

D & D ENGINEERING, INC.

THE PARK @ LIVE OAK SEWER AREA STUDY

JUNE 12, 2018

D & D Engineering, Inc. 8901 S. La Cienega Blvd. Inglewood, CA 90301 424-351-6800









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I. INTRODUCTION

The purpose of this report is to determine the following:

- The expected average daily and peak wastewater flows from the proposed development based on the latest land use designations and building intensities.
- The impact of the proposed project on the existing City of Irwindale sewer system and pipe segments. The pipe segments are analyzed from the proposed development to the Sanitation District of Los Angeles (LACSD) trunk sewer lines.
- The capacities of the existing City and LACSD sewer lines and the adequacy of the existing sewer systems to convey the additional anticipated wastewater from the proposed project.

II. SITE DESCRIPTION

The Park @ Live Oak Project consist of 78.32 acres in the west portion of the City of Irwindale, immediately west of Interstate 605. Project site is bound by Arrow Highway on the North, Live Oak Avenue on the Southeast and Interstate 605 (I-605) on the East. Refer to the project site map, Figure 1 — Vicinity Map, for project site locations.

The existing site is a former sand and gravel quarry. Currently on-site backfill operations are underway to enable the redevelopment of the site. The Park @ Live Oak includes industrial, business park and commercial uses. The project consists of 1,451,400 sq. feet of industrial/business park and 98,600 sq. feet of commercial uses.

III. EXISTING SEWER SYSTEMS DESCRIPTION

The proposed project is located within the jurisdictional boundaries of the City of Irwindale and Los Angeles County Sanitation District (LACSD) District No.22. The wastewater flow originating from the project site will discharge to an existing City of Irwindale sewer line for conveyance to the LACSD Joint Outfall B Unit 8G Trunk Sewer, located in Live Oak Avenue at Myrtle Avenue. Please refer to Figure 2 — Sewer System Exhibit for existing sewer infrastructure.

The table below provides a summary of the existing sewer infrastructure in the vicinity of the proposed project. This summary is based on the latest available and reviewed record drawings. Please refer to *Appendix F - As-Built Plans* for copies of the City of Irwindale record drawings.

Location	Size	Notes
Arrow Hwy	Line B - City of Irwindale 15" Sewer Line	Sewer line flows west
Live Oak Ave	Line A – City of Irwindale 15" Sewer Line	Sewer line southwest of intersection with Arrow Hwy. Sewer line flows northwest to intersection of Live Oak Ave and Arrow Hwy
Live Oak Ave	Line C - City of Irwindale 21" Sewer Line	Sewer line between Arrow Hwy and private drive Line D. Sewer line flows west

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Private Drive Alley	Line D - City of Irwindale 12" Sewer Line	Sewer line flows northwest to MH at Live Oak and private drive intersection
Live Oak Avenue	Line E - City of Irwindale 20" Sewer Line	Sewer line between private road intersection and outfall at Live Oak Ave and Myrtle Avenue. Sewer Line flows west

The original design of the Live Oak sewer was performed by Kenneth Mullen, Consulting Engineers to determine the sewer generation rates, tributary flows and sizes of proposed sewer lines to serve the entire tributary areas. Please refer to *Appendix E - LA Marketplace Sewer Design Live Oak Study* for copies of the tributary area map and sewer design calculations.

Additionally, David Evans and Associates, Inc. prepared a sewer area study dated June 2017 for the project site to determinate the capacity of existing sewer systems. The Sewer Area Study has been reviewed and accepted by the City of Irwindale. Please refer to *Appendix D — Sewer Area Study Arrow Pit Development dated June 2017* for a copy of the Sewer Area Study.

This sewer area study will utilize the findings of the above-mentioned studies and update the sewer generation flow calculations and existing sewer lines capacities based on the latest land use information and record drawings.

IV. PROPOSED DEVELOPMENT AND EXISTING SEWER FLOWS

The Park @ Live Oak consists of 1,451,400 sq. feet of industrial/business park land use and 98,600 sq. feet of commercial uses. The proposed project's sewer demand is estimated based on Los Angeles County Sanitation District (LACSD) sewage generation factors. The expected average and peak wastewater flows from the project are 322,325 GPD and 0.806 MGP respectfully. Please refer to LACSD Table 1, "Loadings for each class of land use" in Appendix A — Estimated Average Daily Sewer Flows for Various Occupancies and Table 1 — Summary of Project Average Daily and Peak Sewer Flows for project sewer demand calculations.

The proposed project site will have multiple points of connection (POC) to the existing sewer lines A and B. The majority of the site peak wastewater flow (approximately 88.8% of the peak flow) will be tributary to existing Line A along Live Oak Ave. The remaining site peak wastewater flow (11.2% of the peak flow) will be tributary to Line B along Arrow Hwy. Please refer to Figure 2 — Sewer System Exhibit for proposed POC to existing sewer lines and Tables 1A and 1B for Line A and Line B contributing flows calculations.

This sewer area study has utilized the same wastewater flows of 80 gpd/1000 sq.ft. from tributary areas that contribute to existing sewer lines as estimated per original LA Marketplace sewer study, except for the LA Racing site located south of Live Oak Avenue. The original sewer study wastewater flow estimate for LA Marketplace (now the LA Racing) was based on 20,000 attendances, where LA Racing has 6,000 attendances capacity. Please refer to Table 1 C— Summary of Contributing Flows for LA Racing for contributing flows calculations.

Existing sewer lines segments area contributing flows and cumulative contributing flows are summarized in *Table 2*— *Sewer Capacity Summary*



V. SEWER PIPE CAPACITY ANALYSIS

Existing sewer lines A & B are 15" pipes diameters, line C is 21" pipe diameter, line D is 12" pipe diameter, and line E is 20" pipes diameter. Peak flow capacities for these lines, normal depths and velocities for peak flows were determined by using Kutter's Formula. Refer to Pipe Size Capacity Calculations in *Appendix C — Pipe Size Capacity Calculations*. Each main line is sized based on the minimum slope (worst case scenario) and half or 3/4 full pipe depending on the pipe size based on Los Angeles County guidelines. Note that LA County defines 100% DESIGN capacity for an existing pipeline, 15" or greater in diameter, as operating at ¾ full. A memo issued from the county, however, allows for the exceedance of this capacity. Refer to *Appendix B* for an excerpt from this memo.

As shown in Table 2 — Sewer Capacity Summary all existing City of Irwindale sewer lines have adequate capacity.

Additionally, a will serve letter request was submitted to LACSD for proposed development to verify trunk sewer line capacity. Based on the LACSD letter dated May 1, 2018 the District's Joint Outfall B Unit 8G Trunk Sewer has a capacity of 4.2 MGP and conveyed peak flow of 1.5 MGP when measured in 2012. This results in an available capacity of 2.7 MGP. The Park @ Live Oak Project will be contributing flow of 0.81 MGP to LACSD trunk sewer line. Therefore, existing trunk sewer line have enough available capacity for the proposed project. Please see LACSD will serve letter in *Appendix B*.

VI. CONCLUSION

A summary of existing pipe diameters, slopes, peak flows capacities and normal depts can be found in *Table 2 — Sewer Capacity Summary*. All existing sewer mains that will serve the project site, except for a portion of line E, meet the County capacity standards of no more than ½ full for mains under 15" diameter and no more than ¾ full for mains with a diameter of 15" and larger and will not negatively impact the available capacity of this sewer lines. The portion of Line E that exceeds the defined 100% capacity is also within the parameters allowed by the county memo. Refer to *Appendix B* and *Appendix C — Pipe Size Capacity Calculations*.

The project site will contribute 0.81 MGD to the LACSD Joint Outfall B Unit 8G Trunk Sewer, which does not exceed the available capacity of 2.7 MGD.

In summary the existing City of Irwindale collector lines have adequate capacity for the proposed project. Additionally, the existing LACSD sewer system have sufficient available capacity to serve the proposed project.



Tables

Table 1 — Summary of Project Average and Peak Sewer Flows

Table 1A — Sewer of Contributing Flows for Line B

Table 1B — Sewer of Contributing Flows for Line A

Table 1C — Sewer of Contributing Flows for

LA Racing

Table 2 — Sewer Capacity Summary

PARK @ LIVE OAK

TABLE 1 - Proposed Project Sewer Demand

Land use/Zone Type	Daily Average Generation Factor	Units	Area(SF)/ Unit Contribution	Daily Average Flow (GPD)	Peak Flow* (MGD)	Daily Average Flow (CFS)	Peak Flow* (CFS)
Industrial/Bussiness Park	200	gal/1000 SF	1,451,400	290,280	0.73	0.45	1.12
Commercial	325	gal/1000 SF	, ,	32,045	0.08	0.05	0.12
Totals			1,550,000	322,325	0.806	0.499	1.247

^{*} Peak Flow = 2.5 x daily average flow

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Table 1A - Proposed Sewer Demand Table Line B

Land use/Zone Type	Daily Average Generation Factor	Units	Area(SF)/ Unit Contribution	Daily Average Flow (GPD)	Peak Flow* (MGD)	Daily Average Flow (CFS)	Peak Flow* (CFS)
Industrial/Bussiness Park	200	gal/1000 SF	157,000	31,400	0.08	0.05	0.12
Commercial	325	gal/1000 SF	14,000	4,550	0.01	0.01	0.02
Totals			171,000	35,950	0.090	0.056	0.139

^{*} Peak Flow = 2.5 x daily average flow

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Table 1 B - Proposed Sewer Demand Table Line A

Land use/Zone Type	Daily Average Generation Factor	Units	Area(SF)/ Unit Contribution	Daily Average Flow (GPD)	Peak Flow* (MGD)	Daily Average Flow (CFS)	Peak Flow* (CFS)
Industrial/Bussiness Park	200	gal/1000 SF	1,294,400	258,880	0.65	0.40	1.00
Commercial	325	gal/1000 SF	84,600	27,495	0.07	0.04	0.11
Totals			1,379,000	286,375	0.716	0.443	1.108

^{*} Peak Flow = 2.5 x daily average flow

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Table 1 C - Proposed Sewer Demand LA Racing

Land use/Zone Type	Daily Average Generation Factor	Units	Unit Contributio n (Seats)	Daily Average Flow (GPD)	Peak Flow* (MGD)	Daily Average Flow (CFS)	Peak Flow* (CFS)
LA Racing	10	gal/Seat	6,000	60,000	0.15	0.09	0.23
Totals			6,000	60,000	0.15	0.09	0.23

^{*} Peak Flow = 2.5 x daily average flow

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TABLE 2 - SEWER CAPACITY SUMMARY

Pipe Segment	Contributing Areas	Pipe Diameter [Inches]	Pipe Slope	Pipe Capacity [CFS]	Area Contributing Flow [CFS]	Cummulative Contributing Flow [CFS]	Cumulative Contributing Flow [MGD]	Capacity?	Normal Depth [FT]	Depth?	Velocity [FT/S]	Velocity?
	Portion (88.8%) of Park @ Live Oak *	15	0.30%	1.72	1.11	1.11	0.72	SUFFICIENT	0.49	SUFFICIENT	2.47	SUFFICIENT
LINE A	LA Racing	15	0.30%	1.72	0.23	1.34	0.87	SUFFICIENT	0.54	SUFFICIENT	2.61	SUFFICIENT
	Sub Total	15	0.30%	1.72	1.34	1.34	0.87	SUFFICIENT	0.60	SUFFICIENT	2.74	SUFFICIENT
	Assessor Maps	15	0.63%	2.96	1.99	1.99	1.29	SUFFICIENT	0.55	SUFFICIENT	3.82	SUFFICIENT
LINE B	Portion (11.2%) of Park @ Live Oak *	15	0.63%	2.96	0.14	2.13	1.38	SUFFICIENT	0.53	SUFFICIENT	3.85	SUFFICIENT
	Sub Total	15	0.63%	2.69	2.13	2.13	1.38	SUFFICIENT	0.53	SUFFICIENT	3.85	SUFFICIENT
	Line A & Line B	20	0.16%	5.08	3.47	3.47	2.24	SUFFICIENT	0.75	SUFFICIENT	2.72	SUFFICIENT
LINE C*	Assessor Maps	20	0.16%	5.08	0.80	4.27	2.76	SUFFICIENT	0.83	SUFFICIENT	2.80	SUFFICIENT
	Sub Total	20	0.16%	5.08	4.27	4.27	2.76	SUFFICIENT	0.90	SUFFICIENT	2.80	SUFFICIENT
LINE D	Assessor Maps	12	0.40%	1.07	1.05	1.05	0.68	SUFFICIENT	0.49	SUFFICIENT	2.72	SUFFICIENT
LINE E*	LINE C + LINE D	20	0.16%	6.00*	5.32	5.32	3.44	SUFFICIENT	1.30	SUFFICIENT	2.82	SUFFICIENT

^{*} DISCHARGE FOR THIS PIPE SEGMENT SEGMENT IS 78.4% FULL, WHICH IS APPROXIMATELY 105% OF THE DESIGN CAPACITY. THIS IS BASED ON LA COUNTY'S DEFINITION OF 100% DESIGN CAPACITY BEING REACHED AT 75% FULL PIPE. HOWEVER, PER LOS ANGELES COUNTY POLICIES FOR MANAGING AVAILABLE SEWER CAPACITY AND SEWAGE DISCHARGE IN EXCESS OF DESIGN CAPACITY, NO FLOW MEASUREMENTS AND NO MITIGATION WILL BE REQUIRED. REFER TO APPENDIX B FOR MEMO FROMLA COUNTY.



Figures

Figure 1 — Vicinity Map

Figure 2 — Sewer Capacity Summary

\17015\Eng\17015\17015\Exhibits\04_Vicinity Map\Vicinity map.dwg 23, 2018 — 5:33pm by: Boris 5:33pm by: Boris Drawing Name: M: Last Opened: Mar





Appendix A

Estimated Average Daily Sewer Flows for Various Occupancies

TABLE 1
LOADINGS FOR EACH CLASS OF LAND USE

DESCRIPTION	UNIT OF MEASURE	FLOW (Gallons Per Day)	COD (Pounds Per Day)	SUSPENDED SOLIDS (Pounds Per Day)
RESIDENTIAL				
Single Family Home	Parcel	260	1.22	0.59
Duplex	Parcel	312	1.46	0.70
Triplex	Parcel	468	2.19	1.05
Fourplex	Parcel	624	2.92	1.40
Condominiums	Parcel	195	0.92	0.44
Single Family Home	Parcel	156	0.73	0.35
(reduced rate)	N CD 1 W	1 5 4	0.72	0.05
Five Units or More	No. of Dwlg. Units	156	0.73	0.35
Mobile Home Parks	No. of Spaces	156	0.73	0.35
COMMERCIAL				
Hotel/Motel/Rooming House	Room	125	0.54	0.28
Store	$1000 \; {\rm ft}^2$	100	0.43	0.23
Supermarket	1000 ft^2	150	2.00	1.00
Shopping Center	$1000 \; \mathrm{ft}^2$	325	3.00	1.17
Regional Mall	$1000 \; {\rm ft}^2$	150	2.10	0.77
Office Building	$1000 \; \mathrm{ft}^2$	200	0.86	0.45
Professional Building	$1000 \; \mathrm{ft}^2$	300	1.29	0.68
Restaurant	$1000 \; \mathrm{ft}^2$	1,000	16.68	5.00
Indoor Theatre	1000 ft^2	125	0.54	0.28
Car Wash				
Tunnel - No Recycling	1000 ft^2	3,700	15.86	8.33
Tunnel - Recycling	1000 ft^2	2,700	11.74	6.16
Wand	1000 ft^2	700	3.00	1.58
Financial Institution	1000 ft^2	100	0.43	0.23
Service Shop	$1000 \; \mathrm{ft}^2$	100	0.43	0.23
Animal Kennels	$1000 \; {\rm ft}^2$	100	0.43	0.23
Service Station	1000 ft^2	100	0.43	0.23
Auto Sales/Repair	1000 ft^2	100	0.43	0.23
Wholesale Outlet	$1000 \; \mathrm{ft}^2$	100	0.43	0.23
Nursery/Greenhouse	1000 ft^2	25	0.11	0.06
Manufacturing	$1000 \; \mathrm{ft}^2$	200	1.86	0.70
Dry Manufacturing	1000 ft^2	25	0.23	0.09
Lumber Yard	1000 ft^2	25	0.23	0.09
Warehousing	1000 ft^2	25	0.23	0.09
Open Storage	1000 ft^2	25	0.23	0.09
Drive-in Theatre	$1000~\mathrm{ft}^2$	20	0.09	0.05

TABLE 1
(continued)
LOADINGS FOR EACH CLASS OF LAND USE

DESCRIPTION	UNIT OF MEASURE	FLOW (Gallons <u>Per Day)</u>	COD (Pounds <u>Per Day)</u>	SUSPENDED SOLIDS (Pounds <u>Per Day)</u>
COMMERCIAL				
Night Club Bowling/Skating Club Auditorium, Amusement Golf Course, Camp, and Park (Structures and Improvements Recreational Vehicle Park Convalescent Home Laundry Mortuary/Cemetery Health Spa, Gymnasium With Showers Without Showers Convention Center, Fairground, Racetrack, Sports Stadium/Arena	1000 ft ² No. of Spaces Bed 1000 ft ² 1000 ft ² 1000 ft ² Average Daily Attendance	350 150 125 350 100 55 125 3,825 100 600 300	1.50 1.76 0.54 1.50 0.43 0.34 0.54 16.40 1.33 2.58 1.29	0.79 0.55 0.27 0.79 0.23 0.14 0.28 8.61 0.67 1.35 0.68 0.02
INSTITUTIONAL				
College/University Private School Church	Student 1000 ft^2 1000 ft^2	20 200 50	0.09 0.86 0.21	0.05 0.45 0.11



Appendix B

Will Serve Letter from the County
 Sanitation District dated May 1, 2018
 Policies for Managing Available Sewer
 Capacity and Sewage Discharge in Excess of Design Capacity



COUNTY SANITATION DISTRICTS OF LOS ANGELES COUNTY

1955 Workman Mill Road, Whittier, CA 90601-1400 Mailing Address: P.O. Box 4998, Whittier, CA 90607-4998 Telephone: (562) 699-7411, FAX: (562) 699-5422 www.lacsd.org

GRACE ROBINSON HYDE Chief Engineer and General Manager

May 1, 2018

Ref. Doc. No.: 4519356

Ms. Marilyn Simpson, AICP Community Development Manager Planning Division City of Irwindale 5050 North Irwindale Avenue Irwindale, CA 91706 CITY OF IRWINDALE
COMMUNITY DEVELOPMENT

MAY 0 2 2018

RECEIVED

Dear Ms. Simpson:

NOP Response for The Park @ Live Oak Specific Plan Project

The Sanitation Districts of Los Angeles County (Districts) received a Notice of Preparation of a Draft Environmental Impact Report (NOP) for the subject project on April 4, 2018. The proposed project is located within the jurisdictional boundaries of District No. 22. We offer the following comments regarding sewerage service:

- 1. The wastewater flow originating from the proposed project will discharge to a local sewer line, which is not maintained by the Districts, for conveyance to the Districts' Joint Outfall B Unit 8G Trunk Sewer, located in Live Oak Avenue at Myrtle Avenue. The Districts' 21-inch diameter trunk sewer has a capacity of 4.2 million gallons per day (mgd) and conveyed a peak flow of 1.5 mgd when last measured in 2012.
- 2. The wastewater generated by the proposed project will be treated at the San Jose Creek Water Reclamation Plant (WRP) located adjacent to the City of Industry, which has a capacity of 100 mgd and currently processes an average flow of 64.1 mgd. All biosolids and wastewater flows that exceed the capacity of the San Jose Creek WRP are diverted to and treated at the Joint Water Pollution Control Plant in the City of Carson.
- 3. The expected average wastewater flow from the project, described in the document as a 1,451,400-square-foot mixed-use industrial and commercial park, is 471,705 gallons per day. For a copy of the Districts' average wastewater generation factors, go to www.lacsd.org, Wastewater & Sewer Systems, click on Will Serve Program, and click on the Table 1, Loadings for Each Class of Land Use link.
- 4. The Districts are empowered by the California Health and Safety Code to charge a fee for the privilege of connecting (directly or indirectly) to the Districts' Sewerage System for increasing the strength or quantity of wastewater discharged from connected facilities. This connection fee is a capital facilities fee that is imposed in an amount sufficient to construct an incremental expansion of the Sewerage System to accommodate the proposed project. Payment of a

DOC #4563864.D22

connection fee will be required before a permit to connect to the sewer is issued. For more information and a copy of the Connection Fee Information Sheet, go to www.lacsd.org, Wastewater & Sewer Systems, click on Will Serve Program, and search for the appropriate link. In determining the impact to the Sewerage System and applicable connection fees, the Districts' Chief Engineer and General Manager will determine the user category (e.g. Condominium, Single Family home, etc.) that best represents the actual or anticipated use of the parcel or facilities on the parcel. For more specific information regarding the connection fee application procedure and fees, please contact the Connection Fee Counter at (562) 908-4288, extension 2727.

In order for the Districts to conform to the requirements of the Federal Clean Air Act (CAA), the capacities of the Districts' wastewater treatment facilities are based on the regional growth forecast adopted by the Southern California Association of Governments (SCAG). Specific policies included in the development of the SCAG regional growth forecast are incorporated into clean air plans, which are prepared by the South Coast and Antelope Valley Air Quality Management Districts in order to improve air quality in the South Coast and Mojave Desert Air Basins as mandated by the CCA. All expansions of Districts' facilities must be sized and service phased in a manner that will be consistent with the SCAG regional growth forecast for the counties of Los Angeles, Orange, San Bernardino, Riverside, Ventura, and Imperial. The available capacity of the Districts' treatment facilities will, therefore, be limited to levels associated with the approved growth identified by SCAG. As such, this letter does not constitute a guarantee of wastewater service, but is to advise you that the Districts intend to provide this service up to the levels that are legally permitted and to inform you of the currently existing capacity and any proposed expansion of the Districts' facilities.

If you have any questions, please contact the undersigned at (562) 908-4288, extension 2717.

Very truly yours,

Adriana Raza

Customer Service Specialist Facilities Planning Department

AR:ar

cc:

A. Schmidt

M. Tatalovich

Stone Bayen

October 12, 2005

TO: Dean Efstathiou

FROM: Dennis Hunter

Land Development Division

POLICIES FOR MANAGING AVAILABLE SEWER CAPACITY AND SEWAGE DISCHARGE IN EXCESS OF DESIGN CAPACITY

The following will set forth Public Works' policies related to managing sewer infrastructure capacity. Design capacity of the sewer mainline is defined as follows:

< 15" diameter ½ full = 100% capacity (d/D) ≥ 15" diameter ¾ full = 100% capacity (d/D)

When Public Works determines there is available capacity in a mainline sewer for infill and redevelopment projects, the remaining available capacity shall be allocated on a first come – first serve basis.

Sewer Advisory Committee

A Sewer Advisory Committee (SAC) will be formed for the purpose of recommending courses of action to address proposed development connecting to existing sewers that will cause them to be operating beyond their design capacity. The SAC will make their recommendations to Dean Efstathiou, Assistant Director. The SAC will be chaired by Waterworks and Sewer Maintenance Division and will have representatives from Design and Land Development Divisions. Each Division will appoint a Principal Engineer or Senior Civil Engineer as a representative to the SAC and will convene whenever sewer decisions are required to address developmental impacts. Sewer Maintenance will maintain records of SAC meetings and will prepare recommendations to Administration for approval. The SAC may require other Division representatives to participate on a case-by-case basis when necessary, such as Building and Safety and Programs Development.

Divisional Responsibilities

Design Division

- Support activities of the SAC.
- 2. Prepare sewer area studies when required.

 Maintain records/archive of all approved sewer area studies and flow measurements.

Land Development Division

- 1. Support activities of the SAC.
- 2. Impose sewer area study requirements for private developments if necessary and review/approve all submittals.
- Refer cases to SAC when both sewer area studies and flow measurements indicate that a potential overload situation exists or will exist based on criteria described below.
- Provide copies of all approved sewer area studies and flow measurements to Design Division for archiving.

Waterworks and Sewer Maintenance Division

- Chair the SAC, maintain meeting records and prepare position papers to Administration.
- Advise the SAC when an overload condition is observed during maintenance activities.
- Initiate effort to track and map all overload areas within the Consolidated Maintenance District.
- 4. Keep database of all flow measurement results.

Design Criteria

- Capacity of sewer mainlines less than 15" in diameter are considered full (100 percent) when the ratio of the depth of flow (d) over the pipe diameter (D) is equal to 0.5, expressed as d/D = 0.5.
- Capacity of sewer mainlines equal to or greater than 15" in diameter are considered full (100 percent) when the ratio of the depth of flow (d) over the pipe diameter (D) is equal to 0.75, expressed as d/D = 0.75.

