 |  | 34 |  |  | 2 |  | 64 |  | 61 |  | 34 |  |  | 2 |  | 69 |  |
|  | delay | 19.9 |  | 13.1 |  |  | 14.5 |  | 23.7 | 19.9 | 19.9 |  | 13.1 |  |  | 14.6 |  | 24.5 | 20.4 |
| Access | vol |  |  |  |  |  |  |  |  |  |  |  |  | 5 |  |  |  | 3 |  |
|  | delay |  |  |  |  |  |  |  |  | \#\#\#\#\# |  |  |  | 9.4 |  |  |  | 7.4 | 8.7 |
| PM |  | EB |  | WB |  | NB |  | SB |  |  | EB |  | WB |  | NB |  | SB |  |  |
|  |  | Left | ıpproac | Left | Approach | Left | Approach | Left | Approach |  | Left | Approach | Left | Approach | Left | Approach | Left | Approach |  |
| Woodgrove/Quail Oaks | vol | 45 |  | 31 |  |  | 34 |  | 38 |  | 45 |  | 31 |  |  | 36 |  | 38 |  |
|  | delay | 17.8 |  | 20.5 |  |  | 315.3882 |  | 149.6 | 120.6 | 18.3 |  | 20.6 |  |  | 315.6706 |  | 150.1 | 123.5 |
| Granite Estates | vol |  |  | 13 |  |  | 39 |  |  |  |  |  | 33 |  |  | 39 |  |  |  |
|  | delay |  |  | 19.5 |  |  | 24.6 |  |  | 23.3 |  |  | 21.1 |  |  | 24.8 |  |  | 23.1 |
| Berg | vol | 68 |  | 40 |  |  | 11 |  | 48 |  | 75 |  | 40 |  |  | 11 |  | 105 |  |
|  | delay | 17.8 |  | 18.8 |  |  | 19.8 |  | 20 | 18.8 | 18.2 |  | 19.1 |  |  | 20 |  | 25 | 21.5 |
| Access | vol |  |  |  |  |  |  |  |  |  |  |  |  | 61 |  |  |  | 1 |  |
|  | delay |  |  |  |  |  |  |  |  |  |  |  |  | 9.6 |  |  |  | 7.4 | 9.6 |





[^0]:    1 Placer County Public Works Department. Requirements for Sewer Service for Berg Street Office Complex, (PLN16-00026) (Approx. 10 EDUs) (APN 048-084-030). March 10, 2016.

[^1]:    CHAPTER 4 - MITIGATION MONITORING AND REPORTING PROGRAM

[^2]:    CHAPTER 4 - Mitigation Monitoring and REporting Program

[^3]:    ChAPTER 4 - Mitigation MONitoring and REporting Program

[^4]:    Traffic Impact Analysis for Quarry Ridge Professional Office Park, Granite Bay, CA (4/5/2019)