- 3. When an area study indicates that flow conditions based on calculated discharges is between 101 percent to 150 percent of capacity, no flow measurements and no mitigation will be required. If maintenance records warrant, a flow test may be required.
- 4. When an area study for a development that proposes to increase the density or change the zoning indicates that flow conditions are between 151 to 200 percent of capacity, flow measurements shall be required. If the flow test indicates that the actual flow condition is below 151 percent, no mitigation will be required. If the flow test results indicate the actual flow is above 151 percent, the case shall be referred to the SAC to evaluate options and make recommendations to Administration for approval. These options may include, but are not limited to: requiring full mitigation from the development, assessing pro-rata shares, creation of a reimbursement district, or establishing a County Improvement (CI) district.

AHN:ca

PALDPUBISUBPCHECKISEWERIMISCELLANEOUSISEWER INFRASTRUCTURE MANAGEMENT

cc: Administration (Kelly)

Building and Safety (Patel)

Design (Kumar)

Land Development (D'Antonio, Burger, Ruiz, Chong, Witler, Narag)

Programs Development (Afshari)

Waterworks and Sewer Maintenance (Del Real, Lehto)



Appendix C

Pipe Size Capacity Calculations

Worksheet for Line A, S=0.3%, 1/2 full

	worksneet for	Line A, 5=0	7.3%, 1/2 Iuli	
Project Description				
Friction Method	Kutter Formula			
Solve For	Discharge			
Input Data				
Roughness Coefficient		0.013		
Channel Slope		0.00300	ft/ft	
Normal Depth		0.63	ft	
Diameter		1.25	ft	
Results				
Discharge		1.72	ft³/s	
Flow Area		0.61	ft²	
Wetted Perimeter		1.96	ft	
Hydraulic Radius		0.31	ft	
Top Width		1.25	ft	
Critical Depth		0.52	ft	
Percent Full		50.0	%	
Critical Slope		0.00581	ft/ft	
Velocity		2.80	ft/s	
Velocity Head		0.12	ft	
Specific Energy		0.75	ft	
Froude Number		0.70		
Maximum Discharge		3.74	ft³/s	
Discharge Full		3.43	ft³/s	
Slope Full		0.00077	ft/ft	
Flow Type	SubCritical			
GVF Input Data				
Downstream Depth		0.00	ft	
Length		0.00	ft	
Number Of Steps		0		
GVF Output Data				
Upstream Depth		0.00	ft	
Profile Description				
Profile Headloss		0.00	ft	
Average End Depth Over Ris	se	0.00	%	
Normal Depth Over Rise		50.00	%	
Downstream Velocity		Infinity	ft/s	

Worksheet for Line A, S=0.3%, 1/2 full

GVF Output Data

Upstream Velocity Infinity ft/s Normal Depth 0.63 ft Critical Depth 0.52 ft Channel Slope 0.00300 ft/ft Critical Slope 0.00581 ft/ft

Worksheet for Line A, S=0.3%, Q=1.475

	orksneet for	Lille A, 3-U.	3 /0, Q =1.473	
Project Description				
Friction Method	Kutter Formula			
Solve For	Normal Depth			
	·			
Input Data				
Roughness Coefficient		0.013		
Channel Slope		0.00300	ft/ft	
Diameter		1.25	ft	
Discharge		1.11	ft³/s	
Results				
Normal Depth		0.49	ft	
Flow Area		0.45	ft²	
Wetted Perimeter		1.70	ft	
Hydraulic Radius		0.26	ft	
Top Width		1.22	ft	
Critical Depth		0.41	ft	
Percent Full		39.4	%	
Critical Slope		0.00584	ft/ft	
Velocity		2.47	ft/s	
Velocity Head		0.09	ft	
Specific Energy		0.59	ft	
Froude Number		0.72		
Maximum Discharge		3.74	ft³/s	
Discharge Full		3.43	ft³/s	
Slope Full		0.00034	ft/ft	
Flow Type	SubCritical			
GVF Input Data				
Downstream Depth		0.00	ft	
Length		0.00	ft	
Number Of Steps		0		
GVF Output Data				
Upstream Depth		0.00	ft	
Profile Description				
Profile Headloss		0.00	ft	
Average End Depth Over Rise		0.00	%	
Normal Depth Over Rise		39.41	%	
Downstream Velocity		Infinity	ft/s	

Worksheet for Line A, S=0.3%, Q=1.475

GVF Output Data

 Upstream Velocity
 Infinity
 ft/s

 Normal Depth
 0.49
 ft

 Critical Depth
 0.41
 ft

 Channel Slope
 0.00300
 ft/ft

 Critical Slope
 0.00584
 ft/ft

Worksheet for Line A, S=0.3%, Q=2.03

	worksneet for			
Project Description				
Friction Method	Kutter Formula			
Solve For	Normal Depth			
Input Data				
Roughness Coefficient		0.013		
Channel Slope		0.00300	ft/ft	
Diameter		1.25	ft	
Discharge		1.34	ft³/s	
Results				
Normal Depth		0.54	ft	
Flow Area		0.51	ft²	
Wetted Perimeter		1.80	ft	
Hydraulic Radius		0.28	ft	
Top Width		1.24	ft	
Critical Depth		0.46	ft	
Percent Full		43.6	%	
Critical Slope		0.00580	ft/ft	
Velocity		2.61	ft/s	
Velocity Head		0.11	ft	
Specific Energy		0.65	ft	
Froude Number		0.71		
Maximum Discharge		3.74	ft³/s	
Discharge Full		3.43	ft³/s	
Slope Full		0.00049	ft/ft	
Flow Type	SubCritical			
GVF Input Data				
Downstream Depth		0.00	ft	
Length		0.00	ft	
Number Of Steps		0		
GVF Output Data				
Upstream Depth		0.00	ft	
Profile Description				
Profile Headloss		0.00	ft	
Average End Depth Over Ris	se	0.00	%	
Normal Depth Over Rise		43.59	%	
Downstream Velocity		Infinity	ft/s	

Worksheet for Line A, S=0.3%, Q=2.03

GVF Output Data

 Upstream Velocity
 Infinity
 ft/s

 Normal Depth
 0.54
 ft

 Critical Depth
 0.46
 ft

 Channel Slope
 0.00300
 ft/ft

 Critical Slope
 0.00580
 ft/ft

Worksheet for Line B, S=0.63%,3/4 full

	orksneet for Li	ne B, 5=∪	.03%,3/4 tuli
Project Description			
Friction Method	Kutter Formula		
Solve For	Discharge		
Input Data			
Roughness Coefficient		0.013	
Channel Slope		0.00630	ft/ft
Normal Depth		0.63	ft
Diameter		1.50	ft
Results			
Discharge		2.96	ft³/s
Flow Area		0.70	ft²
Wetted Perimeter		2.11	ft
Hydraulic Radius		0.33	ft
Top Width		1.48	ft
Critical Depth		0.65	ft
Percent Full		41.7	%
Critical Slope		0.00533	ft/ft
Velocity		4.25	ft/s
Velocity Head		0.28	ft
Specific Energy		0.91	ft
Froude Number		1.09	
Maximum Discharge		8.94	ft³/s
Discharge Full		8.23	ft³/s
Slope Full		0.00084	ft/ft
Flow Type	SuperCritical		
GVF Input Data			
Downstream Depth		0.00	ft
Length		0.00	ft
Number Of Steps		0	
GVF Output Data			
Upstream Depth		0.00	ft
Profile Description			
Profile Headloss		0.00	ft
Average End Depth Over Rise		0.00	%
Normal Depth Over Rise		41.67	%
Downstream Velocity		Infinity	ft/s

Worksheet for Line B, S=0.63%,3/4 full

GVF Output Data

Upstream Velocity	Infinity	ft/s
Normal Depth	0.63	ft
Critical Depth	0.65	ft
Channel Slope	0.00630	ft/ft
Critical Slope	0.00533	ft/ft

Worksheet for Line B, S=0.63%,Q=1.99

	WOI KSHEEL IOI	Lilie D, 5-0	100 /0,4 = 1100	
Project Description				
Friction Method	Kutter Formula			
Solve For	Normal Depth			
Input Data				
Roughness Coefficient		0.013		
Channel Slope		0.00630	ft/ft	
Diameter		1.25	ft	
Discharge		1.99	ft³/s	
Results				
		0.55		
Normal Depth		0.55	ft	
Flow Area		0.52	ft²	
Wetted Perimeter		1.82	ft	
Hydraulic Radius		0.29	ft	
Top Width Critical Depth		1.24 0.56	ft ft	
Percent Full		44.1	%	
Critical Slope		0.00585	ft/ft	
Velocity		3.82	ft/s	
Velocity Head		0.23	ft	
Specific Energy		0.78	ft	
Froude Number		1.04	•	
Maximum Discharge		5.43	ft³/s	
Discharge Full		4.99	ft³/s	
Slope Full		0.00103	ft/ft	
Flow Type	SuperCritical			
GVF Input Data				
Downstream Depth		0.00	ft	
Length		0.00		
Number Of Steps		0		
GVF Output Data				
Upstream Depth		0.00	ft	
Profile Description		2.00	••	
Profile Headloss		0.00	ft	
Average End Depth Over Rise	•	0.00	%	
Normal Depth Over Rise		44.09	%	
Downstream Velocity		Infinity	ft/s	
-				

Worksheet for Line B, S=0.63%,Q=1.99

GVF Output Data

Upstream Velocity	Infinity	ft/s
Normal Depth	0.55	ft
Critical Depth	0.56	ft
Channel Slope	0.00630	ft/ft
Critical Slope	0.00585	ft/ft

Worksheet for Line B, S=0.63%,Q=2.13

	I KSHEEL IOI	Line b, 3-0	.03 /0,Q=2.13
Project Description			
Friction Method	Kutter Formula		
Solve For	Normal Depth		
	<u>'</u>		
Input Data			
Roughness Coefficient		0.013	
Channel Slope		0.00630	ft/ft
Diameter		1.50	ft
Discharge		2.13	ft³/s
Results			
Normal Depth		0.53	ft
Flow Area		0.55	ft²
Wetted Perimeter		1.90	ft
Hydraulic Radius		0.29	ft
Top Width		1.43	ft
Critical Depth		0.55	ft
Percent Full		35.1	%
Critical Slope		0.00528	ft/ft
Velocity		3.85	ft/s
Velocity Head		0.23	ft
Specific Energy		0.76	ft
Froude Number		1.09	
Maximum Discharge		8.94	ft³/s
Discharge Full		8.23	ft³/s
Slope Full		0.00045	ft/ft
Flow Type	SuperCritical		
GVF Input Data			
Downstream Depth		0.00	ft
Length		0.00	ft
Number Of Steps		0	
GVF Output Data			
Upstream Depth		0.00	ft
Profile Description			
Profile Headloss		0.00	ft
Average End Depth Over Rise		0.00	%
Normal Depth Over Rise		35.08	%
Downstream Velocity		Infinity	ft/s

Worksheet for Line B, S=0.63%,Q=2.13

GVF Output Data

Upstream Velocity	Infinity	ft/s
Normal Depth	0.53	ft
Critical Depth	0.55	ft
Channel Slope	0.00630	ft/ft
Critical Slope	0.00528	ft/ft

Worksheet for Line C -20 ", S=0.16%,3/4 full

		, -	
Project Description			
Friction Method	Kutter Formula		
Solve For	Discharge		
Input Data			
Roughness Coefficient		0.013	
Channel Slope		0.00160	ft/ft
Normal Depth		1.25	ft
Diameter		1.67	ft
Results			
Discharge		5.08	ft³/s
Flow Area		1.76	ft²
Wetted Perimeter		3.49	ft
		0.50	ft
Hydraulic Radius Top Width		1.45	ft
Critical Depth		0.84	ft
Percent Full		74.9	%
Critical Slope		0.00525	ft/ft
Velocity		2.89	ft/s
Velocity Head		0.13	ft
Specific Energy		1.38	ft
Froude Number		0.46	
Maximum Discharge		5.99	ft³/s
Discharge Full		5.52	ft³/s
Slope Full		0.00136	ft/ft
Flow Type	SubCritical		
GVF Input Data			
Downstream Depth		0.00	ft
Length		0.00	
Number Of Steps		0.00	II.
GVF Output Data			
Upstream Depth		0.00	ft
Profile Description			
Profile Headloss		0.00	ft
Average End Depth Over Rise		0.00	%
Normal Depth Over Rise		74.85	%
Downstream Velocity		Infinity	ft/s

Worksheet for Line C -20 ", S=0.16%,3/4 full

GVF Output Data

Upstream Velocity	Infinity	ft/s
Normal Depth	1.25	ft
Critical Depth	0.84	ft
Channel Slope	0.00160	ft/ft
Critical Slope	0.00525	ft/ft

Worksheet for Line C -20 ", S=0.16% full flow

Project Description				
Friction Method	Kutter Formula			
Solve For	Discharge			
	3			
Input Data				
Roughness Coefficient		0.013		
Channel Slope		0.00160	ft/ft	
Normal Depth		1.56	ft	
Diameter		1.67	ft	
Results				
Discharge		6.00	ft³/s	
Flow Area		2.13	ft²	
Wetted Perimeter		4.38	ft	
Hydraulic Radius		0.49	ft	
Top Width		0.83	ft	
Critical Depth		0.92	ft	
Percent Full		93.4	%	
Critical Slope		0.00545	ft/ft	
Velocity		2.82	ft/s	
Velocity Head		0.12	ft	
Specific Energy		1.68	ft	
Froude Number		0.31		
Maximum Discharge		5.99	ft³/s	
Discharge Full		5.52	ft³/s	
Slope Full		0.00188	ft/ft	
Flow Type	SubCritical			
GVF Input Data				
Downstream Depth		0.00	ft	
Length		0.00		
Number Of Steps		0		
GVF Output Data				
Upstream Depth		0.00	ft	
Profile Description		0.00	IL.	
Profile Headloss		0.00	ft	
Average End Depth Over Rise		0.00	%	
Normal Depth Over Rise		93.41	%	
Downstream Velocity		Infinity	ft/s	
20 mondani volodity			.40	

Worksheet for Line C -20 ", S=0.16% full flow

GVF Output Data

Upstream Velocity	Infinity	ft/s
Normal Depth	1.56	ft
Critical Depth	0.92	ft
Channel Slope	0.00160	ft/ft
Critical Slope	0.00545	ft/ft

Worksheet for Line C, S=0.16%,Q=3.74

	KSHEEL IOI	Line C, 3-0	· 10 /0,Q=3.7 -
Project Description			
Friction Method	Kutter Formula		
Solve For	Normal Depth		
Input Data			
Roughness Coefficient		0.013	
Channel Slope		0.00160	ft/ft
Diameter		1.67	ft
Discharge		3.74	ft³/s
Results			
Normal Depth		1.00	ft
Flow Area		1.37	ft²
Wetted Perimeter		2.96	ft
Hydraulic Radius		0.46	ft
Top Width		1.64	ft
Critical Depth		0.71	ft
Percent Full		60.1	%
Critical Slope		0.00506	ft/ft
Velocity		2.72	ft/s
Velocity Head		0.12	ft
Specific Energy		1.12	ft
Froude Number		0.52	
Maximum Discharge		5.99	ft³/s
Discharge Full		5.52	ft³/s
Slope Full		0.00075	ft/ft
Flow Type	SubCritical		
GVF Input Data			
Downstream Depth		0.00	ft
Length		0.00	ft
Number Of Steps		0	
GVF Output Data			
Upstream Depth		0.00	ft
Profile Description			
Profile Headloss		0.00	ft
Average End Depth Over Rise		0.00	%
Normal Depth Over Rise		60.06	%
Downstream Velocity		Infinity	ft/s

Worksheet for Line C, S=0.16%,Q=3.74

GVF Output Data

 Upstream Velocity
 Infinity
 ft/s

 Normal Depth
 1.00
 ft

 Critical Depth
 0.71
 ft

 Channel Slope
 0.00160
 ft/ft

 Critical Slope
 0.00506
 ft/ft

Worksheet for Line C, S=0.16%,Q=4.27

	orksheet for Li	ine C, 5=U	.16%,Q=4.2 <i>1</i>
Project Description			
Friction Method	Kutter Formula		
Solve For	Normal Depth		
Input Data			
Roughness Coefficient		0.013	
Channel Slope		0.00160	ft/ft
Diameter		1.67	ft
Discharge		4.27	ft³/s
Results			
Normal Depth		1.10	ft
Flow Area		1.52	ft²
Wetted Perimeter		3.15	ft
Hydraulic Radius		0.48	ft
Top Width		1.59	ft
Critical Depth		0.77	ft
Percent Full		65.6	%
Critical Slope		0.00511	ft/ft
Velocity		2.80	ft/s
Velocity Head		0.12	ft
Specific Energy		1.22	ft
Froude Number		0.50	
Maximum Discharge		5.99	ft³/s
Discharge Full		5.52	ft³/s
Slope Full		0.00097	ft/ft
Flow Type	SubCritical		
GVF Input Data			
Downstream Depth		0.00	ft
Length		0.00	ft
Number Of Steps		0	
GVF Output Data			
Upstream Depth		0.00	ft
Profile Description			
Profile Headloss		0.00	ft
Average End Depth Over Rise		0.00	%
Normal Depth Over Rise		65.60	%
Downstream Velocity		Infinity	ft/s

Worksheet for Line C, S=0.16%,Q=4.27

GVF Output Data

Upstream Velocity	Infinity	ft/s
Normal Depth	1.10	ft
Critical Depth	0.77	ft
Channel Slope	0.00160	ft/ft
Critical Slope	0.00511	ft/ft

Worksheet for Line C, S=0.4%,Q=4.54

			,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	
Project Description				
Friction Method	Kutter Formula			
Solve For	Normal Depth			
Input Data				
Roughness Coefficient		0.013		
Channel Slope		0.00400	ft/ft	
Diameter		1.75	ft	
Discharge		4.54	ft³/s	
Results				
Normal Depth		0.83	ft	
Flow Area		1.12	ft²	
Wetted Perimeter		2.66	ft	
Hydraulic Radius		0.42	ft	
Top Width		1.75	ft	
Critical Depth		0.78	ft	
Percent Full		47.4	%	
Critical Slope		0.00498	ft/ft	
Velocity		4.04	ft/s	
Velocity Head		0.25	ft	
Specific Energy		1.08	ft	
Froude Number		0.89		
Maximum Discharge		10.82	ft³/s	
Discharge Full		9.98	ft³/s	
Slope Full		0.00085	ft/ft	
Flow Type	SubCritical			
GVF Input Data				
Downstream Depth		0.00	ft	
Length		0.00		
Number Of Steps		0		
GVF Output Data				
·		0.00	4	
Upstream Depth		0.00	ft	
Profile Description		0.00	#	
Profile Headloss		0.00	ft %	
Average End Depth Over Rise		47.39	%	
Normal Depth Over Rise Downstream Velocity		Infinity	% ft/s	
Downstream velocity		ппппц	IVO	

Worksheet for Line C, S=0.4%,Q=4.54

GVF Output Data

 Upstream Velocity
 Infinity
 ft/s

 Normal Depth
 0.83
 ft

 Critical Depth
 0.78
 ft

 Channel Slope
 0.00400
 ft/ft

 Critical Slope
 0.00498
 ft/ft

Worksheet for Line D. S=0.4%.1/2 full

	Worksheet for	Line D, S=0).4%,1/2 full	
Project Description				
Friction Method	Kutter Formula			
Solve For	Normal Depth			
Input Data				
Roughness Coefficient		0.013		
Channel Slope		0.00400	ft/ft	
Diameter		1.00	ft	
Discharge		1.05	ft³/s	
Results				
Normal Depth		0.49	ft	
Flow Area		0.39	ft²	
Wetted Perimeter		1.56	ft	
Hydraulic Radius		0.25	ft	
Top Width		1.00	ft	
Critical Depth		0.43	ft	
Percent Full		49.4	%	
Critical Slope		0.00653	ft/ft	
Velocity		2.72	ft/s	
Velocity Head		0.11	ft	
Specific Energy		0.61	ft	
Froude Number		0.77		
Maximum Discharge		2.34	ft³/s	
Discharge Full		2.15	ft³/s	
Slope Full		0.00098	ft/ft	
Flow Type	SubCritical			
GVF Input Data				
Downstream Depth		0.00	ft	
Length		0.00	ft	
Number Of Steps		0		
GVF Output Data				
Upstream Depth		0.00	ft	
Profile Description				
Profile Headloss		0.00	ft	
Average End Depth Over Ris	se	0.00	%	
Normal Depth Over Rise		49.35	%	
Downstream Velocity		Infinity	ft/s	

Worksheet for Line D, S=0.4%,1/2 full

GVF Output Data

Upstream Velocity	Infinity	ft/s
Normal Depth	0.49	ft
Critical Depth	0.43	ft
Channel Slope	0.00400	ft/ft
Critical Slope	0.00653	ft/ft

Worksheet for Line E, S=0.4%, Q=5.45

	OI KSIICEL IOI	Lille L, 0-0	i + 70; Q - 51 + 5	
Project Description				
Friction Method	Kutter Formula			
Solve For	Normal Depth			
Input Data				
Roughness Coefficient		0.013		
Channel Slope		0.00400	ft/ft	
Diameter		1.75	ft	
Discharge		9.06	ft³/s	
Results				
Normal Depth		1.30	ft	
Flow Area		1.91	ft²	
Wetted Perimeter		3.63	ft	
Hydraulic Radius		0.53	ft	
Top Width		1.53	ft	
Critical Depth		1.12	ft	
Percent Full		74.1	%	
Critical Slope		0.00594	ft/ft	
Velocity		4.74	ft/s	
Velocity Head		0.35	ft	
Specific Energy		1.65	ft	
Froude Number		0.75		
Maximum Discharge		10.82	ft³/s	
Discharge Full		9.98	ft³/s	
Slope Full		0.00331	ft/ft	
Flow Type	SubCritical			
GVF Input Data				
Downstream Depth		0.00	ft	
Length		0.00	ft	
Number Of Steps		0		
GVF Output Data				
Upstream Depth		0.00	ft	
Profile Description				
Profile Headloss		0.00	ft	
Average End Depth Over Rise		0.00	%	
Normal Depth Over Rise		74.10	%	
Downstream Velocity		Infinity	ft/s	

Worksheet for Line E, S=0.4%, Q=5.45

GVF Output Data

 Upstream Velocity
 Infinity
 ft/s

 Normal Depth
 1.30
 ft

 Critical Depth
 1.12
 ft

 Channel Slope
 0.00400
 ft/ft

 Critical Slope
 0.00594
 ft/ft

Worksheet for Line E, S=0.16%,Q=5.32

	KSHCCL IOI	Lilie L, G-U	110 /0,4-0102
Project Description			
Friction Method	Kutter Formula		
Solve For	Normal Depth		
Innut Data			
Input Data			
Roughness Coefficient		0.013	
Channel Slope		0.00160	ft/ft
Diameter		1.67	ft
Discharge		5.32	ft³/s
Results			
Normal Depth		1.31	ft
Flow Area		1.83	ft²
Wetted Perimeter		3.62	ft
Hydraulic Radius		0.51	ft
Top Width		1.37	ft
Critical Depth		0.86	ft
Percent Full		78.4	%
Critical Slope		0.00531	ft/ft
Velocity		2.90	ft/s
Velocity Head		0.13	ft
Specific Energy		1.44	ft
Froude Number		0.44	
Maximum Discharge		5.96	ft³/s
Discharge Full		5.49	ft³/s
Slope Full		0.00150	ft/ft
Flow Type	SubCritical		
GVF Input Data			
Downstream Depth		0.00	ft
Length		0.00	ft
Number Of Steps		0	
GVF Output Data			
Upstream Depth		0.00	ft
Profile Description		2.00	
Profile Headloss		0.00	ft
Average End Depth Over Rise		0.00	%
Normal Depth Over Rise		78.38	%
Downstream Velocity		Infinity	ft/s
-			

Worksheet for Line E, S=0.16%,Q=5.32

GVF Output Data

 Upstream Velocity
 Infinity
 ft/s

 Normal Depth
 1.31
 ft

 Critical Depth
 0.86
 ft

 Channel Slope
 0.00160
 ft/ft

 Critical Slope
 0.00531
 ft/ft



Appendix D

Sewer Area Study Arrow Pit Development dated June 2017



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SEWER AREA STUDY

Arrow Pit Development

Irwindale, CA

Prepared for:

Irwindale Partners 2 510 E Foothill Blvd, Suite 206 San Dimas, CA 91773

Prepared under the Supervision of:

John C. Hogan, P.E. R.C.E. No. 26229

March 16th, 2017 (revised June 2017)

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1. PROJECT DESCRIPTION

The existing 77-acre quarry site sits in the triangular area bounded by Arrow Highway to the north, Live Oak Ave to the south, and the 605 Freeway to the east. The site is currently being filled to rough graded condition and will ultimately be developed as a mixed-use facility consisting of warehouse, retail, and restaurant space. See Appendix A for project site plan. The project site currently does not discharge into the City of Irwindale's sewer system.

2. PURPOSE OF STUDY

The following study was prepared to determine if the existing sanitary sewer main in Live Oak Ave has the capacity to accept the flows from the proposed Arrow Pit Development Project. The expected flows from the proposed development will be compared to the assumed flows from the original sewer design. Our study also revises the original sewer design calculations to utilize Kutter's Formula and the updated pipe capacity requirements discussed further below.

3. ORIGINAL SEWER DESIGN FLOWS

The original design of the Live Oak Sewer was performed by Kenneth Mullen, Consulting Engineers (See **Appendix D**). In the study "LA Marketplace – Sewer main Design Live Oak Ave", the assumed tributary areas to the sewer main in Live Oak Ave between Arrow Highway and the 605 Freeway included the Arrow Pit site. The assumed flow that was used at the time for all of the tributary areas was 80 gpd/1,000 SF and the calculated daily flow rate for the Arrow Pit site was 0.39 cfs. These numbers were based on a theoretical future land use consisting of warehouse, office buildings, and restaurant space. The assumed flows from the Arrow Pit site and the LA Marketplace (now the Irwindale Speedway) resulted in calculations showing that a minimum 12" pipe was needed at 0.4% slope. The calculations utilized Manning's Equation to determine the required pipe sizes. Per the record drawings (See **Appendix E**) a 15" pipe at 0.3% slope was built in Live Oak Ave.

4. PROPOSED DEVELOPMENT FLOWS

It is anticipated that the proposed Arrow Pit development will consist of 1.355 million SF of warehouse, 47,000 SF of retail space, and 33,000 SF of restaurants. Using the LA County Sanitation Districts (LACSD) generations tables, an average flow of 57.2 gpd/1,000 SF can be assumed for the area resulting in total daily flow rate of 0.13 cfs. Peak flow in each line was determined by multiplying the average daily flow rate of each pipe by the factor of 2.5 per LACSD. These calculations can be seen in **Appendix B** and in a summary **Table 1** and **Table 2** below. In order to obtain conservative values, the

retail space was calculated as a "Shopping Center" per the LACSD table, however it is more likely to generate flows closer to "Store" (225 gpd/1,000 SF less than "Shopping Center"). The LACSD generation table is attached in **Appendix C** for reference.

TABLE 1

	TRIBUTARY AREA BY LAND USE							
	LACSD	AREA	WILSRV LOADS	FLOW				
	DESCRIPTION	SF	GPD/1000SF	GPD				
Warehouse	Warehouse	1355000	25	33875				
Retail	Shopping Center	47000	325	15275				
Restaurants	Restaurant	33000	1000	33000				
TOTAL	-	1435000	-	82150				
-	WEIGHTED AVG	0.0572	GPD	-				
_	-	57.2	GPD/1000SF	-				
_	AVG DAILY FLOW	0.13	CFS	-				

TABLE 2 – PEAK FLOW IN EACH PIPE LINE

	Q (CFS)	Q _P (CFS)	NOTES
LINE A	0.53	1.32	
LINE B	0.80	1.99	
LINE C	1.64	4.11	$Q_A+Q_B+Q_C$
LINE D	0.42	1.04	
LINE E	2.06	5.15	Q _{CT} +Q _D

5. SEWER PIPE CAPACITY ANALYSIS

Per the record drawings, a 15" pipe at 0.3% slope was built in Live Oak Avenue (See **Appendix E**). An updated sewer capacity analysis was done to revise the calculations utilizing Kutter's Formula and the requirement of pipe sizes greater than 15 inches to flow ¾ full and pipe sizes 15 inches and less to flow ½ full. Using Kutter's Formula in flowmaster, with 15" pipe, a slope of 0.003 ft/ft, a roughness coefficient of 0.013, and a peak flow of 1.32 cfs, the pipe was 43.2 percent full. The result shows that the existing 15" pipe has sufficient capacity to handle the discharge from the proposed Arrow Pit development. See **Appendix B** for the Flowmaster calculation results and a summary in **Table 3** below.

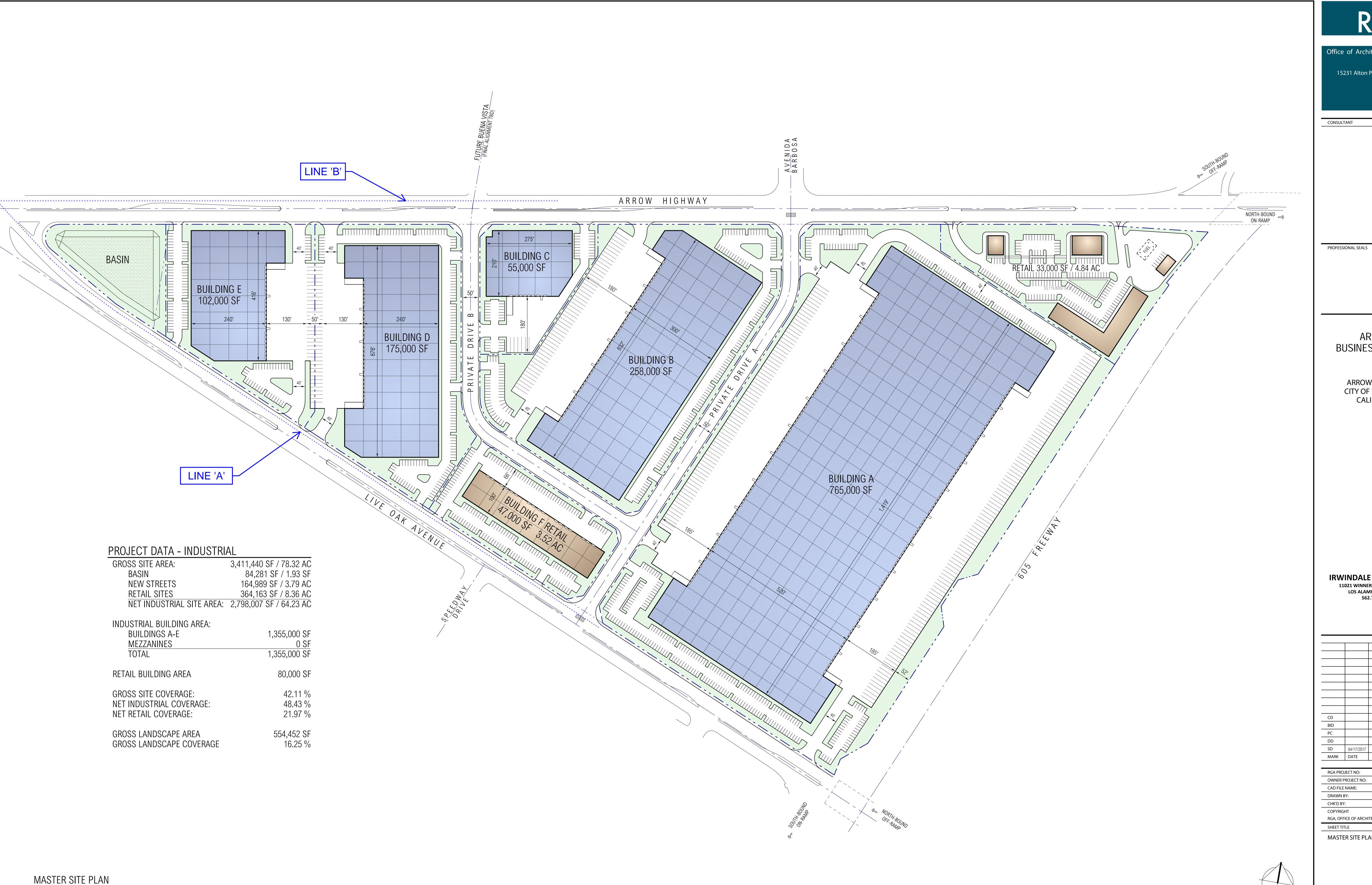
TABLE 3 – SEWER CAPACITY ANALYSIS SUMMARY

	Q _P (CFS)	PIPE (IN)	%FULL	EX PIPE	EX SLOPE
				(IN)	(%)
LINE A	1.32	15	43.2	15	0.3
LINE B	1.99	18	38.1	-	-
LINE C	4.11	18	57.2	21	0.4
LINE D	1.04	12	49.1	-	-
LINE E	5.15	18	66.3	-	-

6. SUMMARY OF RESULTS

Our conservative flow estimate average of 57.2 gpd/1,000 SF is considerably less than the original assumed design flow average of 80 gpd/1,000 SF. Similarly, the anticipated total daily flow volume for the proposed Arrow Pit development is 3 times less (0.13 cfs vs 0.39 cfs) than what the City's sewer main was originally designed to accept from the 77-acre property. This is due to the conservative nature of the original design, which assumed that commercial buildings would cover the entire footprint of the tributary areas. Since our calculated flows are significantly lower than the original design, we conclude that there is sufficient capacity to handle the discharge from the proposed Arrow Pit development.

Proposed Arrow Pit Site Plan



Office of Architectural Design 15231 Alton Parkway, Suite 100 Irvine, CA 92618 T 949-341-0920 FX 949-341-0922

BUSINESS CENTER

ARROW HIGHWAY CITY OF IRWINDALE CALIFORNIA

IRWINDALE PARTNERS, LP 11021 WINNERS CIRCLE, SUITE 200 LOS ALAMITOS, CA 90720 562.799.2366

PC
DD
SD 04/17/2017 SCHEMATIC DESIGN
MARK DATE DESCRIPTION

RGA PROJECT NO: 16152.00

RGA, OFFICE OF ARCHITECTURAL DESIGN

MASTER SITE PLAN

Proposed Arrow Pit Flow Calculations



JOB DESCRIPTION ARROW PIT
CALCULATION FOR AVERAGE FLOW CALCS

BY OF SHEETS

CHECKED BY

DATE

(REVISED 06/01/17)

SHEETS

DATE

LAND USE

1,355,000 SF - WAREHOUSE 25 gpd
$$= 33,875$$
 gpd $= 33,875$ gpd $= 47,000$ SF - RETAIL (SHOPPING CENTER) - 325 gpd $= 15,275$ gpd $= 33,000$ SF - RESTAURANT $= 1,000$ gpd $= 33,000$ gpd

$$\frac{1,355,000}{1,355,000} = \frac{(2597)_{10005F} + 47,0005F(32597)_{10005F} + 33,0005F(1,0005F)_{10005F}}{1,355,000} = \frac{47,0005F(32597)_{10005F} + 33,0005F(1,0005F)_{10005F}}{1,355,000} = \frac{1,355,000}{1,0005F} = \frac{1,0005F}{1,0005F} = \frac{1,0005F}$$

33,875
$$gpd + 15,275 gpd + 33,000 gpd = 82,150 gpd$$

82,150 $Spd \times \frac{1day}{24hr} \times \frac{1hr}{60 min} \times \frac{1min}{60 sec} \times \frac{1 cF}{7.48 gnl}$
= 0.13 cfs DAILY FLOW

ORIGINAL DESIGN ASSUMED 0.39 CFS DAILY FLOW FROM PROJECT SITE [72.3 Ac x 0.0054 cfs/Ac = 0.39 cfs]

By: PTBD Date: Revised 6/1/2017

TRIBUTARY AREA BY LAND USE							
	FLOW GPD						
Warehouse	Warehouse	33875					
Retail	Shopping Center	47000	325	15275			
Restaurants	staurants Restaurant 33000 1000 33						
TOTAL	TOTAL - 1435000 - 82150						
-	WEIGHTED AVG	/G 0.0572 GPD -					
57.2 GPD/1000SF							
-	AVG DAILY FLOW	0.13	CFS	-			

100111

A. TRIBUTARY FLOWS						
LINE A		LIVE OAK B/W AF	ROW HWY &	SAN GABRIEL	RIVER FWY	
2114271	AREA (AC)	AVG Q (CFS)		- O, 114 O, 1511122		
ASSESSOR MAP	74.15	0.400				
PROJECT SITE	32.94	0.127				
TOTAL	107.093	0.528				
TOTAL	107.095	0.526				
LINE B	Λ.	RROW HWY B/W	IIVE OAK AVE	S. CAN GARD	IEI DIVED EWAY	
LINE D	AREA (AC)	AVG Q (CFS)	LIVE OAK AVE	& SAN GADIN	ILL KIVLK I VV I	
ASSESSOR MAP	147.55	0.797				
PROJECT SITE	0.00	0.000				
TOTAL	147.550	0.797				
LINE C	LIVE	LOAK AVE FROM	550' EAST OF	PECK ROAD T	O ARROW HW	Y
	AREA (AC)	AVG Q (CFS)				
ASSESSOR MAP	58.98	0.318				
PROJECT SITE	0.00	0.000				
TOTAL	58.980	0.318				
	72					
LINE D		EASEMENT S. C	F LIVE OAK 5!	50' EAST OF PI	ECK ROAD	<u> </u>
	AREA (AC)	AVG Q (CFS)				
ASSESSOR MAP	77.2	0.417				
PROJECT SITE	0.00	0.000				
TOTAL	77.200	0.417				
TOTAL	77.200	0.417				
B. SIZE OF PIPELINES						
1. FLOWMASTER USED F	OR CALCULATI	ONS				
1. I LOWINASTER OSED I	<15" PIPE	FLOW 1/2 FULL				
	>15" PIPE	FLOW 3/4 FULL				
	>13 FIFE	11000 3/41011				
2. PEAK FLOW IN EACH I	DIDELINE	MULTIPLY AVG Q	RV 2 5 TO OR	ΤΔΙΝΙ ΡΕΔΚ ΕΙ ()W	
2. FLAR I LOW IN LACIT	Q (CFS)	QP (CFS)	NOTES	TAINTLAKTE	J V V	
LINE A	0.528	1.32	NOTES			
LINE B	0.797	1.99				
			04.00.00			
LINE C	1.643	4.11	QA+QB+QC			
LINE D	0.417	1.04	0.07.00			
LINE E	2.060	5.15	QCT+QD			
A DETERMANDE DIDE CITE						
3. DETERMINE PIPE SIZE	I					
n	0.013	0.002 f LINE A				
S	0.004	0.003 for LINE A				
Qp Diameter	See Table 2					
Diameter		ermine based on				
	<15" PIPE	FLOW 1/2 FULL	50%			
ما د م د	>15" PIPE	FLOW 3/4 FULL	75%			
depth		ermine based on				
	<15" PIPE	FLOW 2/4 FULL	50%			
	>15" PIPE	FLOW 3/4 FULL	75%			
	0 (070)		_			
	Q _P (CFS)	PIPE (IN)	%FULL	EX PIPE (IN)	EX SLOPE (%)	
LINE A	1.32	15	43.2	15	0.3	
LINE B	1.99	18	38.1	i	-	
LINE C	4.11	18	57.2	21	0.4	
LINE D	1.04	12	49.1	-	-	
LINE E	5.15	18	66.3	-	-	
*SEE FLOWMASTER SHE						

LINE A - 15IN 43%

Project Description			
Friction Method	Kutter Formula		
Solve For	Normal Depth		
Input Data			
Roughness Coefficient		0.013	
Channel Slope		0.00300	ft/ft
Diameter		15.00	in
Discharge		1.32	ft³/s
Results			
Normal Depth		6.49	in
Flow Area		0.51	ft²
Wetted Perimeter		1.79	ft
Hydraulic Radius		3.40	in
Top Width		1.24	ft
Critical Depth		0.45	ft
Percent Full		43.2	%
Critical Slope		0.00580	ft/ft
Velocity		2.60	ft/s
Velocity Head		0.10	ft
Specific Energy		0.65	ft
Froude Number		0.71	
Maximum Discharge		3.74	ft³/s
Discharge Full		3.43	ft³/s
Slope Full		0.00047	ft/ft
Flow Type	SubCritical		
GVF Input Data			
Downstream Depth		0.00	in
Length		0.00	ft
Number Of Steps		0	
GVF Output Data			
Upstream Depth		0.00	in
Profile Description			
Profile Headloss		0.00	ft
Average End Depth Over Rise		0.00	%
Normal Depth Over Rise		43.24	%
Downstream Velocity		Infinity	ft/s

LINE A - 15IN 43%

GVF Output Data

 Upstream Velocity
 Infinity
 ft/s

 Normal Depth
 6.49
 in

 Critical Depth
 0.45
 ft

 Channel Slope
 0.00300
 ft/ft

 Critical Slope
 0.00580
 ft/ft

	LINE B	- 18IN 38	3%		
Project Description					
Friction Method	Kutter Formula				
Solve For	Normal Depth				
Input Data					
Roughness Coefficient		0.013			
Channel Slope		0.00400	ft/ft		
Diameter		18.00	in		
Discharge		1.99	ft³/s		
Results					
Normal Depth		6.86	in		
Flow Area		0.62	ft²		
Wetted Perimeter		2.00	ft		
Hydraulic Radius		3.72	in		
Top Width		1.46	ft		
Critical Depth		0.53	ft		
Percent Full		38.1	%		
Critical Slope		0.00527	ft/ft		
Velocity		3.21	ft/s		
Velocity Head		0.16	ft		
Specific Energy		0.73	ft		
Froude Number		0.87			
Maximum Discharge		7.11	ft³/s		
Discharge Full		6.55	ft³/s		
Slope Full		0.00040	ft/ft		
Flow Type	SubCritical				
GVF Input Data					
Downstream Depth		0.00	in		
Length		0.00	ft		
Number Of Steps		0			
GVF Output Data					
Upstream Depth		0.00	in		
Profile Description					
Profile Headloss		0.00	ft		
Average End Depth Over Rise		0.00	%		
Normal Depth Over Rise		38.13	%		

Infinity ft/s

Downstream Velocity

LINE B - 18IN 38%

GVF Output Data

Upstream Velocity Infinity ft/s Normal Depth 6.86 in Critical Depth 0.53 ft Channel Slope 0.00400 ft/ft Critical Slope 0.00527 ft/ft

LINE C - 18IN 57%

	LINE	: - 18IN 57	<u>%</u>	
Project Description				
Friction Method	Kutter Formula			
Solve For	Normal Depth			
Input Data				
Roughness Coefficient		0.013		
Channel Slope		0.00400	ft/ft	
Diameter		18.00	in	
Discharge		4.11	ft³/s	
Results				
Normal Depth		10.30	in	
Flow Area		1.05	ft²	
Wetted Perimeter		2.57	ft	
Hydraulic Radius		4.88	in	
Top Width		1.48	ft	
Critical Depth		0.78	ft	
Percent Full		57.2	%	
Critical Slope		0.00559	ft/ft	
Velocity		3.93	ft/s	
Velocity Head		0.24	ft	
Specific Energy		1.10	ft	
Froude Number		0.83		
Maximum Discharge		7.11	ft³/s	
Discharge Full		6.55	ft³/s	
Slope Full		0.00160	ft/ft	
Flow Type	SubCritical			
GVF Input Data				
Downstream Depth		0.00	in	
Length		0.00	ft	
Number Of Steps		0		
GVF Output Data				
Upstream Depth		0.00	in	
Profile Description				
Profile Headloss		0.00	ft	
Average End Depth Over Rise		0.00	%	
Normal Depth Over Rise		57.25	%	
Downstream Velocity		Infinity	ft/s	

LINE C - 18IN 57%

GVF Output Data

 Upstream Velocity
 Infinity
 ft/s

 Normal Depth
 10.30
 in

 Critical Depth
 0.78
 ft

 Channel Slope
 0.00400
 ft/ft

 Critical Slope
 0.00559
 ft/ft

LINE D - 12IN 49%

	LINE D	- 12IN 49	%	
Project Description				
Friction Method	Kutter Formula			
Solve For	Normal Depth			
Input Data				
Roughness Coefficient		0.013		
Channel Slope		0.00400	ft/ft	
Diameter		12.00	in	
Discharge		1.04	ft³/s	
Results				
Normal Depth		5.89	in	
Flow Area		0.38	ft²	
Wetted Perimeter		1.55	ft	
Hydraulic Radius		2.96	in	
Top Width		1.00	ft	
Critical Depth		0.43	ft	
Percent Full		49.1	%	
Critical Slope		0.00655	ft/ft	
Velocity		2.71	ft/s	
Velocity Head		0.11	ft	
Specific Energy		0.61	ft	
Froude Number		0.77		
Maximum Discharge		2.34	ft³/s	
Discharge Full		2.15	ft³/s	
Slope Full		0.00097	ft/ft	
Flow Type	SubCritical			
GVF Input Data				
Downstream Depth		0.00	in	
Length		0.00	ft	
Number Of Steps		0		
GVF Output Data				
Upstream Depth		0.00	in	
Profile Description				
Profile Headloss		0.00	ft	
Average End Depth Over Rise		0.00	%	
Normal Depth Over Rise		49.09	%	

Infinity ft/s

Downstream Velocity

LINE D - 12IN 49%

GVF Output Data

 Upstream Velocity
 Infinity
 ft/s

 Normal Depth
 5.89
 in

 Critical Depth
 0.43
 ft

 Channel Slope
 0.00400
 ft/ft

 Critical Slope
 0.00655
 ft/ft

LINE E - 18IN 66%

LINE E - 18IN 66%											
Project Description											
Friction Method	Kutter Formula										
Solve For	Normal Depth										
Input Data											
Roughness Coefficient		0.013									
Channel Slope		0.00400	ft/ft								
Diameter		18.00	in								
Discharge		5.15	ft³/s								
Results											
Normal Depth		11.94	in								
Flow Area		1.24	ft²								
Wetted Perimeter		2.86	ft								
Hydraulic Radius		5.23	in								
Top Width		1.42	ft								
Critical Depth		0.87	ft								
Percent Full		66.3	%								
Critical Slope		0.00592	ft/ft								
Velocity		4.14	ft/s								
Velocity Head		0.27	ft								
Specific Energy		1.26	ft								
Froude Number		0.78									
Maximum Discharge		7.11	ft³/s								
Discharge Full		6.55	ft³/s								
Slope Full		0.00249	ft/ft								
Flow Type	SubCritical										
GVF Input Data											
Downstream Depth		0.00	in								
Length		0.00	ft								
Number Of Steps		0									
GVF Output Data											
Upstream Depth		0.00	in								
Profile Description											
Profile Headloss		0.00	ft								
Average End Depth Over Rise		0.00	%								
Normal Depth Over Rise		66.35	%								

Infinity ft/s

Downstream Velocity

LINE E - 18IN 66%

GVF Output Data

Upstream Velocity Infinity ft/s Normal Depth 11.94 in Critical Depth 0.87 ft Channel Slope 0.00400 ft/ft Critical Slope 0.00592 ft/ft

LACSD Loadings for Each Class of Land Use

TABLE 1
LOADINGS FOR EACH CLASS OF LAND USE

DESCRIPTION	UNIT OF MEASURE	FLOW (Gallons Per Day)	COD (Pounds Per Day)	SUSPENDED SOLIDS (Pounds Per Day)
<u></u>				
RESIDENTIAL				
Single Family Home	Parcel	260	1.22	0.59
Duplex	Parcel	312	1.46	0.70
Triplex	Parcel	468	2.19	1.05
Fourplex	Parcel	624	2.92	1.40
Condominiums	Parcel	195	0.92	0.44
Single Family Home	Parcel	156	0.73	0.35
(reduced rate)				
Five Units or More	No. of Dwlg. Units	156	0.73	0.35
Mobile Home Parks	No. of Spaces	156	0.73	0.35
COMMERCIAL				
Hotel/Motel/Rooming House	Room	125	0.54	0.28
Store	$1000 \; \mathrm{ft}^2$	100	0.43	0.23
Supermarket	$1000 \mathrm{ft}^2$	150	2.00	1.00
Shopping Center	1000 ft^2	325	3.00	1.17
Regional Mall	1000 ft^2	150	2.10	0.77
Office Building	1000 ft^2	200	0.86	0.45
Professional Building	1000 ft^2	300	1.29	0.68
Restaurant	1000 ft^2	1,000	16.68	5.00
Indoor Theatre	1000 ft^2	125	0.54	0.28
Car Wash				
Tunnel - No Recycling	1000 ft^2	3,700	15.86	8.33
Tunnel - Recycling	1000 ft^2	2,700	11.74	6.16
Wand	1000 ft^2	700	3.00	1.58
Financial Institution	1000 ft^2	100	0.43	0.23
Service Shop	$1000 \; \mathrm{ft}^2$	100	0.43	0.23
Animal Kennels	1000 ft^2	100	0.43	0.23
Service Station	1000 ft^2	100	0.43	0.23
Auto Sales/Repair	1000 ft^2	100	0.43	0.23
Wholesale Outlet	1000 ft^2	100	0.43	0.23
Nursery/Greenhouse	1000 ft^2	25	0.11	0.06
Manufacturing	1000 ft^2	200	1.86	0.70
Dry Manufacturing	1000 ft^2	25	0.23	0.09
Lumber Yard	1000 ft^2	25	0.23	0.09
Warehousing	1000 ft^2	25	0.23	0.09
Open Storage	$1000 \; \mathrm{ft}^2$	25	0.23	0.09
Drive-in Theatre	$1000~\mathrm{ft}^2$	20	0.09	0.05

TABLE 1
(continued)
LOADINGS FOR EACH CLASS OF LAND USE

DESCRIPTION	UNIT OF MEASURE	FLOW (Gallons <u>Per Day)</u>	COD (Pounds <u>Per Day)</u>	SUSPENDED SOLIDS (Pounds <u>Per Day)</u>
COMMERCIAL				
Night Club Bowling/Skating Club Auditorium, Amusement Golf Course, Camp, and Park (Structures and Improvements Recreational Vehicle Park Convalescent Home Laundry Mortuary/Cemetery Health Spa, Gymnasium With Showers Without Showers Convention Center, Fairground, Racetrack, Sports Stadium/Arena	1000 ft ² 4verage Daily Attendance	350 150 125 350 100 55 125 3,825 100 600 300	1.50 1.76 0.54 1.50 0.43 0.34 0.54 16.40 1.33 2.58 1.29	0.79 0.55 0.27 0.79 0.23 0.14 0.28 8.61 0.67 1.35 0.68
INSTITUTIONAL				
College/University Private School Church	Student 1000 ft ² 1000 ft ²	20 200 50	0.09 0.86 0.21	0.05 0.45 0.11

LA Marketplace Sewer Design Live Oak Study

BY B.L. HALL DATE 8/11/92

ARCADIA. CALIFORNIA

SHEET NO. ____ OF 8

(213) 681-5428

(818) 445-2212

SUBJECT LA MARKET PLACE - SEWER DESIGN LIVEDAK ANE

DETERMINE SIZE OF PROPOSED SOUDEMAIN REQUIRED TO SERVE ENTIRE TRIBUTARY AREA (SEE ATTACHED MAP)

DESIGN CEITERIA:

MIN. PIDE SIZE = 8" MIN. VELOCITY = Zfps PRELINE FLOWING 1/2 FULL FOR 0 5 10" PIREUNE FLOWING 3/4 FULL FOR 0 > 10" PRAKING FACTORS DETERMINED FROM ATTACHED CUEVES CURRENT ZONING: MZ OR QUARRY

DETERMINE GENERATION PATES:

THE TYPES OF USES ALLOWED IN AN M-2 ZONE ARE MOSTLY "DRY USES", IC. THEY DO NOT PRODUCE LARGE VOLUMES OF SEWAGE. DISCUSSIONS WITH CITY STAFF INDICATE THAT SOME USES WHICH PRODUCE MORE SENAGE MAY BE ALLOWED, SICH AS RESTAURANTS OR R&D PARKS, ESDECIALLY ALONG THE FREEWAY FRONTAGE. THELEFORE, SONAGE GENERATION PATES COULD VARY BETWEEN 1000 gpd/10005F TO 25gpd/10005F.

GIVEN THE LAND REQUIREMENTS FOR THE MZ USES AND THOSE FOR RESTAURANT USES, A COMPROMISE USING AN AVERAGE SOURCE GENERATION RATE WOULD BE APPROPRIATE. THE MAJORITY OF LAND WOULD UNDOUBLEDLY BEDEVOTED TO USES SUCH AS LUMBER YARD, WARREHOUSING, AUTOSALES, TRUCKING & SOME OFFICE TYPE USES. VERY SMALL AMOUNTS OF LAND WOULD BE DEVOTED TO MORE INTENSIVE USES SUCH AS RESTAURANTS & HEALTH CLUBS.

A TOTAL OF 357 ACRES, PLUSTHEPROJECTSITE, ARE TELBUTARY TO THE SUBJECT SEWER MAIN: OF THIS CARGE SINGLE PARCES OF IDACKES OR MORE EQUAL 287 ACKES.

KENN	ETH I. MULLEN, CON	SULTING ENGINEERS,	INC.		
BY B.L. HML DATE	ARCADIA.	CALIFORNIA	SHEET NO	2	_ OF 8
CHKD DATE	(213) 681-5428	(818) 445-2212	JOB NO		
SUBJECT LA MARKET	PLACE - SEWER	DESIGN LIVE DAK	AVE.		

THE FOLLOWING IS A THEORETICAL BEEAKOOWN BY LANDUSE TYPE OF THE TRIBUTARY AREA:

SEWAGE * AREA WAREHOUSING, LUMBORYAND, OPEN STORAGE, NURSBRY, DRY MANUPACTURING ETC. 287 25 apd/1000 SF

OFFICE BUOG., R&D ETC, AUTO SALES 60AL 200gpd 10005F

RESTAURANT 10AC 1000gpd 11000SF

USE A "WEIGHTED AVG"

287 (259 pd/1000) + 60 (200) + 10 (1000) = 81,79 pd/1000 SF

AVERAGE SOUNDE GOVERATION USE 80 9 pd/1000 SF FOR SURROUNDING PROPERTIES CONVERT TO COS/ACRE

Q = 809Pd /1000SF × 10PM × 1MR × 1M × 1CF × 43560SF = ,0054 cfs/Ac

DETERMINE SOURCE VOLUME FOR LAMARKET PLACE ESTIMATED ATTENDANCE = 20,000 PEOPLE PERDAY

* SEWAGE GENERATION = 10 gpd/ PERSON (ATTENDANCE) Q = 109pd/person x 20,000 x 1CF x 1000 x 1HE x 1m 600 605

= 0.3095 cfs

OF FROM ATTACHED LETTER FROM LA CO. SAN DIST.

BY B.L. HALLDATE 8/11/92

ARCADIA, CALIFORNIA

(213) 681-5428

(818) 445-2212

JOB NO._ SUBJECT LA MARKET PLACE - SELVER MAIN DESIGN IN LIVE DAK AVE

A, DETERMINE TRIBUTARY FLOWS

1. LINE "A" LIVE OAK AVE BETWEEN ARROW HWY & SAN GABRIEL RIVER FLUY

TELBUTARY AREA IN ACRES (FROM ASSESSOR'S MAPS) AREA = 60+12.3+1.85+ PROJECT SITE

QAT=74.15Ac (,0054cts/Ac) + 0,3095cts = 0.71 cfs AVG. DAY FLOW

2. LINE "B" ARROW HUY BENNESS LIVEDAK AVE & SAN GABRIEL BUER FWY

TELBUTARY AREA IN ACRES (GROM ASSESSOR'S MAPS)

= 10,6+12,4+35,78+44,85+43,92

= 147.55

Que 147.55x,0054 Cfs/AC

= 0.80 CFS

3. LINE "C" LIVE DAK AVE. FROM 550 BAST OF PECK ROAD TO APROW HWY TELBUTARY AREA IN ACRES (FROM ASSESSOR'S MAPS)

> M-2 USE = 1.55+1.55+2.0+2.0+2.45B+3.598+6.054 + 0,4 + 0,3 + 2,29 + 6,93 + 4,0 + 22,06 + 0,4 +0,2+2,02+0,28+0,23+0,36+0,3 = 58.98AC

Ucr= 58.98 x ,0054cfs/AC = 0.32 cfs

BY B.L. HALL DATE 8/11/92

(213) 681-5428

(818) 445-2212

LA MARICET PLACE - SCHER MAIN DESIGN LIVEDAK AVE.

4. LINE"D" EASEMENT SO. OF LIVE DAK SOD EAST OF PECK PO. TRIBUTARY AREA IN ACRES (FROM ASSESSOR'S MAPS) M-2 USE = 9,3 +4,77 + 14,3+45,53 +3,3 = 17.20 AC

> Qof= 77,20Ac x .0054 cfs/Ac = 0.42 cfs

B. DETERMINE SIZE OF PIDEUNES

1. DERIVE STANDARD EQUASIONS

a, ASSUME PIDELINES \$ 10"\$ FLOWING 1/2 FULL USE MANNING'S EQN. & SOLVE FOR DIAMETER

WHERE: A= AREA OF FLOW = 1/2 (TOZZ) = TOZZ $R_{H} = \frac{A}{P} = \frac{1/2}{1600} = \frac{D}{4}$

n=1013

THEREFORE: Q= 11.486) (=) 43 51/2 Q= (17.81) D2 (D2/3) 51/2 Q= 17.81 08/3 51/2 FOR PIPES \(\leq 10"\ph BY B. L. HALL DATE 8/11/92

ARCADIA, CALIFORNIA

SHEET NO. 5 OF B

(213) 681-5428

(818) 445-2212

JOB NO. LAMMENT PLACE - SEWER MAIN DESIGN LIVE OME ANE

b. ASSUME PIPELINES > 10" & FLOWING 3/4 FULL USE MANNING'S EQN & SOLVE FOR DIAMETER

WHERE: A = AREA OF FLOW = 0.632D2 FROM TABLE 7-4 * RH= = 0.302D FROM TABLE 7-5 &

N=1013

* KING'S HANDBOOK OF HYDRAULICS PAGE 7-35 FOR 0/0 = 0.75

THEREFORE: Q = 0.63202 (1.486) (0.3020)23 51/2 = $92.52 D^{2}(D^{2/3}) s^{1/2}$ Q = 32.52 08/3 6"2 FOR PIPES 710"\$

2. DETERMINE PEAK FLOWIN EACH PIDELINE

a LINE "A"

F= 2.8 GROW ATTACHED GRAPH F16,2-5 LAGSAN DIST.

QAO= 0.71 (2.8) = 1,99cts

BY B.L. HALL DATE 8/11/92

ARCADIA, CALIFORNIA

SHEET NO. 6 OF 8

(213) 681-5428

(818) 445-2212

JOB NO.__

MARKET PLACE - SOLVER MAIN DESIGN LIVEDAK AVE

b. LINE "B"

C. LINE "C"

= 0.71+0.80+0.32

= 1.83 cfs

d. LINE "D"

F = 2.9 FROM ATTACHED

e. LINE "E"

F = 2.45 FROM ATTACHED GRAPH

BY B.L. HALLBATE B/11/92

ARCADIA. CALIFORNIA

SHEET NO __ 7 OF B

CHKD_____DATE______ (213) 681-5428 (818) 445-2212 JOB NO_____ SUBJECT_LA MARKET PLACE - SEWER MAIN DESIGN LIVE DAIL AVE

3, DETERMINE PIRE SIZES

a. LINE A ASSUME D> 10"\$

Q= 32.52 D8/3 51/2 S= ,004

1.99 = 32.52 D 8/3 (,004) 1/2

D8/3 = 0.9675

D = 0.99 ft = 11.85 INCHES USE 12" PIPE

b. LINEB ASSUME D > 10"

Q= 32,520 8/3 5 1/2 5=,004

2.16 = 32.520 43 (.004) 1/2

D8/3= 1.05

D = 1.02 ft = 12.2 IN. USE 12"PIPE

C. LINE C ASSUME D>10"

Q = 32.52 D 93 512 5=,004

4.58 cfs = 32.52 00/3 (.004) 12

D8/3 = 2,23

D = 1.35 ft = 16.2 IN. USE 18" PIRE

d. LINED ASSUME 0> 10"

Q= 32,5208/35"/2 5=.004

1,22 = 32.52 0 8/3 (.004) 1/2

D \$3 = 0.5932

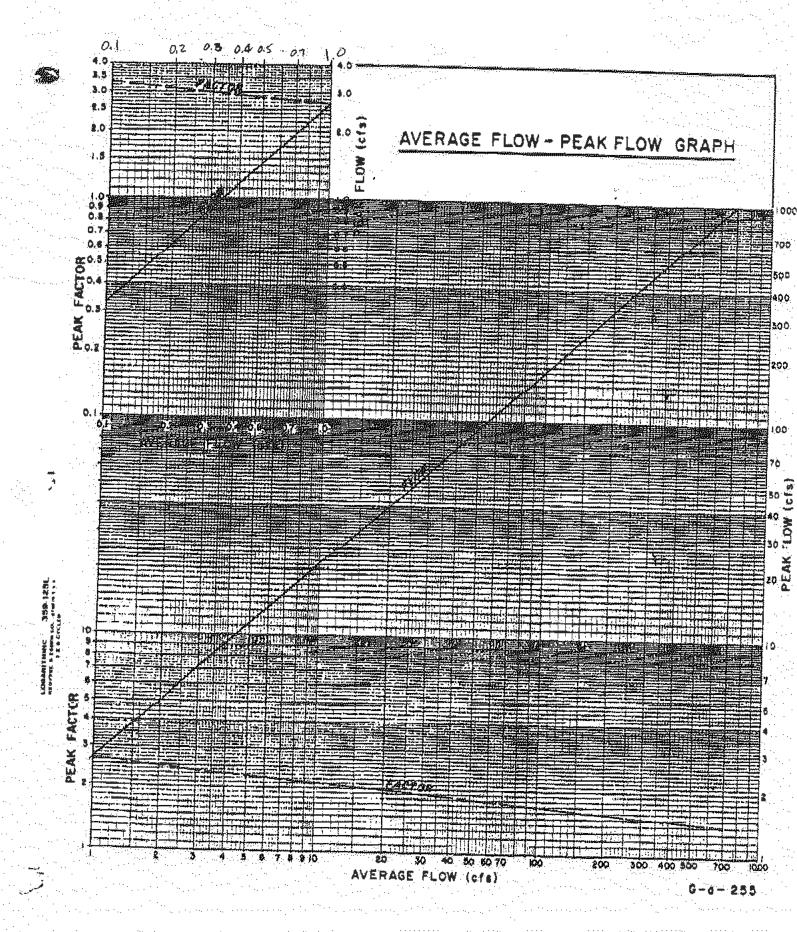
D = 0.82 ft = 9.87 USE 10" PIPE

KENNETH I. MULLEN, CONSULTING ENGINEERS, INC.

BY B.L. HALL DATE B/11/97 ARCADIA. CALIFORNIA SHEET NO. 8 OF B

CHKD DATE (213) 681-5428 (818) 445-2212 JOB NO. SUBJECT LA MARKET PLACE - SEWER MAIN DESIGN LIVE OAK AVE.

e line E Assume D710" $Q = 32.52 D^{8/3} S''^2 \qquad S = .004$ $5.51 = 32.52 D^{8/3} (.004)''^2$ $D^{8/3} = 2.68$ $D = 1.45 \text{ ft} = 17.36 \text{ in}. \quad USE 18'' \text{ pipe}$





COUNTY SANITATION DISTRICTS OF LOS ANGELES COUNTY

1955 Workman Mill Road, Whittier, CA 90601-4998 Mailing Address: P. O. Box 4998, Whittier, CA 90607-4998 Telephone: (213) 699-7411, (213) 685-5217

CHARLES W. CARRY Chief Engineer and General Manager

October 5, 1989

File No: JOA-00.00-00

Ms. Barbara Hull Kenneth Mullen Consulting Engineers 325 North Santa Anita Avenue Arcadia, CA 91006

Dear Ms. Hull:

Standard Wastewater Discharge Factors

Enclosed, per your request, is a copy of the standard wastewater discharge factors used by the Sanitation Districts.

If you have any questions regarding this information, please contact the undersigned at (213) 699-7411, extension 2704.

Very truly yours,

Charles W. Carry

David B. Bruns

Supervising Civil Engineer

Financial Planning &

Property Management Section

JB. R

DBB:mah

Enclosure

LOADINGS FOR EACH CLASS OF LAND USE

TABLE 1

DESCRIPTION	UNIT OF MEASURE	FLOW (Gallons per Day)	COD (Pounds per Day)	SUSPENDED SOLIDS (Pounds per Day)
RESIDENTIAL				
Single Family Home	Parcel	260	1.22	0.59
Duplex	Parcel	312	1.46	0.70
Triplex	Parcel	468	2.19	1.05
Fourplex	Parcel	624	2.92	1.40
Condominiums	Parcel	156	0.73	0.35
Single Family Home (reduced rate)	Parcel	156	0.73	0.35
Five Units or More	No. of Dwlg. Units	156	0.73	0.35
Mobile Home Parks	No. of Spaces	156	0.73	0.35
COMMERCIAL				
Hotel/Motel/Rooming House	Room	125	0.54	0.28
Store	1000 ft ²	100	0.43	0.23
Supermarket	1000 ft ²	150	2.00	1.00
Shopping Center	1000 ft ²	325	3.00	1.17
Office Building	1000 ft ²	200	0.86	0.45
Professional Building	1000 ft ²	300	1.29	0.68
Restaurant	1000 ft ²	1,000	16.68	5.00
Indoor Theatre	1000 ft ²	125	0.54	0.28
Car Wash				
Tunnel Type	1000 ft ²	3,700	15.86	8.33
Wand Type	1000 ft ²	700	3.00	1.58
Financial Institution	1000 ft^2	100	0.43	0.23
Service Shop	1000 ft ²	100	0.43	0.23
Animal Kennels	1000 ft ²	100	0.43	0.23
Service Station	1000ft^2	100	0.43	0.23
Auto Sales/Repair	1000 ft ²	100	0.43	0.23
Wholesale Outlet	1000 ft ²	100	0.43	0.23
Nursery/Greenhouse	1000 ft ²	25	0.11	0.06
Manufacturing	1000 ft ²	200	1.86	0.70
Dry Manufacturing	1000 ft ²	25	0.23	0.09
Lumber Yard	1000 ft ²	25	0.23	0.09
Warehousing	1000 ft ²	25	0.23	0.09
Open Storage	1000 ft ²	25	0.23	0.09
Drive-in Theatre	1000 ft ²	20	0.09	0.05
Night Club	1000 ft ²	350	1.50	0.79
Bowling/Skating	1000 ft^2	150	1.76	0.55

TABLE 1
(continued)

LOADINGS FOR EACH CLASS OF LAND USE

DESCRIPTION	UNIT OF MEASURE	FLOW (Gallons per Day)	COD (Pounds per Day)	SUSPENDED SOLIDS (Pounds per Day)
COMMERCIAL				
Club Auditorium, Amusement Golf Course, Camp, and Park (Structures and Improvements)	1000 ft ² 1000 ft ² 1000 ft ²	37 350 100	0.16 1.50 0.43	0.08 0.79 0.23
Convalescent Home Laundry Mortuary/Cemetery Health Spa, Gymnasium With Showers Without Showers Convention Center, Fairground, Racetrack, Sports Stadium/Arena	Bed 1000 ft ² 1000 ft ² 1000 ft ² 1000 ft ² Average Daily Attendance	125 3,825 100 600 300	0.54 16.40 1.33 2.58 1.29	0.28 8.61 0.67 1.35 0.68
INSTITUTION College/University Private School Church (noncharitable)	A L Student 1000 ft ² 1000 ft ²	20 200 50	0.09 0.86 0.21	0.05 0.45 0.11

STEADY UNIFORM FLOW IN OPEN CHANNELS 7-35

Table 7-4. For Determining the Area a of the Cross Section of a Circular Conduit Flowing Part Full

Let depth of water $\frac{D}{d}$ and $C_a =$ the tabulated value. Then $a = C_a d^3$.

Then

Let $\frac{\text{depth of water}}{\text{bottom width of channel}} = \frac{D}{b}$ and $C_{\bar{y}} = \text{tabulated}$ value.

 $\bar{v} = C_{\bar{v}}D$.

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-	.0400	0470	.0534	0090	8990	.0739	1180.	0885	1960	.1039
N	1118	159	1281	.1365	1449	.1535	.1623	11711	800	.1890
60	.1982	2074	2167	2250	.2355	.2450	.2546	2642	2739	.2836
4	2934	3032	.3130	.3229	.3328	.3428	.3527	.3627	.3727	3827
10	.393	.403	.413	.423	.433	.443	.453	.462	.472	.482
9	.492	.502	.512	.521	.531	.540	.550	.559	.569	.578
1	.587	.596	909.	.614	.623	.632	.640	.649	.657	999.
00	.674	.681	689	269.	.704	.712	.719	.725	.732	.738
0	.745	.750	.756	.761	.766	.771	.775	.779	.782	.784

Table 7-5. For Determining the Hydraulic Radius r of the Cross Let depth of where $=\frac{D}{A}$ and C_r = the tabulated value. Then $r=C_rd$. Section of a Circular Conduit Flowing Part Full

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ė	_	-	-	_	_	_	-	-	-	-
.07	.045	.104	.157	.202	.240	.270	.292	.303	.302	278
90.	.039	660.	.152	.198	.236	.268	.290	302	.303	283
.05	.033	.093	.147	.193	.233	.265	.288	.302	.303	286
.04	.026	780.	.142	.189	.229	.262	.286	.301	.304	980
g	.020	.081	.136	.185	.226	.259	.284	.300	.304	606
20'	.013	.075	.131	.180	.222	.256	.282	.299	.304	204
10.	700.	020.	.126	921.	.218	.253	.280	.298	.304	906
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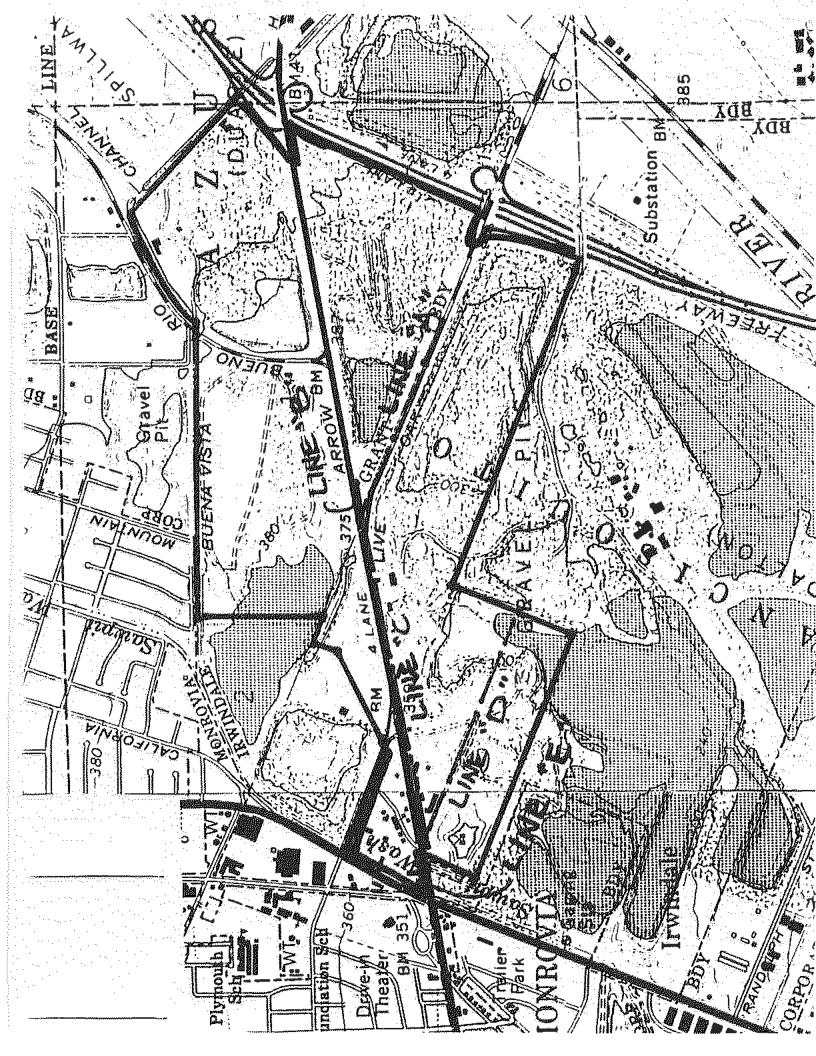
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	4-1	.472	.452	.438	.426	.417	408	.403	397	.393	.389	385	.377	.373	.370	.367	364	362	.360	.359	.357	9	0000	.355	.354	.353	.352
tical	3-1	.478	.462	.448	.438	.420	.421	.415	400	404	.400	.393	.387	.382	.378	.375	372	370	.367	365	.364	000	70c.	.361	.359	.358	.357
Side alopes of channel, ratio of horizontal to vertical	214-1	.481	.467	.455	.444	.436	.429	.422	.417	.412	407	8 7 :	.394	.389	388	.381	378	37.5	.373	.370	.368	i c	100.	.365	.364	.362	.361
rizonta	2-1	.485	.472	.462	.452	.444	438	.431	.426	.421	.417	409	.403	.397	.393	.389	300	382	.380	.377	.375	1	0/0	.371	.370	.368	.367
o of ho	174-1	.488	.478	.469	.462	.455	448	.443	.438	.433	.420	.421	.415	.409	404	.400	396	393	.390	387	.385	Ġ	700.	.380	.378	.377	.375
el, rati	1	.492	.485	.478	.472	.467	.462	.457	.452	.448	.444	.438	.431	.426	.421	.417	413	409	.406	.403	.400	Š	/Ac-	.395	.393	.391	.389
f chann	34-1	494	.488	.483	.478	474	.469	465	.462	.458	.455	.448	.443	.438	.433	.420	425	.421	.418	.415	.412	5	AO#	.407	404	.402	.400
dopes o	1-56	.496	.492	.488	.485	.481	.478	475	.472	.469	.467	.462	.457	.452	.448	.444	.441	438	.434	.431	.429	907	09#	.423	.421	.419	.417
Side B	1-1/	.498	.496	494	.492	.490	488	.487	.485	.483	.481	.478	.475	.472	.469	.467	464	462	.459	.457	.455	2	707.	.420	.448	.446	.444
	1/8-1	.499	.498	.497	.496	.495	494	.493	.492	.491	.490	.488	.487	.485	.483	.481	.480	478	.477	.475	474	110	7/1	.471	.469	.468	.467
q	٩	0.05	Τ.	-15	ų	-25	က့	.35	4.	.45	20.	9.	.7	οó	ø.	1.0	1:1	1.2	1.3	1.4	1.5	9	2 .	1.7	1.8	1.9	2.0

Table 7-3. For Determining the Vertical Distance y below the Water Surface to the Center of Gravity of a Cross Section

of a Trapezoidal Channel

HANDBOOK OF HYDRAULICS

7-34



¥60

SUBDIVISION OF THE RANCHO AZUSA DE DUA M.R. 6 - 80 - 82

POR. SEC.36, T.IN., R.IIW.

FOR PERY, ASSAUTT, SEE: 13770 - 32

CHESTY OF LES AND PROPERTY. offer S.abfillists

BVD

8532

SCALE 1" - 400" 10 BUENA VISTA S.F. 1 (D) 8533 POR SE I/4 SECT, TIS, RIW. * 111 - 25 - 24 GABREL (e)

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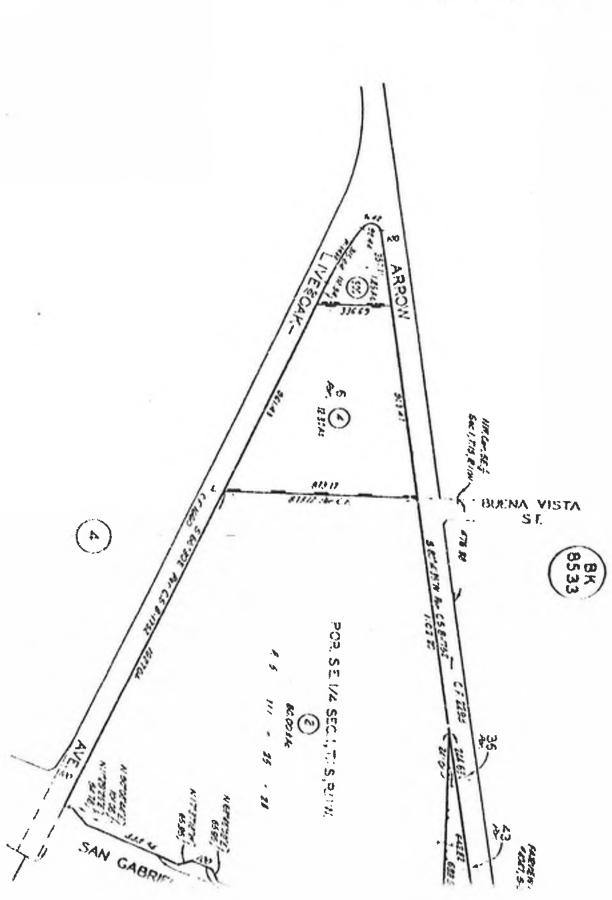
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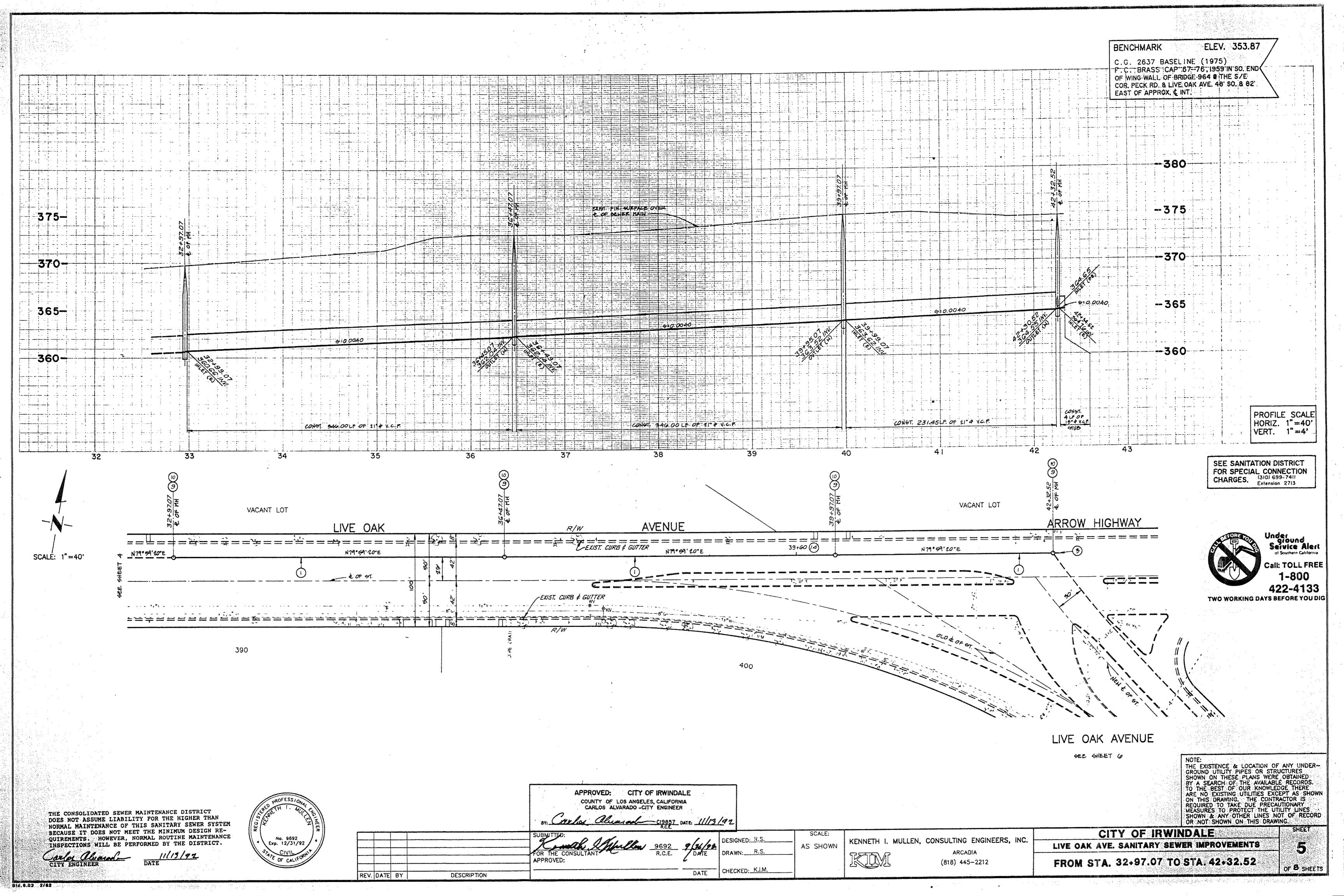
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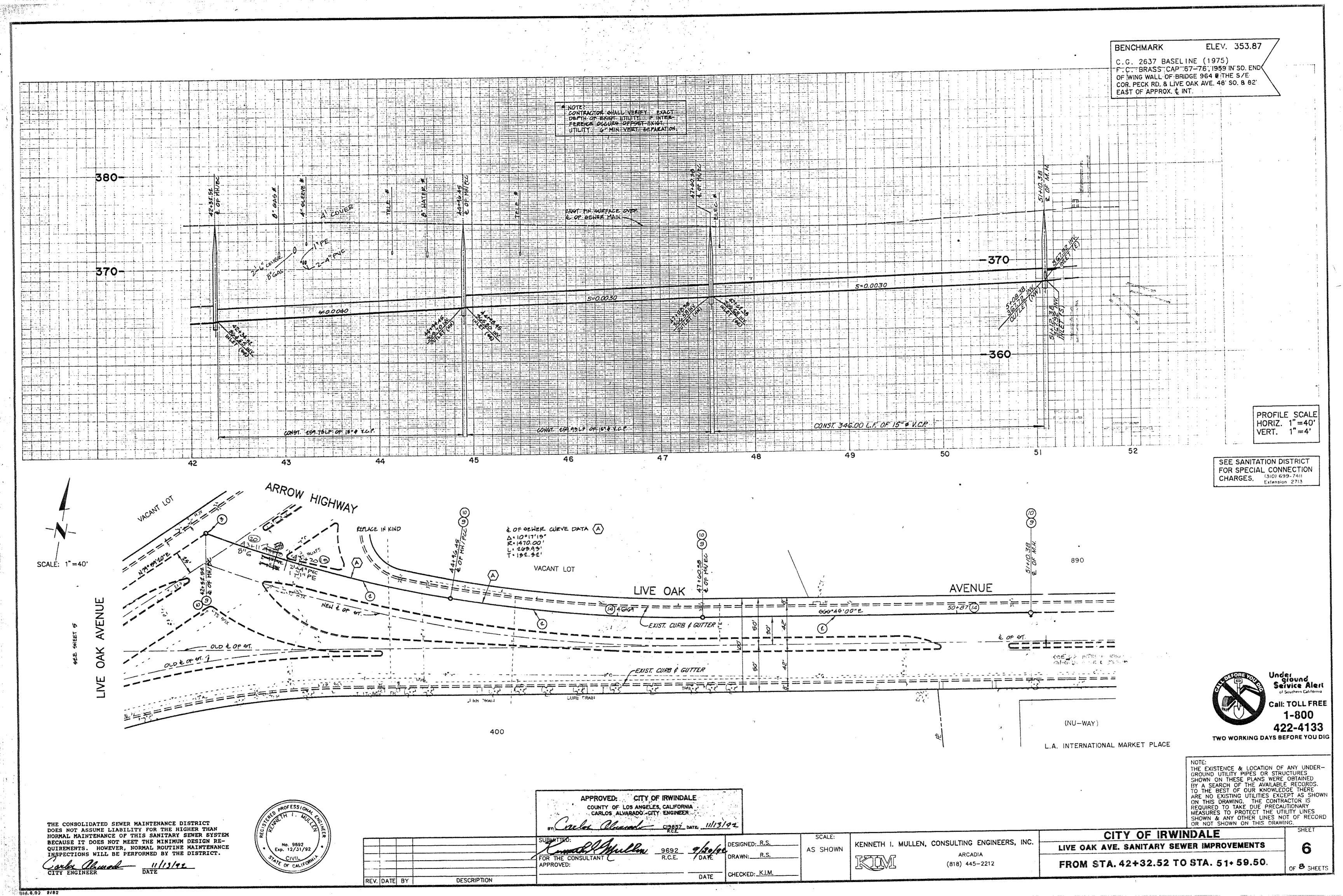
All \$25 series porcess on this page are essessed to the freindale Community Redevelopment Agency, unless otherwise noted.

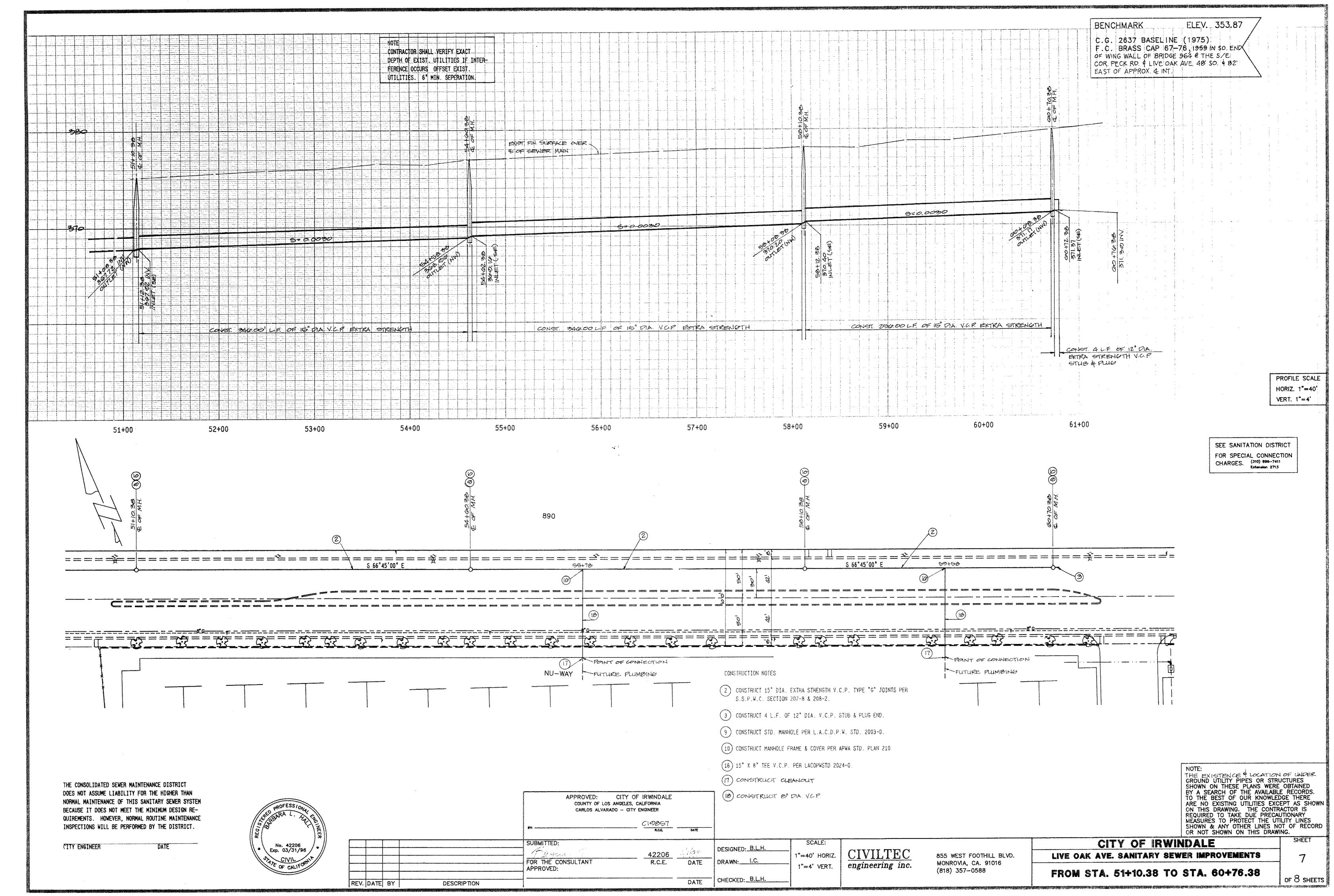
SCALE 1"

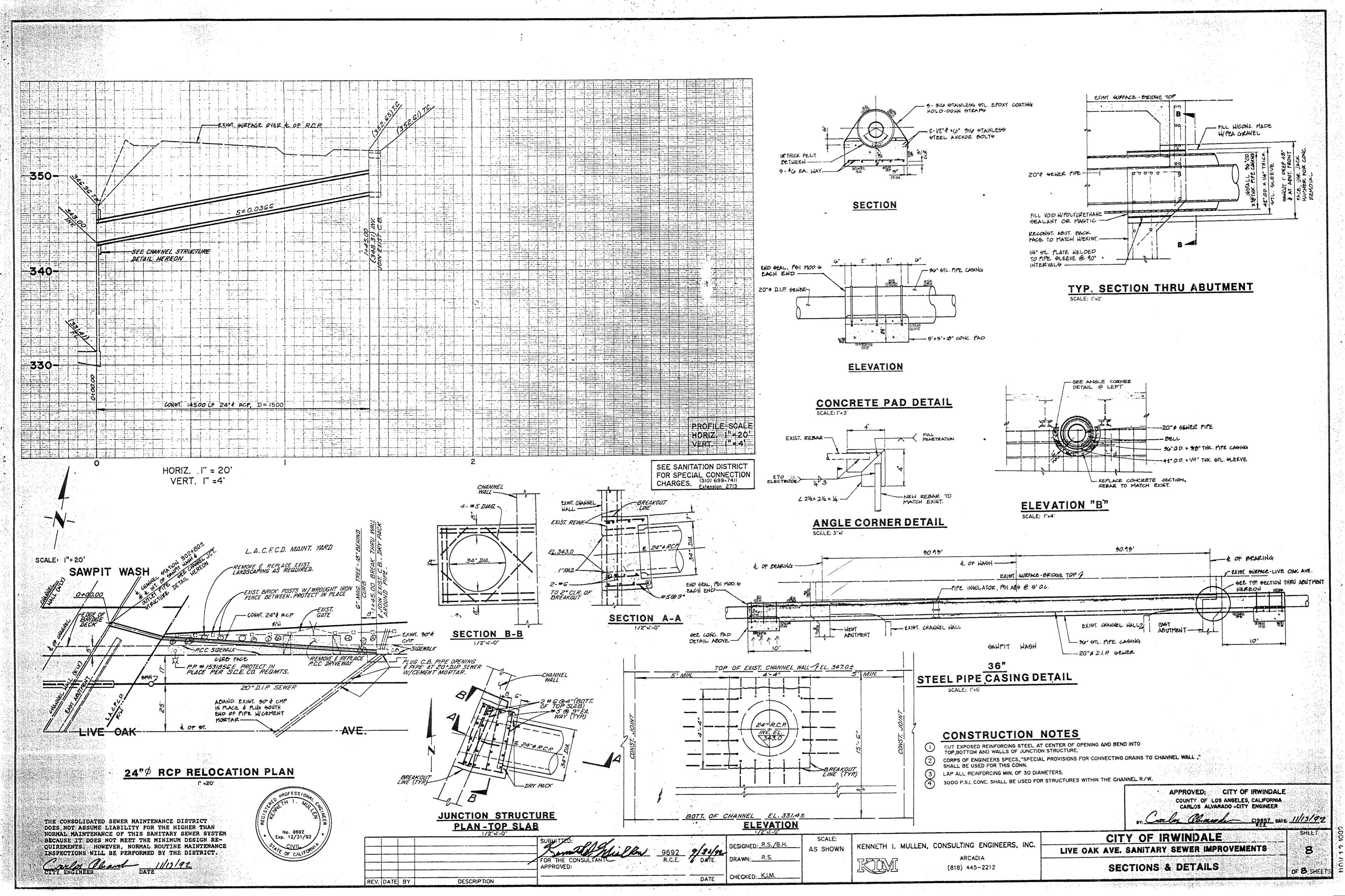


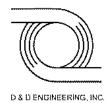
Live Oak Sanitary Sewer Improvement Plans











Appendix E

LA Marketplace Sewer Design Live Oak Study

KENN	ETH I. MULLEN, CON	SULTING ENGINEERS,	INC.		
BY B.L. HML DATE	ARCADIA.	CALIFORNIA	SHEET NO	2	_ OF 8
CHKD DATE	(213) 681-5428	(818) 445-2212	JOB NO		
SUBJECT LA MARKET	PLACE - SEWER	DESIGN LIVE DAK	AVE.		

THE FOLLOWING IS A THEORETICAL BEEAKOOWN BY LANDUSE TYPE OF THE TRIBUTARY AREA:

SEWAGE * AREA WAREHOUSING, LUMBORYAND, OPEN STORAGE, NURSBRY, DRY MANUPACTURING ETC. 287 25 apd/1000 SF

OFFICE BUOG., R&D ETC, AUTO SALES 60AL 200gpd 10005F

RESTAURANT 10AC 1000gpd 11000SF

USE A "WEIGHTED AVG"

287 (259 pd/1000) + 60 (200) + 10 (1000) = 81,79 pd/1000 SF

AVERAGE SOUNDE GOVERATION USE 80 9 pd/1000 SF FOR SURROUNDING PROPERTIES CONVERT TO COS/ACRE

Q = 809Pd /1000SF × 10PM × 1MR × 1M × 1CF × 43560SF = ,0054 cfs/Ac

DETERMINE SOURCE VOLUME FOR LAMARKET PLACE ESTIMATED ATTENDANCE = 20,000 PEOPLE PERDAY

* SEWAGE GENERATION = 10 gpd/ PERSON (ATTENDANCE) Q = 109pd/person x 20,000 x 1CF x 1000 x 1HE x 1m 600 605

= 0.3095 cfs

OF FROM ATTACHED LETTER FROM LA CO. SAN DIST.

BY B.L. HALLDATE 8/11/92

ARCADIA, CALIFORNIA

(213) 681-5428

(818) 445-2212

JOB NO._ SUBJECT LA MARKET PLACE - SELVER MAIN DESIGN IN LIVE DAK AVE

A, DETERMINE TRIBUTARY FLOWS

1. LINE "A" LIVE OAK AVE BETWEEN ARROW HWY & SAN GABRIEL RIVER FLUY

TELBUTARY AREA IN ACRES (FROM ASSESSOR'S MAPS) AREA = 60+12.3+1.85+ PROJECT SITE

QAT=74.15Ac (,0054cts/Ac) + 0,3095cts = 0.71 cfs AVG. DAY FLOW

2. LINE "B" ARROW HUY BENNESS LIVEDAK AVE & SAN GABRIEL BUER FWY

TELBUTARY AREA IN ACRES (GROM ASSESSOR'S MAPS)

= 10,6+12,4+35,78+44,85+43,92

= 147.55

Que 147.55x,0054 Cfs/AC

= 0.80 CFS

3. LINE "C" LIVE DAK AVE. FROM 550 BAST OF PECK ROAD TO APROW HWY TELBUTARY AREA IN ACRES (FROM ASSESSOR'S MAPS)

> M-2 USE = 1.55+1.55+2.0+2.0+2.45B+3.598+6.054 + 0,4 + 0,3 + 2,29 + 6,93 + 4,0 + 22,06 + 0,4 +0,2+2,02+0,28+0,23+0,36+0,3 = 58.98AC

Ucr= 58.98 x ,0054cfs/AC = 0.32 cfs

BY B.L. HALL DATE 8/11/92

(213) 681-5428

(818) 445-2212

LA MARICET PLACE - SCHER MAIN DESIGN LIVEDAK AVE.

4. LINE"D" EASEMENT SO. OF LIVE DAK SOD EAST OF PECK PO. TRIBUTARY AREA IN ACRES (FROM ASSESSOR'S MAPS) M-2 USE = 9,3 +4,77 + 14,3+45,53 +3,3 = 17.20 AC

> Qof= 77,20Ac x .0054 cfs/Ac = 0.42 cfs

B. DETERMINE SIZE OF PIDEUNES

1. DERIVE STANDARD EQUASIONS

a, ASSUME PIDELINES \$ 10"\$ FLOWING 1/2 FULL USE MANNING'S EQN. & SOLVE FOR DIAMETER

WHERE: A= AREA OF FLOW = 1/2 (TOZZ) = TOZZ $R_{H} = \frac{A}{P} = \frac{1/2}{1600} = \frac{D}{4}$

n=1013

THEREFORE: Q= 11.486) (=) 43 51/2 Q= (17.81) D2 (D2/3) 51/2 Q= 17.81 08/3 51/2 FOR PIPES \(\leq 10"\ph BY B. L. HALL DATE 8/11/92

ARCADIA, CALIFORNIA

SHEET NO. 5 OF B

(213) 681-5428

(818) 445-2212

JOB NO. LAMMENT PLACE - SEWER MAIN DESIGN LIVE OME ANE

b. ASSUME PIPELINES > 10" & FLOWING 3/4 FULL USE MANNING'S EQN & SOLVE FOR DIAMETER

WHERE: A = AREA OF FLOW = 0.632D2 FROM TABLE 7-4 * RH= = 0.302D FROM TABLE 7-5 &

N=1013

* KING'S HANDBOOK OF HYDRAULICS PAGE 7-35 FOR 0/0 = 0.75

THEREFORE: Q = 0.63202 (1.486) (0.3020)23 51/2 = $92.52 D^{2}(D^{2/3}) s^{1/2}$ Q = 32.52 08/3 6"2 FOR PIPES 710"\$

2. DETERMINE PEAK FLOWIN EACH PIDELINE

a LINE "A"

F= 2.8 GROW ATTACHED GRAPH F16,2-5 LAGSAN DIST.

QAO= 0.71 (2.8) = 1,99cts

BY B.L. HALL DATE 8/11/92

ARCADIA, CALIFORNIA

SHEET NO. 6 OF 8

(213) 681-5428

(818) 445-2212

JOB NO.__

MARKET PLACE - SOLVER MAIN DESIGN LIVEDAK AVE

b. LINE "B"

C. LINE "C"

= 0.71+0.80+0.32

= 1.83 cfs

d. LINE "D"

F = 2.9 FROM ATTACHED

e. LINE "E"

F = 2.45 FROM ATTACHED GRAPH

BY B.L. HALLBATE B/11/92

ARCADIA. CALIFORNIA

SHEET NO __ 7 OF B

CHKD_____DATE______ (213) 681-5428 (818) 445-2212 JOB NO_____ SUBJECT_LA MARKET PLACE - SEWER MAIN DESIGN LIVE DAIL AVE

3, DETERMINE PIRE SIZES

a. LINE A ASSUME D> 10"\$

Q= 32.52 D8/3 51/2 S= ,004

1.99 = 32.52 D 8/3 (,004) 1/2

D8/3 = 0.9675

D = 0.99 ft = 11.85 INCHES USE 12" PIPE

b. LINEB ASSUME D > 10"

Q= 32,520 8/3 5 1/2 5=,004

2.16 = 32.520 43 (.004) 1/2

D8/3= 1.05

D = 1.02 ft = 12.2 IN. USE 12"PIPE

C. LINE C ASSUME D>10"

Q = 32.52 D 93 512 5=,004

4.58 cfs = 32.52 00/3 (.004) 12

D8/3 = 2,23

D = 1.35 ft = 16.2 IN. USE 18" PIRE

d. LINED ASSUME 0> 10"

Q= 32,5208/35"/2 5=.004

1,22 = 32.52 0 8/3 (.004) 1/2

D \$3 = 0.5932

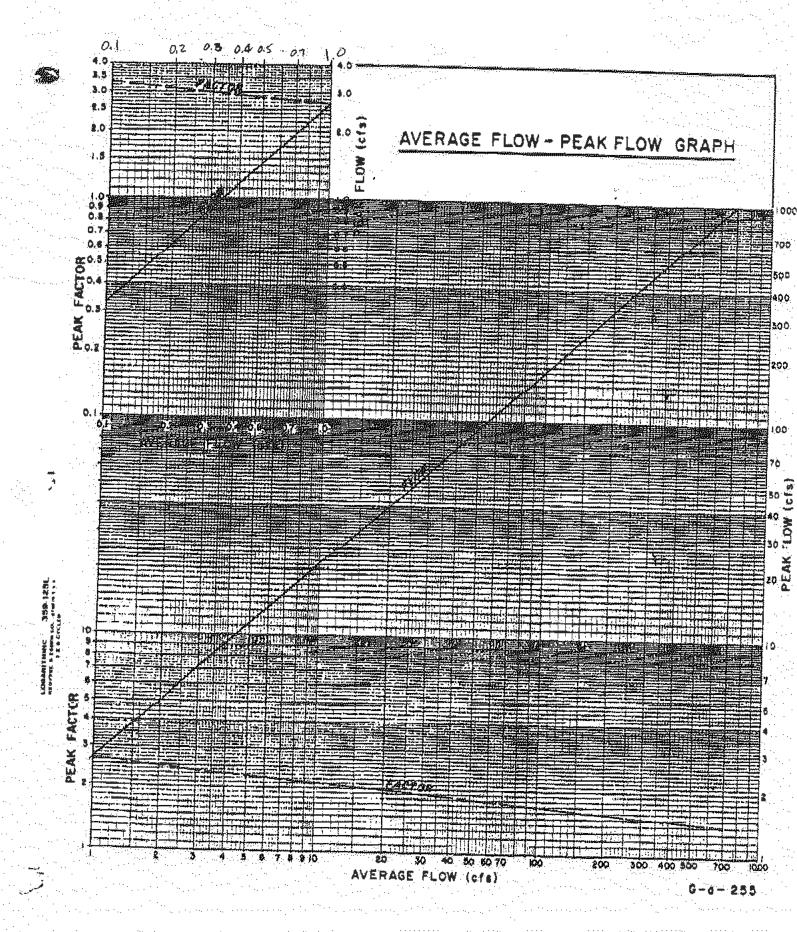
D = 0.82 ft = 9.87 USE 10" PIPE

KENNETH I. MULLEN, CONSULTING ENGINEERS, INC.

BY B.L. HALL DATE B/11/97 ARCADIA. CALIFORNIA SHEET NO. 8 OF B

CHKD DATE (213) 681-5428 (818) 445-2212 JOB NO. SUBJECT LA MARKET PLACE - SEWER MAIN DESIGN LIVE OAK AVE.

e line E Assume D710" $Q = 32.52 D^{8/3} S''^2 \qquad S = .004$ $5.51 = 32.52 D^{8/3} (.004)''^2$ $D^{8/3} = 2.68$ $D = 1.45 \text{ ft} = 17.36 \text{ in}. \quad USE 18'' \text{ pipe}$





COUNTY SANITATION DISTRICTS OF LOS ANGELES COUNTY

1955 Workman Mill Road, Whittier, CA 90601-4998 Mailing Address: P. O. Box 4998, Whittier, CA 90607-4998 Telephone: (213) 699-7411, (213) 685-5217

CHARLES W. CARRY Chief Engineer and General Manager

October 5, 1989

File No: JOA-00.00-00

Ms. Barbara Hull Kenneth Mullen Consulting Engineers 325 North Santa Anita Avenue Arcadia, CA 91006

Dear Ms. Hull:

Standard Wastewater Discharge Factors

Enclosed, per your request, is a copy of the standard wastewater discharge factors used by the Sanitation Districts.

If you have any questions regarding this information, please contact the undersigned at (213) 699-7411, extension 2704.

Very truly yours,

Charles W. Carry

David B. Bruns

Supervising Civil Engineer

Financial Planning &

Property Management Section

JB. R

DBB:mah

Enclosure

LOADINGS FOR EACH CLASS OF LAND USE

TABLE 1

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RESIDENTIAL				
Single Family Home Duplex Triplex Fourplex Condominiums Single Family Home (reduced rate) Five Units or More Mobile Home Parks	Parcel Parcel Parcel Parcel Parcel Parcel Parcel No. of Dwlg. Units No. of Spaces	260 312 468 624 156 156	1.22 1.46 2.19 2.92 0.73 0.73	0.59 0.70 1.05 1.40 0.35 0.35
COMMERCIAL	The st opens	200	3.72	3,55
Hotel/Motel/Rooming House Store Supermarket Shopping Center Office Building Professional Building Restaurant Indoor Theatre Car Wash	Room 1000 ft ² 1000 ft ² 1000 ft ² 1000 ft ² 1000 ft ² 1000 ft ²	125 100 150 325 200 300 1,000 125	0.54 0.43 2.00 3.00 0.86 1.29 16.68 0.54	0.28 0.23 1.00 1.17 0.45 0.68 5.00 0.28
Tunnel Type Wand Type Financial Institution Service Shop Animal Kennels Service Station Auto Sales/Repair Wholesale Outlet Nursery/Greenhouse	1000 ft ²	3,700 700 100 100 100 100 100 100 25	15.86 3.00 0.43 0.43 0.43 0.43 0.43 0.43 0.11	8.33 1.58 0.23 0.23 0.23 0.23 0.23 0.23 0.06
Manufacturing Dry Manufacturing Lumber Yard Warehousing Open Storage Drive-in Theatre Night Club Bowling/Skating	1000 ft ² 1000 ft ² 1000 ft ² 1000 ft ² 1000 ft ² 1000 ft ² 1000 ft ²	200 25 25 25 25 25 20 350 150	1.86 0.23 0.23 0.23 0.23 0.09 1.50 1.76	0.70 0.09 0.09 0.09 0.09 0.05 0.79 0.55

TABLE 1
(continued)

LOADINGS FOR EACH CLASS OF LAND USE

DESCRIPTION	UNIT OF MEASURE	FLOW (Gallons per Day)	COD (Pounds per Day)	SUSPENDED SOLIDS (Pounds per Day)
COMMERCIAL				
Club Auditorium, Amusement Golf Course, Camp, and Park (Structures and Improvements)	1000 ft ² 1000 ft ² 1000 ft ²	37 350 100	0.16 1.50 0.43	0.08 0.79 0.23
Convalescent Home Laundry Mortuary/Cemetery Health Spa, Gymnasium With Showers Without Showers Convention Center, Fairground, Racetrack, Sports Stadium/Arena	Bed 1000 ft ² 1000 ft ² 1000 ft ² 1000 ft ² Average Daily Attendance	125 3,825 100 600 300	0.54 16.40 1.33 2.58 1.29	0.28 8.61 0.67 1.35 0.68
INSTITUTION College/University Private School Church (noncharitable)	A L Student 1000 ft ² 1000 ft ²	20 200 50	0.09 0.86 0.21	0.05 0.45 0.11

STEADY UNIFORM FLOW IN OPEN CHANNELS 7-35

Table 7-4. For Determining the Area a of the Cross Section of a Circular Conduit Flowing Part Full

Let depth of water $\frac{D}{d}$ and $C_a =$ the tabulated value. Then $a = C_a d^3$.

Then

Let $\frac{\text{depth of water}}{\text{bottom width of channel}} = \frac{D}{b}$ and $C_{\bar{y}} = \text{tabulated}$ value.

 $\bar{v} = C_{\bar{v}}D$.

שונ	8.	.01	.02	.03	.04	90.	90.	.07	80.	8.
-	0000	0013	6037	6900	0105	.0147	.0192	0242	0.294	0380
-	.0400	0470	.0534	0090	8990	.0739	1180.	0885	1960	.1039
N	1118	159	1281	.1365	1449	.1535	.1623	11711	800	.1890
60	.1982	2074	2167	2250	.2355	.2450	.2546	2642	2739	.2836
4	2934	3032	.3130	.3229	.3328	.3428	.3527	.3627	.3727	3827
10	.393	.403	.413	.423	.433	.443	.453	.462	.472	.482
9	.492	.502	.512	.521	.531	.540	.550	.559	.569	.578
1	.587	.596	909.	.614	.623	.632	.640	.649	.657	999.
00	.674	.681	689	269.	.704	.712	.719	.725	.732	.738
0	.745	.750	.756	.761	.766	.771	.775	.779	.782	.784

Table 7-5. For Determining the Hydraulic Radius r of the Cross Let depth of where $=\frac{D}{A}$ and C_r = the tabulated value. Then $r=C_rd$. Section of a Circular Conduit Flowing Part Full

80.	_	-	_	-	.243 .247	73 275	-	-	.301	-
ė	_	-	-	_	_	_	-	-	-	-
.07	.045	.104	.157	.202	.240	270	.292	.303	.302	278
90.	.039	660.	.152	.198	.236	.268	.290	302	.303	283
.05	.033	.093	.147	.193	.233	.265	.288	.302	.303	286
.04	.026	780.	.142	.189	.229	.262	.286	.301	.304	980
g	.020	.081	.136	.185	.226	.259	.284	.300	.304	606
20'	.013	.075	.131	.180	.222	.256	.282	.299	.304	204
10.	700.	020.	.126	.176	.218	.253	.280	.298	.304	906
90.	000	.063	121	171.	.214	.250	.278	.296	.304	000
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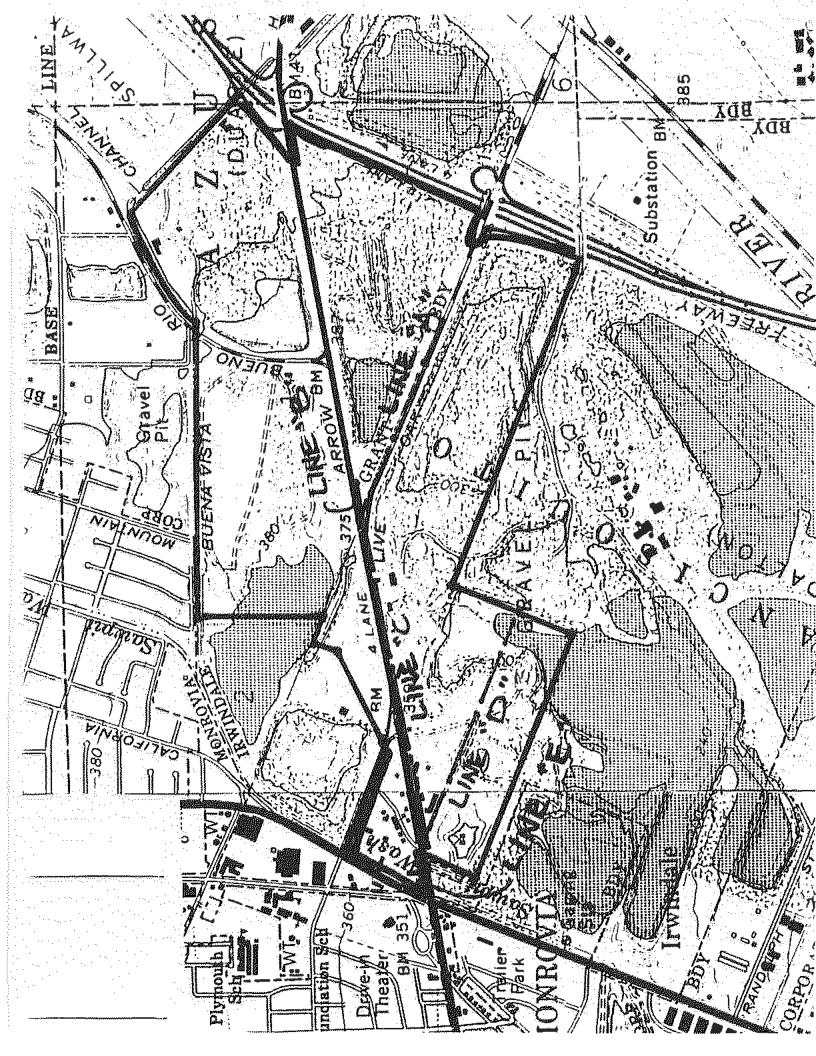
																							_				
	4-1	.472	.452	.438	.426	.417	408	.403	.397	.393	.389	385	.377	.373	.370	.367	364	362	.360	.359	.357	276	9	355	.354	.353	.352
tical	3-1	.478	.462	.448	.438	.420	.421	.415	400	404	.400	.393	.387	.382	.378	.375	372	370	.367	365	.364	989	300	.361	.359	.358	.357
Side alopes of channel, ratio of horizontal to vertical	214-1	.481	.467	.455	.444	.436	.429	.422	.417	.412	.407	8 7 :	.394	.389	388	.381	378	37.5	.373	.370	.368	136		.365	.364	.362	.361
rizonta	2-1	.485	.472	.462	.452	.444	438	.431	.426	.421	.417	409	.403	.397	.393	.389	300	382	.380	.377	.375	979	2 1	.371	.370	.368	.367
o of ho	174-1	.488	.478	.469	.462	.455	448	.443	.438	.433	.420	.421	.415	.409	404	.400	396	393	.390	387	.385	969	300	.380	.378	.377	.375
el, rati	1	.492	.485	.478	.472	.467	.462	.457	.452	.448	.444	.438	.431	.426	.421	.417	413	409	.406	.403	.400	201		395	.393	.391	.389
f chann	34-1	494	.488	.483	.478	474	.469	.465	.462	.458	.455	.448	.443	.438	.433	.420	425	.421	.418	.415	.412	8	100	.407	404	.402	.400
dopes o	1-56	.496	.492	.488	.485	.481	.478	475	.472	.469	.467	.462	.457	.452	.448	.444	.441	438	.434	.431	.429	496	2	.423	.421	.419	.417
Side B	1-1/	.498	.496	494	.492	.490	488	.487	.485	.483	.481	.478	.475	.472	.469	.467	464	462	.459	.457	.455	627		.450	.448	.446	.444
	1/8-1	.499	.498	.497	.496	.495	494	.493	.492	.491	.490	.488	.487	.485	.483	.481	.480	478	.477	.475	474	47.9		471	.469	.468	.467
P	۵	0.05	1.	-15	લ	55	ကံ	.35	4.	.45	ю.	9.	.7	οó	е.	1.0	1.1	1.2	1.3	1.4	1.5	9	2 .	7.7	.8	1.9	2.0

Table 7-3. For Determining the Vertical Distance y below the Water Surface to the Center of Gravity of a Cross Section

of a Trapezoidal Channel

HANDBOOK OF HYDRAULICS

7-34



¥60

SUBDIVISION OF THE RANCHO AZUSA DE DUA M.R. 6 - 80 - 82

POR. SEC.36, T.IN., R.IIW.

FOR PERY, ASSAUTT, SEE: 13770 - 32

CHESTY OF LES AND PROPERTY. offer S.abfillists

BVD

8532

SCALE 1" - 400" 10 BUENA VISTA S.F. 1 (D) 8533 POR SE I/4 SECT, TIS, RIW. * 111 - 25 - 24 GABREL (e)

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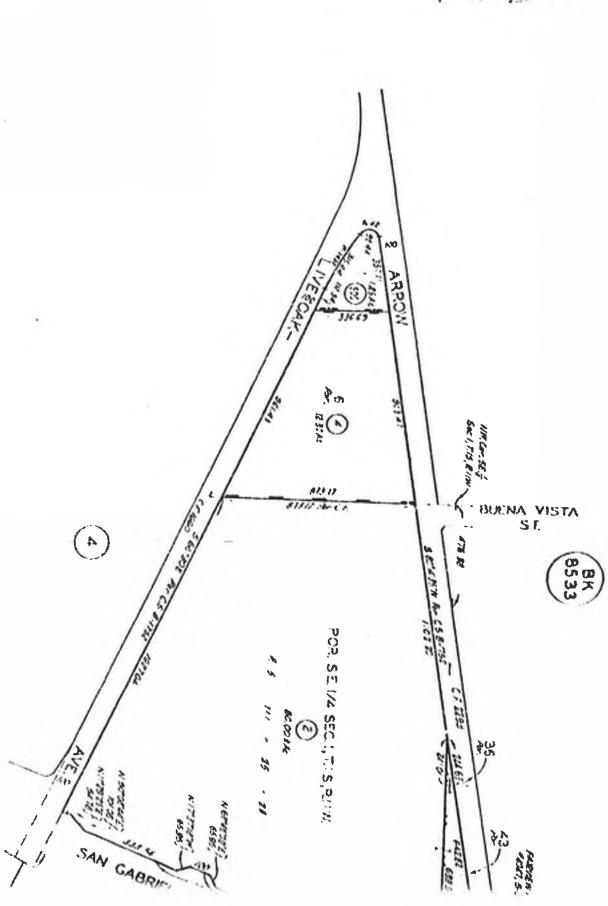
CONFRMEN TO ANDREAS DUARTE P.2-560-561

P.M. 198 - 77-78

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All \$25 series porcess on this page are essessed to the freindale Community Redevelopment Agency, unless otherwise noted.

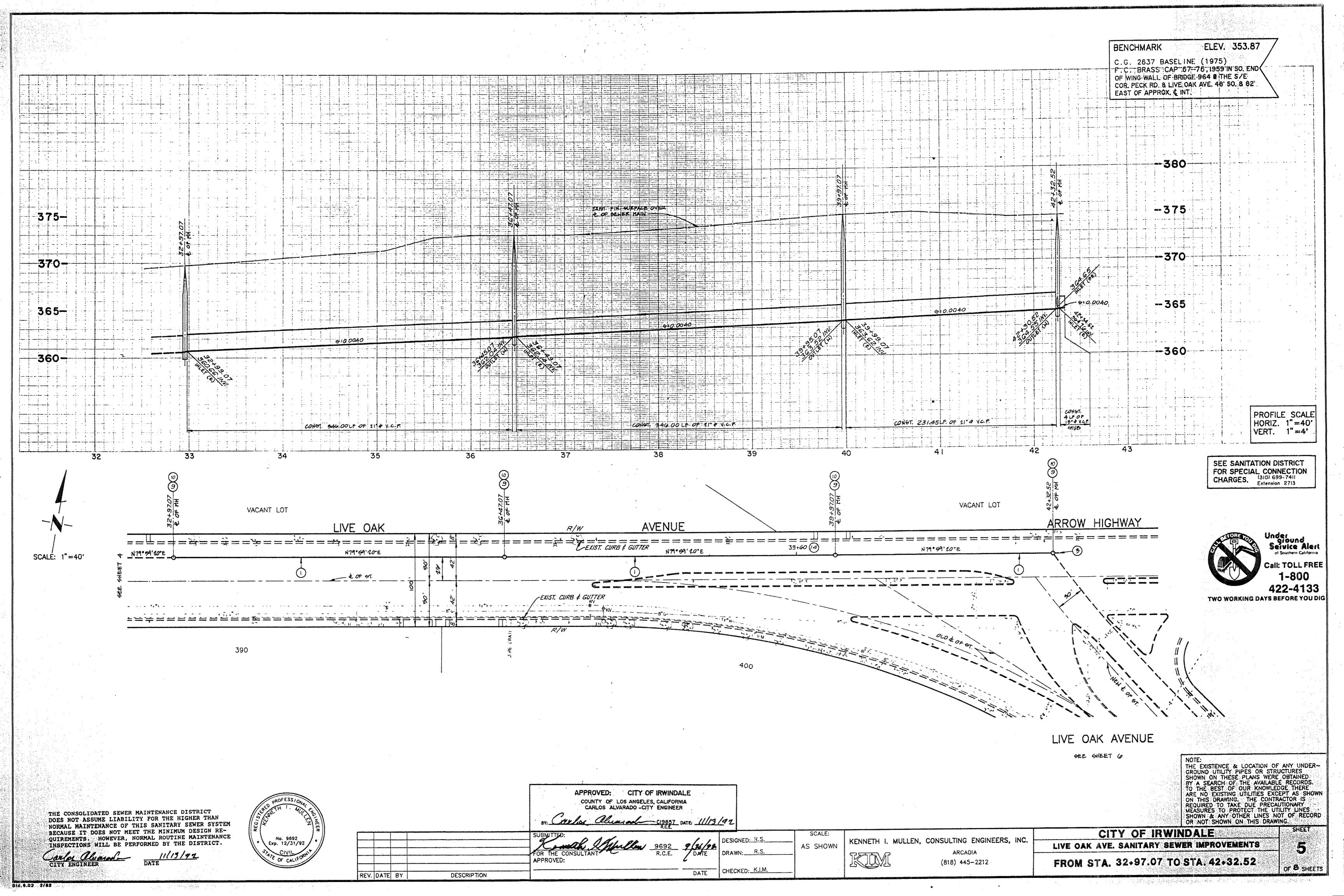
SCALE 1"

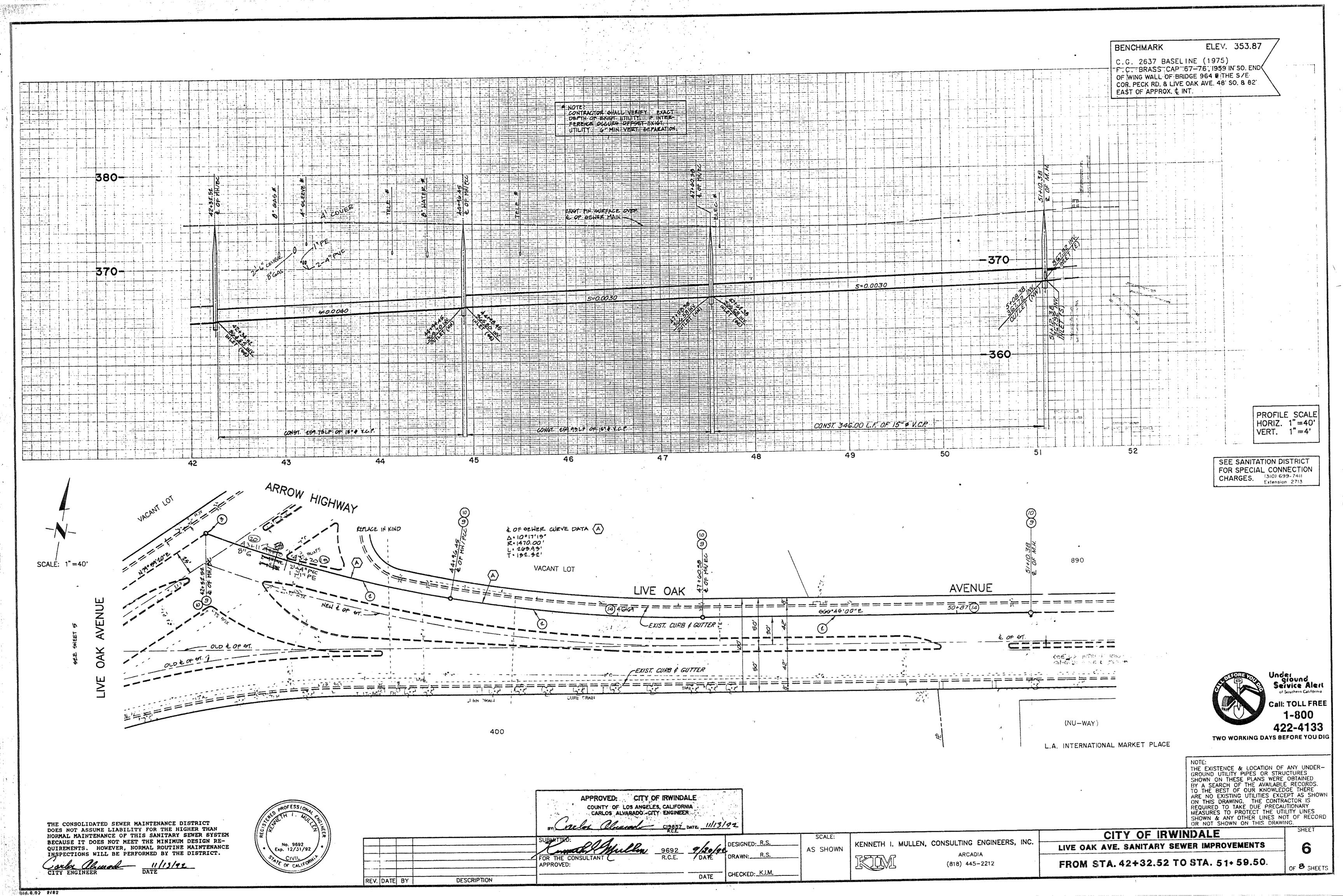


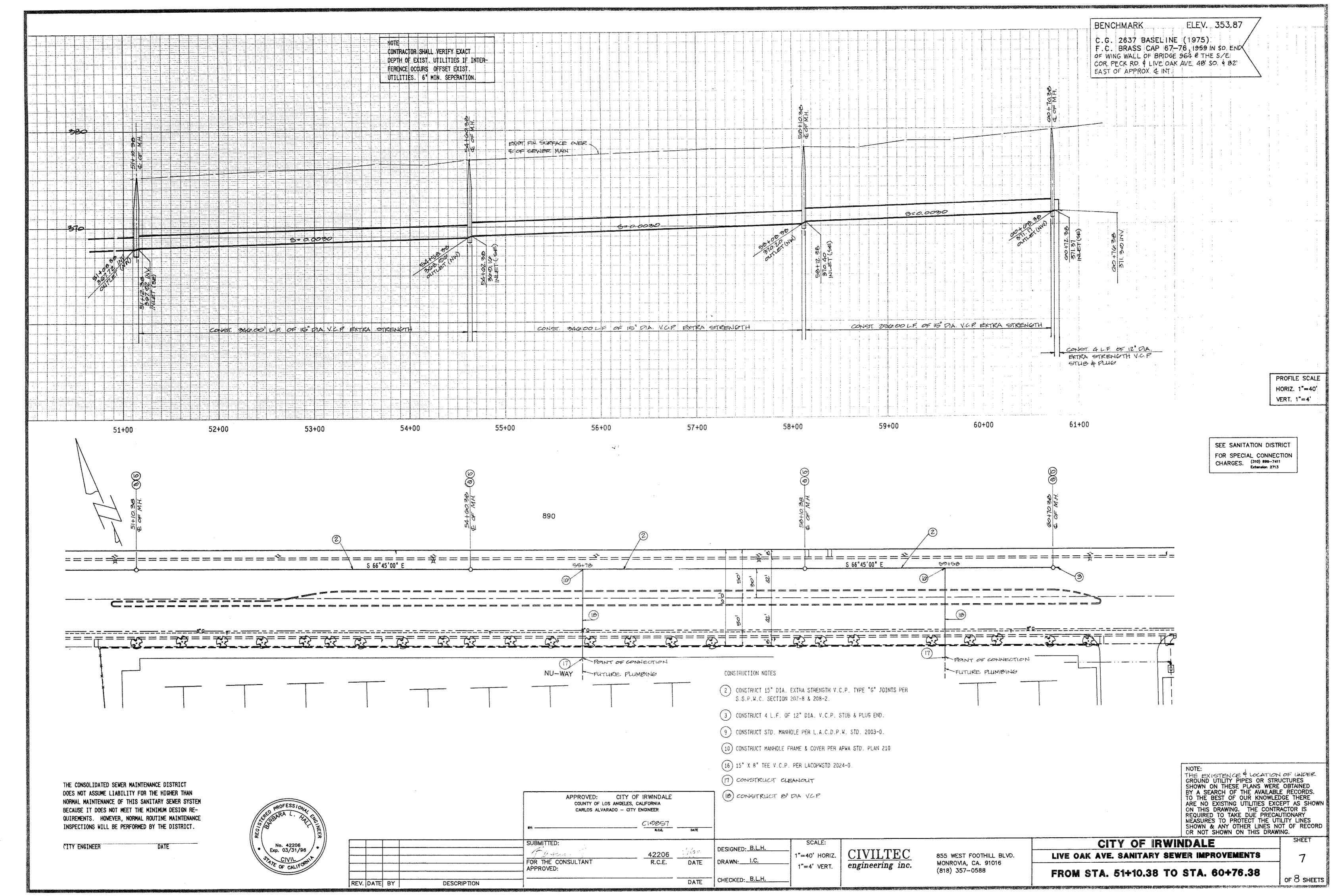
Live Oak Sanitary Sewer Improvement Plans



Appendix F As-Built Plans









CITY OF IRWINDALE

COUNTY OF LOS ANGELES, CALIFORNIA

SEWER IMPROVEMENTS

LIVE OAK AVENUE

FROM STATION 51+10.38 TO STATION 59+28.38

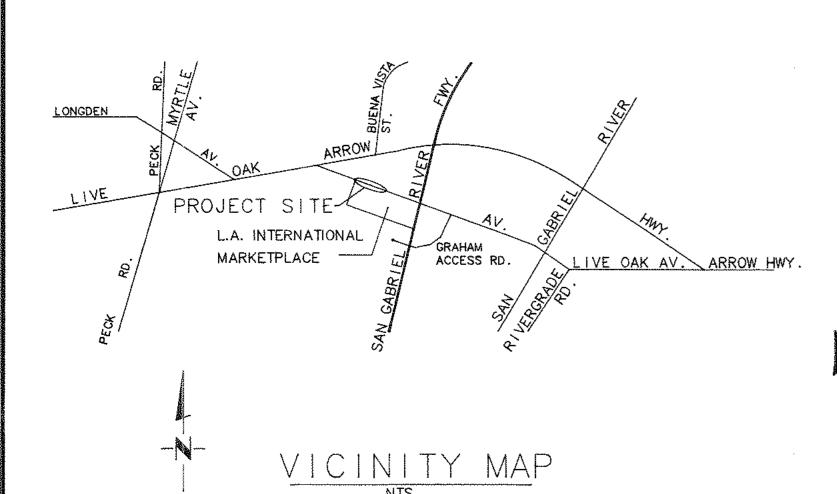
LIST OF DRAWINGS

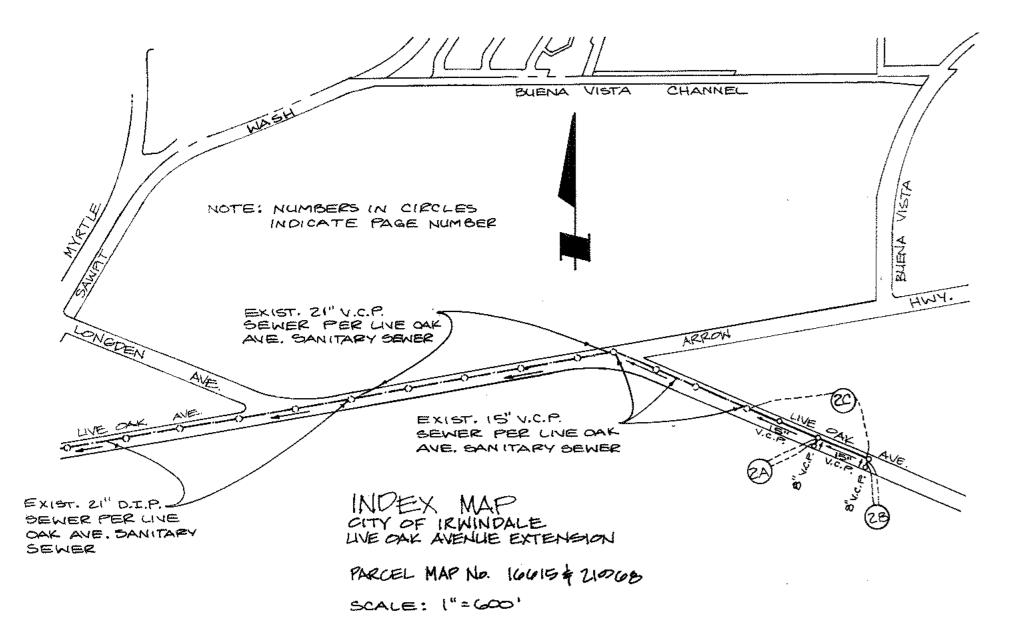
DESCRIPTION

PLAN & PROFILE

TITLE SHEET

SHEET NO.





THE CONSOLIDATED SEVER MAINTENANCE DISTRICT
DOES NOT ASSUME LIABILITY FOR THE HIGHER THAN
NORMAL MAINTENANCE OF THIS SANITARY SEVER SYSTEM
BECAUSE IT DOES NOT MEET THE MINIMUM DESIGN REQUIREMENTS. HOWEVER, NORMAL ROUTINE MAINTENANCE
INSPECTIONS WILL BE PERFORMED BY THE DISTRICT.

APPROVED - CITY OF IRWINDALE

COUNTY OF LOS ANGELES, CALIFORNIA

CARLOS ALVARADO - CITY ENGINEER

Carlot Olicerosla - C19857 4-16/93

RCE DATE

SUBMITTED:

REVISIONS

DESCRIPTION

APP. DATE

No. 42206
Exp. 03/31/96

*

CIVIL CRUIT

SUBMITTED:

Butan Lal 42206 3/10/93
BY THE CONSULTANT RCE DATE

BENCHMARK

ELEV. 353.87

C.G. 2637 BASELINE (1975)

F.C. BRASS CAP 67-76, 1959 IN S

END OF WING WALL OF BRIDGE 964 @

THE S/E COR. PECK RD. & LIVE OAK

AVE. 48' S & 82' E OF APPROX CLINT

GENERAL NOTES

- ALL WORK SHALL BE PERFORMED IN STRICT CONFORMANCE WITH THE CURRENT STANDARD SPECIFICATIONS FOR PUBLIC WORKS CONSTRUCTION. 1992 EDITION AND ALL SUPPLEMENTS APPURTENANT THERETO AND LACDPW STANDARD DRAWINGS LATEST EDITION.
- ANY CONTRACTOR PERFORMING WORK ON THIS PROJECT SHALL FAMILIARIZE HIMSELF WITH THE SITE AND SHALL BE SOLELY RESPONSIBLE FOR ANY DAMAGE TO EXISTING FACILITIES RESULTING DIRECTLY OR INDIRECTLY FROM HIS OPERATIONS, WHETHER OR NOT THEY ARE SHOWN ON THE PLANS.
- ALL OBSTRUCTIONS WITHIN THE AREA TO BE IMPROVED ARE TO BE REMOVED AND/OR RELOCATED AT THE DIRECTION OF THE CITY ENGINEER. UTILITIES SHALL BE RELOCATED BY THEIR RESPECTIVE OWNERS. THE CONTRACTOR IS REFERRED TO SECTION 5 OF THE STANDARD SPECIFICATIONS.
- 4 UTILITY LINE LOCATIONS WERE TAKEN FROM RECORD AND WERE NOT LOCATED IN THE FIELD, UNLESS OTHERWISE NOTED ON THE PLAN. THE CONTRACTOR IS REFERRED TO SECTION 5 OF THE STANDARD SPECIFICATIONS.
- ALL WORK SHALL CONFORM TO THE PROVISIONS OF CONSTRUCTION SAFETY ORDERS ISSUED BY THE STATE DIVISION OF INDUSTRIAL SAFETY. IN CASE OF ANY ACCIDENTS INVOLVING SAFETY MATTERS COVERED BY SECTION 6424 OF THE CALIFORNIA LABOR CODE, THE CONTRACTOR SHALL IMMEDIATELY NOTIFY THE STATE DIVISION OF INDUSTRIAL SAFETY.
- 6 CALL UNDERGROUND SERVICE ALERT FOR UNDERGROUND LOCATIONS 48 HOURS BEFORE YOU DIG AND PAVE AT (800) 422-4133.
- THE CONTRACTOR SHALL OBTAIN A NO-FEE TRAFFIC CONTROL PERMIT 48
 HOURS PRIOR TO TIME OF CONSTRUCTION WITHIN THE PUBLIC RIGHT-OF-WAY.
 THE CONTRACTOR IS REFERRED TO SECTION 7-10.3 OF THE STANDARD
 SPECIFICATIONS.
- THE CONTRACTOR SHALL RENEW OR REPLACE ANY EXISTING TRAFFIC STRIPING AND/OR PAVEMENT MARKINGS WHICH HAVE BEEN EITHER REMOVED OR THE EFFECTIVENESS OF WHICH HAS BEEN REDUCED AS A RESULT OF HIS OPERATIONS. RENEWAL OF PAVEMENT STRIPING AND MARKINGS SHALL BE DONE IN CONFORMANCE WITH SECTION 310-5.6 OF THE STANDARD SPECIFICATIONS.
- ALL SEWER MAINS SHALL BE EXTRA STRENGTH VITRIFIED CLAY PIPE (V.C.P.)
 UNLESS OTHERWISE SHOWN AND APPROVED BY THE CITY ENGINEER.
- PRIOR TO STARTING CONSTRUCTION, THE CONTRACTOR SHALL VERIFY LOCATION AND ELEVATION OF EXISTING SEWER MAIN(S) AND NOTIFY THE DESIGN ENGINEER OF ANY VARIATION FROM DESIGN.
- ALL MANHOLES ARE CONSIDERED A CONFINED SPACE WHERE TOXIC FUMES MAY COLLECT. THE CONTRACTOR SHALL FOLLOW ALL CAL-OSHA REGULATIONS WHILE WORKING IN SUCH CONFINED SPACES INCLUDING THE USE OF BREATHING APPARATUS WHERE FOUND NECESSARY.
- CONSTRUCTION OF NEW SEWER MAIN SHALL BE DONE IN ACCORDANCE WITH STATE OF CALIFORNIA DEPARTMENT OF HEALTH SERVICES CRITERIA FOR SEPARATION OF WATER MAINS AND SANITARY SEWERS. THE PLANS INDICATE THE CASE AND ZONE UNDER THESE QUIDELINES DETERMINED BY A SEARCH OF AVAILABLE UTILITY RECORDS. SHOULD THE CONTRACTOR ENCOUNTER CONDITIONS WHICH REQUIRE A MODIFICATION OF THE STATED CASE AND ZONE IN THE FIELD, HE SHALL IMMEDIATELY BRING IT TO THE ATTENTION OF THE CITY ENGINEER.
- 13 LEAKAGE TESTS SHALL BE PERFROMED ON ALL SEWERS AS SPECIFIED IN S.S.P.W.C. SECTION 306-1.4.4
- TRAFFIC CONTROL WILL BE PROVIDED IN ACCORDANCE WITH THE SPECIAL PROVISIONS OF THE CITY OF IRWINDALE

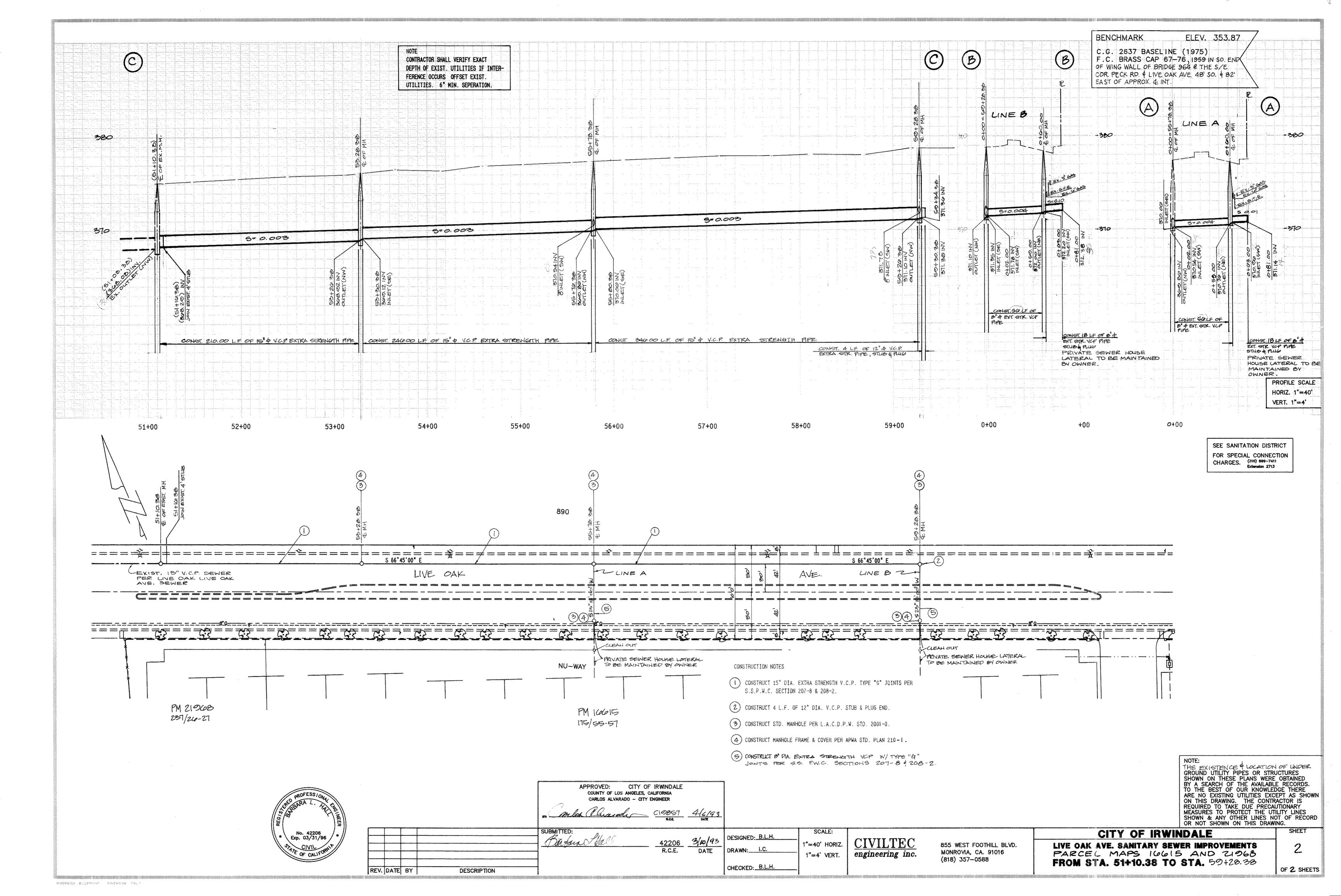
NO CONNECTION FOR THE DISPOSAL OF INDUSTRIAL WASTES SHALL BE MADE TO SEWERS SHOWN ON THESE DRAWINGS UNTIL A PERMIT FOR INDUSTRIAL WASTEWATER DISCHARGE HAS BEEN ISSUED BY THE SANITATION DISTRICTS FOR SAID CONNECTION.

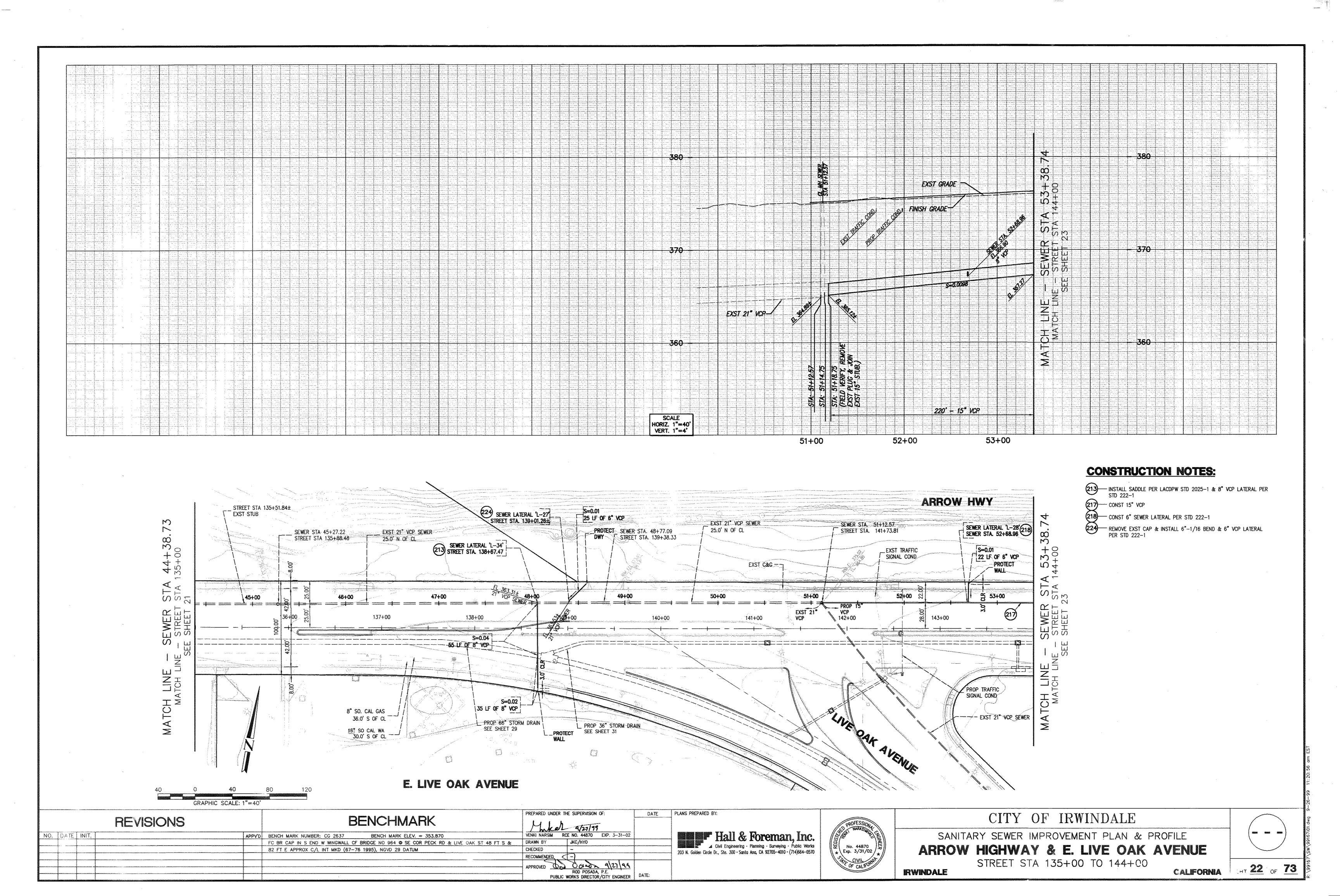


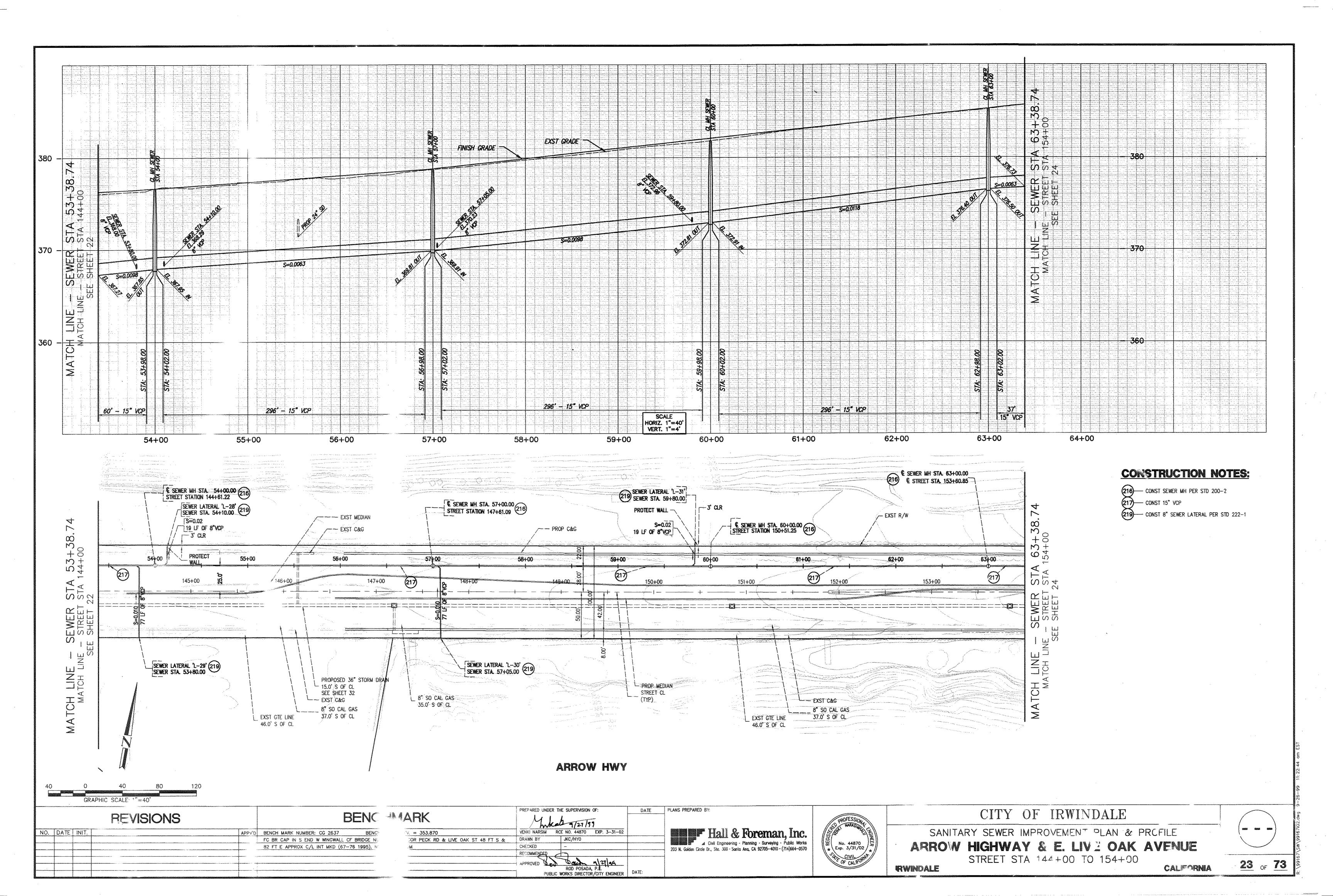
CITY OF IRWINDALE

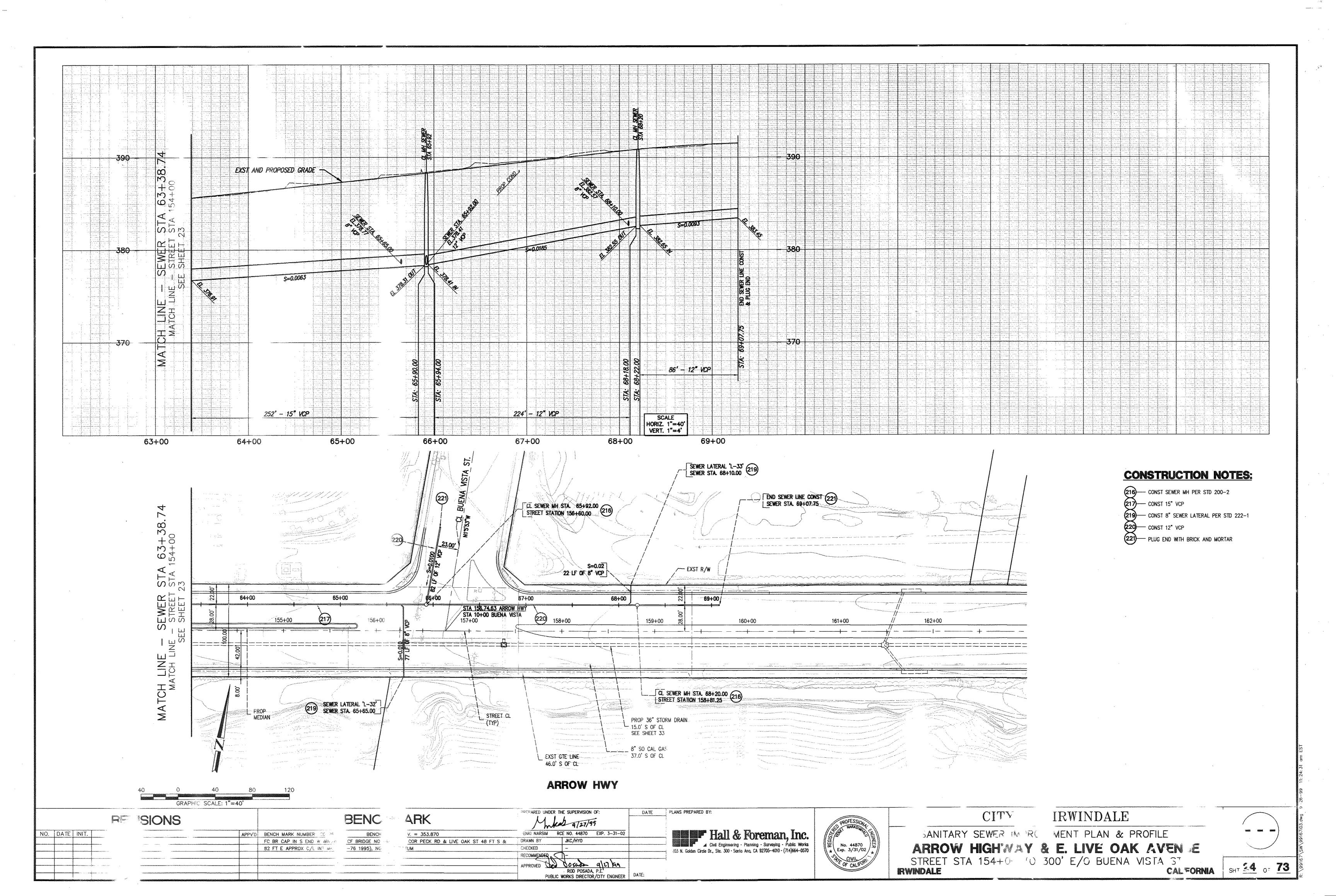
PARCEL MAPS 16615 AND 21968
TITLE SHEET

DESIGN: BLH CHECKED: SCALE: NONE
DRAWN: IC J.N. 92-206 SHEET 1 OF 2









COUNTY OF LOS ANGELES, CALIFORNIA

SEWER IMPROVEMENTS IN LIVE OAK AVENUE

FROM STATION 0+91.50 TO STATION 22+47.07

CONSTRUCTION NOTES:

L.A. INTERNATIONAL

-PROJECT SITE

(5) CONSTRUCT SHALLOW MANHOLE PER LACOPW STD. 2002-0.

(6) CONSTRUCT STO. 60" MANHOLE TYPE "E" PER C.S.O. STO. 5-0-206

VICINITY MAP

INSTALL 36" C.O. X 3/6" TRICK STEEL PIPE CASING.

(1) CONSTRUCT 20° D. I.P. CLASS 50 OR CLASS 52 W/ TYTCH JOINTS. ASTM 4746.

LEVE DAK AV

(2) CONSTRUCT MANHOLE FRAME & COVER PER C.S.D. STD. S-0-228.

(3) CONSTRUCT MANHOLE FRAME & COVER PER LACOPW STD. 2014-0.

(3) CONSTRUCT MANHOLE STEPS PER C.S.D. STO. 5-4-209.

CONSTRUCT JUNCTION STRUCTURE "A" PER ARMY CORPS OF ENGINEERS PERMIT MANUAL FIGURE A-18.

(7) CONSTRUCT CONDUIT SUPPORT, CASE 2, PER APWA STO. PLAN 224-0.

LIST OF DRAWINGS

DESCRIPTION TITLE SHEET **PLAN & PROFILE** PLAN & PROFILE

ALL WORK SHALL DE PERFORMED IN STRICT CONFORMANCE WITH THE CURRENT STANDARD SPECIFICATIONS FOR PUBLIC WORKS CONSTRUCTION. 1892 RUITION AND ALL SUPPLIMENTS APPURIENANT THERETO AND LACEDY STANDARD DRAWINGS LATEST EDITION.

ELEV. 353,87

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ic g 2637 BASELINE (1975) F.C. BRASS CAP 67-76, 1959 IN S. END OF WIND WALL OF BRIDGE 964 @ THE S/E COR, PECK RO, & LIVE OAK AVF. 48'S & 82'E OF APPROX CE

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PRINTED JUN 23 1983

APPROVED - CITY OF IRWINDALE COUNTY OF LOS ANGELES, CALIFORNIA

> CARLOS ALVARADO CITY ENGINEER RCE DATE

PY THE CONSULTANT REE DATE



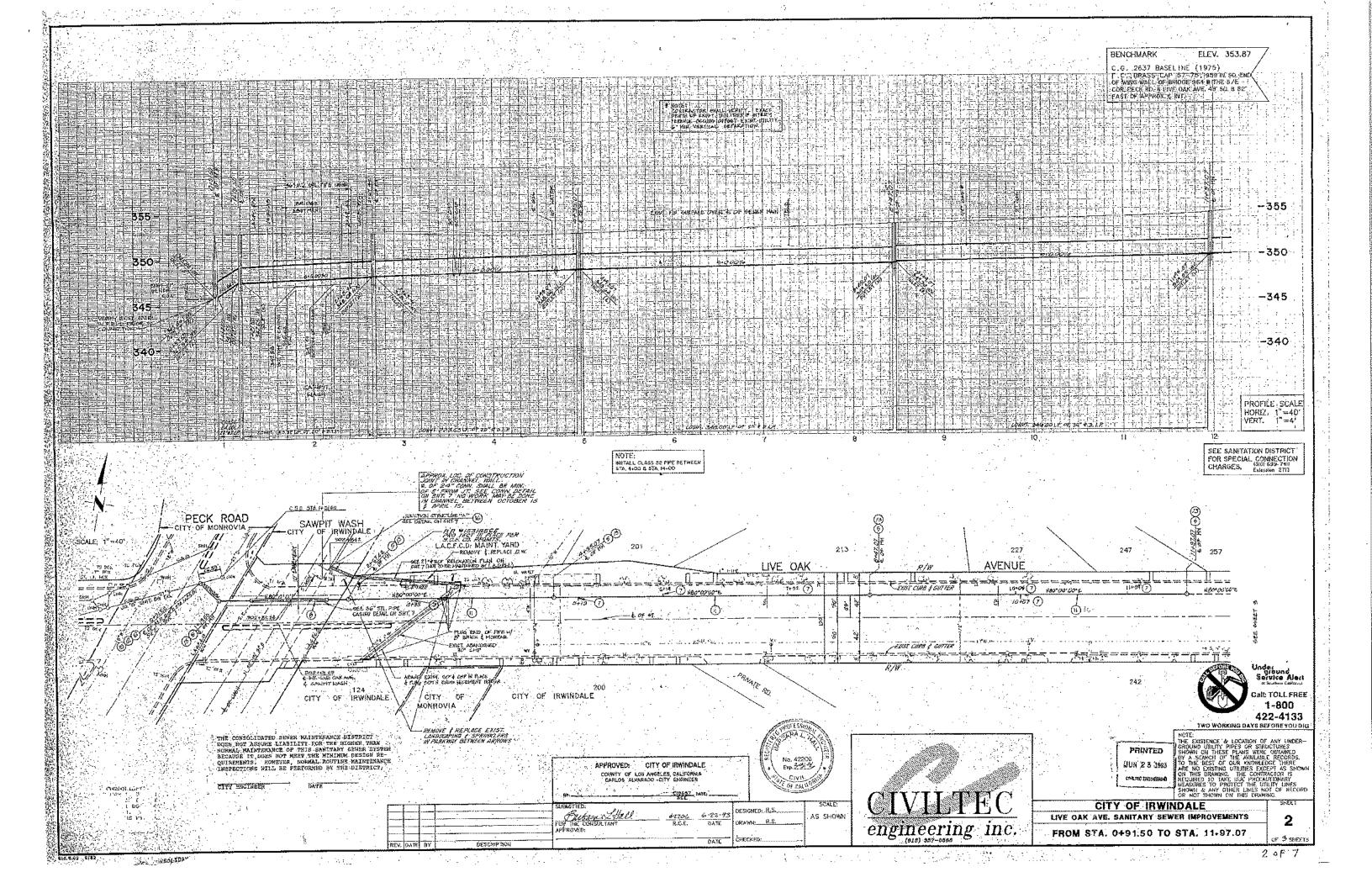
CITY OF IRWINDALE

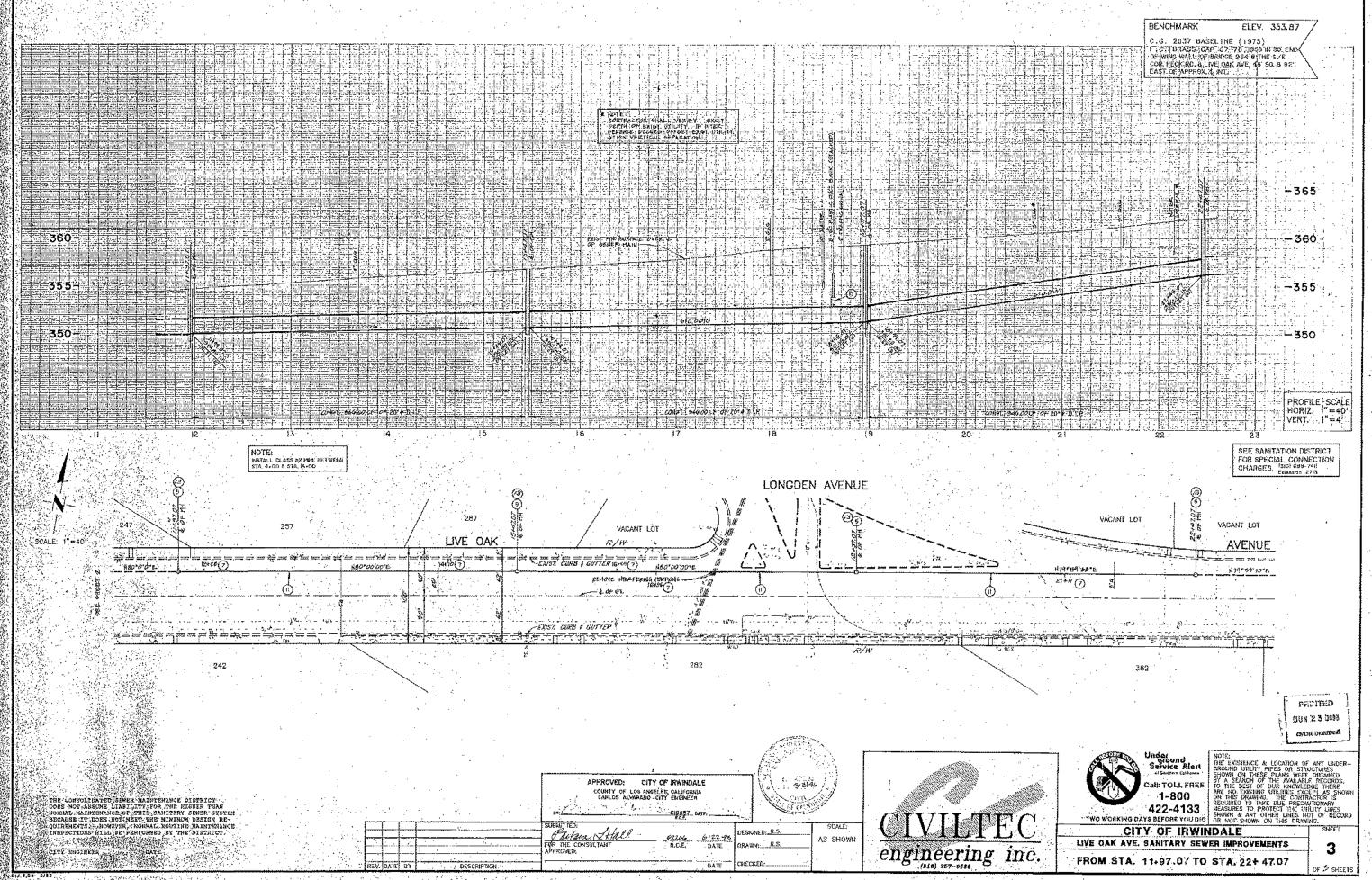
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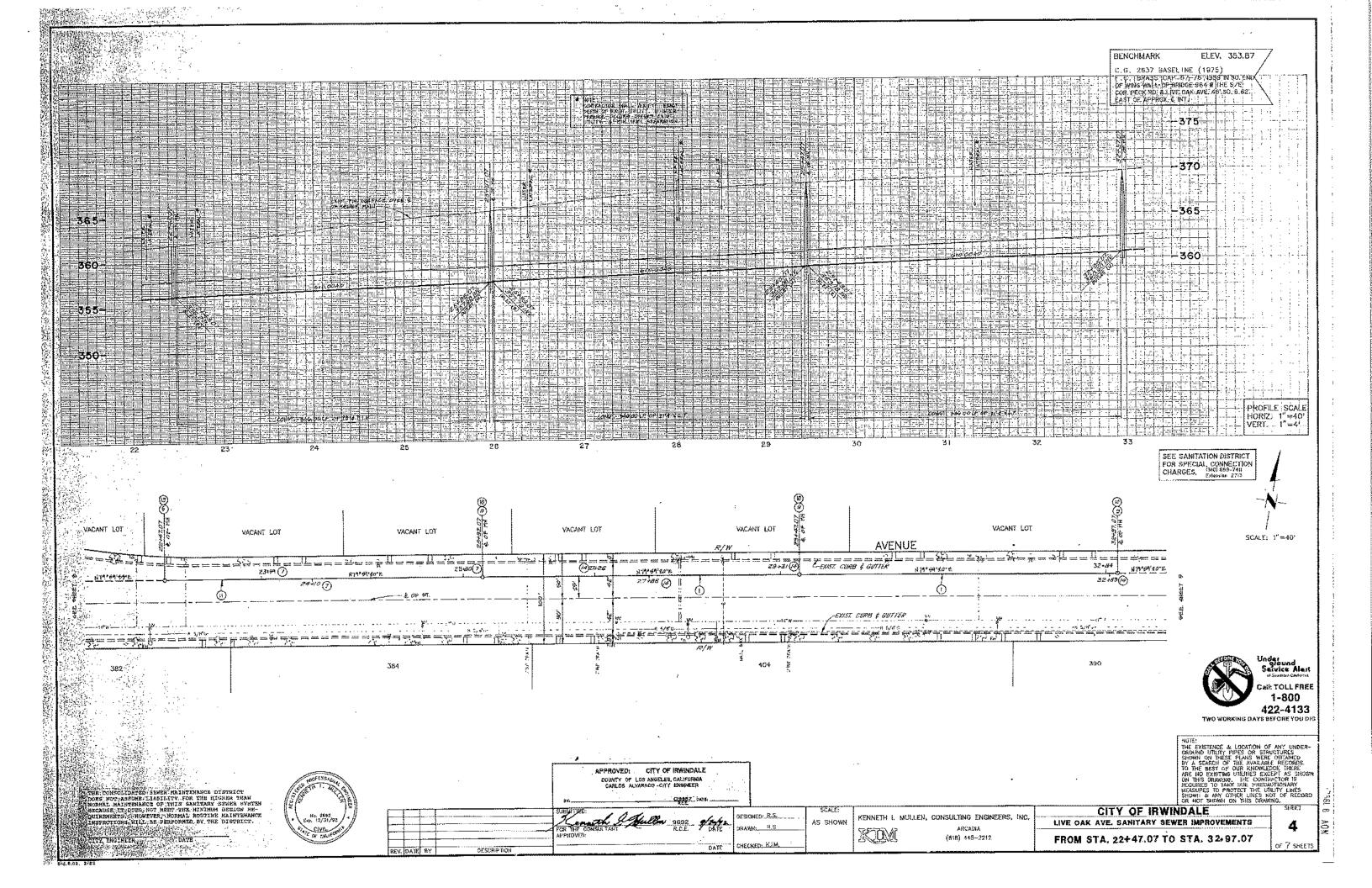
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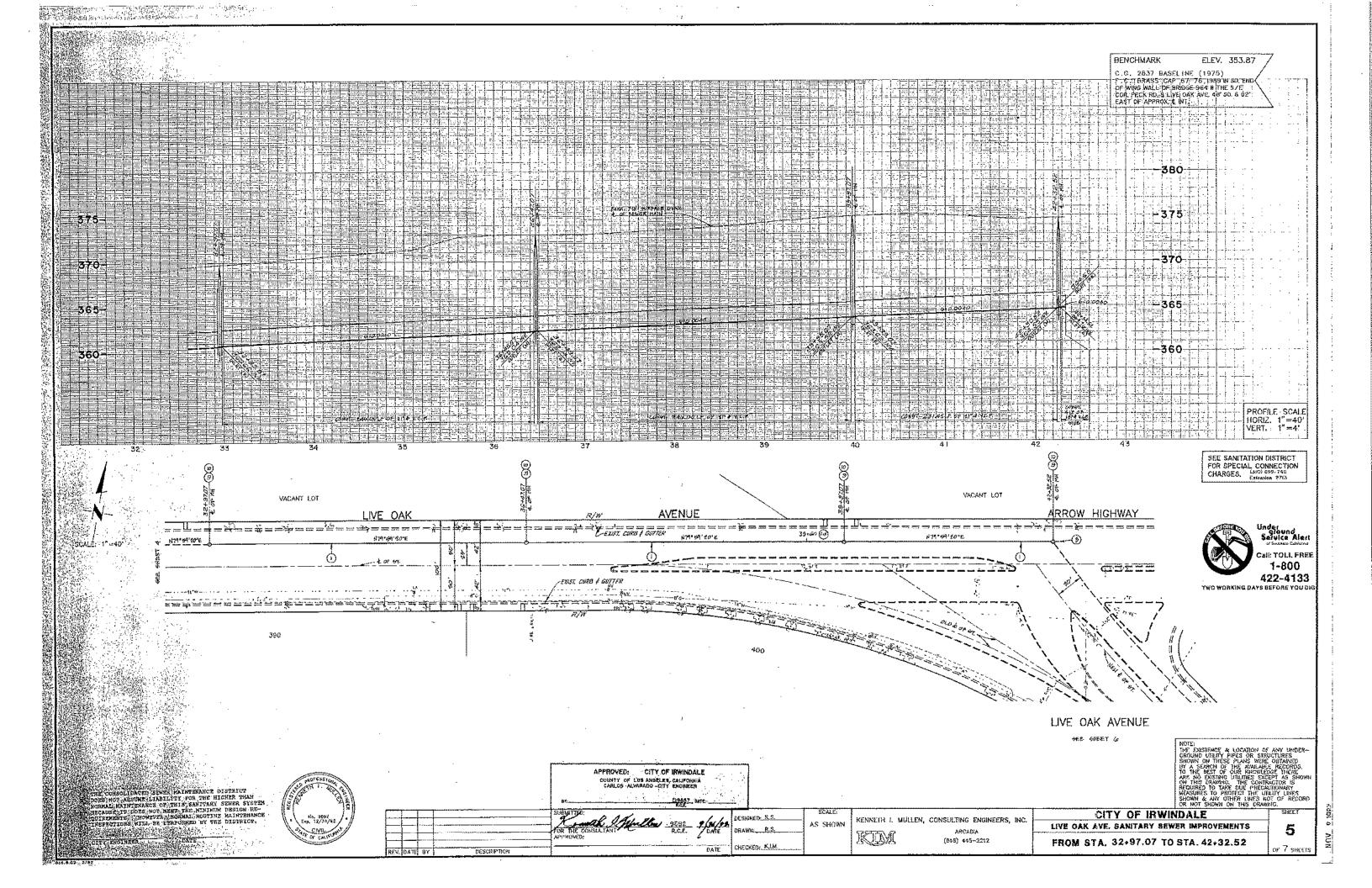
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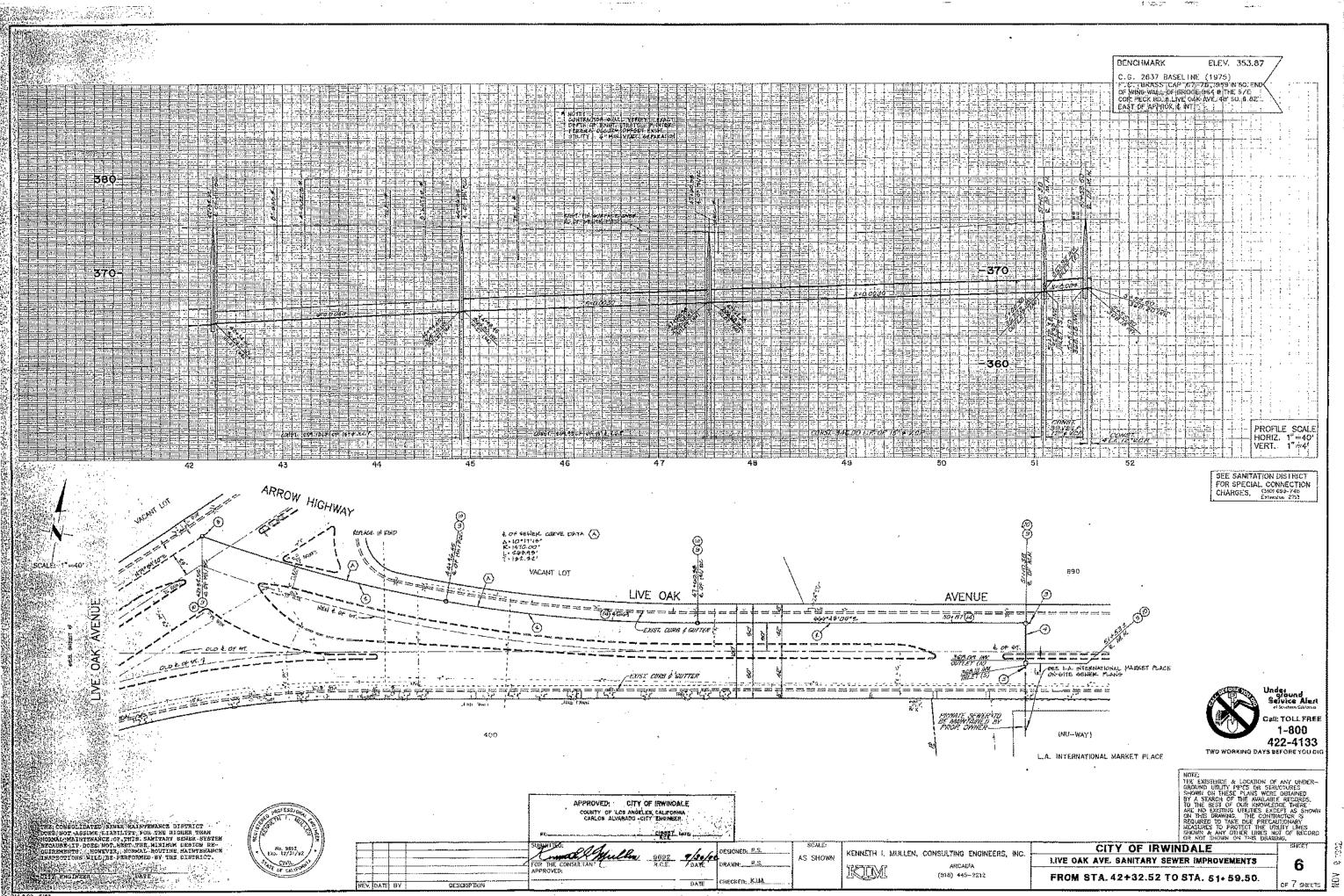
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